City of Chicago – Department of Buildings Building Application – Storm Water Review Only

For the Former Celotex Site 2800 South Sacramento Avenue/ 3031 South Albany Avenue Chicago, Illinois 60623

Prepared for

City of Chicago - Storm Water Permit Review

August 2008



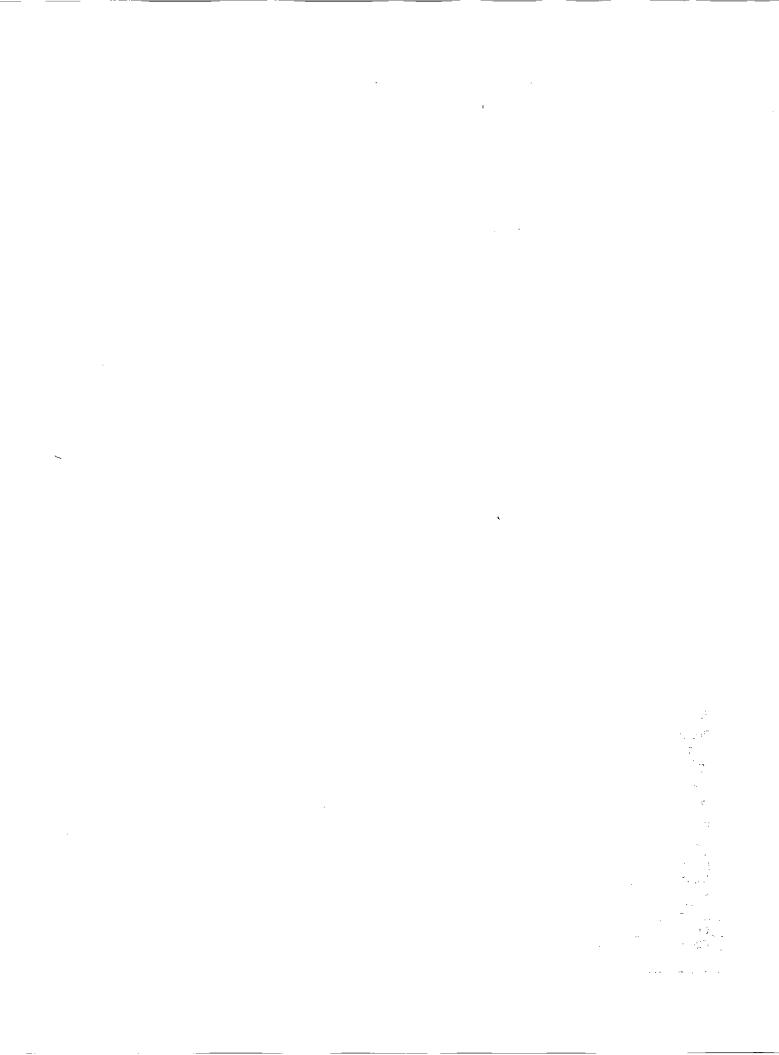




Renovated

DEPARTMENT OF BUILDINGS

Building Permit Application HOLDS: **USE BLACK INK:** Y DO NOT WRITE IN SHADED AREA Stop Order(s): **Violations** APPLICATION PERMIT NO .: 100253796 Landmark Special Admin. Hold DS APPLICATION NO.: Lakefront Prot. Other DATE ISSUED: Flood Plain 1. GENERAL INFORMATION (Provide Original House Number Certificate for new construction.) Property Index Number(s) (PIN) (required): Address: Please enter two if a corner property. 1.16.25.309.012.0000 2800 S. Sacramento Ave and 3031 S. Albany Chicago, IL Number of dwelling units, number of stories, building use, description of proposed work and parking: 216.25.309.014.0000 Regrading, contouring oxsicustopes, fence installation, and installation of new stormwater management sixtem 3.16.25.309.015.0000 Enter permit number if revision to an existing permit: 4.16-25-309-016-0000 Cost of Construction: \$ 5,000,000 5.16-25-309-017-0000 2. CLASSIFICATION BY OCCUPANCY: NA D Open Air Assembly H1 Storage Low Hazard A Residential E Business H2 Storage Moderate Hazard A2 Residential H3 Garages B Institutional F Mercantile 1 Hazardous C1 Assembly Private Garage J Miscellaneous Building C2 Assembly G1 Industrial Low Hazard C3 Assembly G2 Industrial Moderate Hazard Technology Center 3A. BUILDING INFORMATION FOR EXISTING BUILDING: NA Const. Class. Basements No. Comm. Width Height Area (sf) Volume (cf) No Stories No DII Length Units Existing 3B. BUILDING INFORMATION FOR NEW CONSTRUCTION (IF APPLICABLE): No. Comm. Width Const. Class. No. Stories Basements No. D.U. Length Height Area (sf) Volume (cf) Units Addition New Bldg. (Front or Rear) Detached Garage Fence 5,000 6' Trash Enclosure 3C. BUILDING INFORMATION FOR RENOVATION (IF APPLICABLE): NA Const. Class. No. Comm. Height Area (sf) Volume (cf) Basements Width No. Stories No. D.U. Lenath Units Area to be



			s of lot and buildings, showing dimensions, streets, dscaping and north arrow.)
Plat of Survey			Area of Lot
Plate Number		78	Height of Building:
Zoning District/P.D. #:	13. Sep	, , , , , ,	Area and Volume of Building:
Zôning Use:			Number of Parking Spaces:
Front or Rear Building:			Number of Loading Spaces:
Špeciąl Zoning Permission Required for Administrative A	djustm	ent, V	anance or Special Use: □¡Yes 🎉 □ No
Case Number:		3774. 378.3	
Signature of Approval			Date
5. F	1 1		NTION ITEMS:
	Yes	No	
Existing Sprinkler System		×	Flammable Liquids
Install Full Sprinkler System Install Partial Sprinkler System (Designate Areas to be		_X	Corrosive Liquids
Sprinklered):		¥	Hazardous Chemicals
Extend Existing Sprinkler System (Designate Areas to be Sprinklered):		X	Oxidizing Materials
Relocate Sprinkler Heads Only		X	Highly Flammable Materials
Existing Standpipe System		X	Fume Hazardous Gases
Install New Standpipe System		X	Flammable Compressed Gases
Existing Fire Alarm System (Choose One): Class I High Rise Class II Other, clarify		×	Dust Producing Equipment
Install New Fire Alarm System (Choose One): Class I High Rise Class II Other, clarify		×	Is this permit for modifications to the building in order to pass the Life Safety Evaluation as per code section 34 (13-196-206)?

6. MAYOR'S OFFICE FOR PEOPLE WITH DISABILITIES ITEMS Is the project Government financed, subsidized or guaranteed? Ŋ√No If yes, specify type of funding: city, state or federal. RENOVATION PROJECTS ONLY: Provide total alteration cost in last 30 months using EAC / ERC = _ EAC = Estimated Alteration Cost for Project Budget + Alteration Cost in Last 30 Months ERC = Estimated Reproduction Cost = Work Area (sf) x New Construction Cost per sf HOUSING PROJECTS ONLY (Submit Part II Letter of Approval at intake meeting, if applicable.): Multiple Dwellings: Total Number of Dwellings Units: Structure with Four or More Units: Single Family Residential (Detached): Attached Multi-Story Single Family Residential Units with Separate Means of Egress: Other: Proposed No. Actual No. D.U. D.U. Accessible Lodging Units [1107.5.1.1 (ANSI Section 1002)] Units with Communication Features [1107.5.1.1 (ANSI Section 1005)] Accessible Units with Communication Features [1107.5.1.1 (ANSI Section 1002 + 1005)] Type A [1107.5.2.2 (ANSI Section 1003)] Type B [1107.5.2.3 (ANSI Section 1004)] Type A & B with Conduit Lines [1107.5.2.4] Visitable [1107.5.4.3 and 1107.5.5.3] Attached Multi-Story SFR Units with Separate Means of Egress [1107.5.4.3 + 1107.5.5.3] Section 504 Accessible Units [1107.5.5.5.1 and (U.F.A.S. Sec. 4.34)] Section 504 Accessible Units with Communication Features [1107.5.5.5.2 and 1107.5.5.4 (ANSI Section 1005)] Zoning Incentive Building Type A Units [17-2-0304 A & B, 17-2-0306, 17-2-0311 A & A (a) (Zoning Code) (ANSI Section 1003)] Change of Occupancy (20+ Units) 7. ENVIRONMENTAL ITEMS Yes No Yes No Boiler(s) $\boldsymbol{\times}$ X **Dry Cleaning Machinery** Gas Fired Hot Water Heater(s) Manufacturing Process Equipment and Control X X Devices Gas Fired Package Rooftop, Furnaces Manufacturing Process Equipment or Area, X X Hazardous/Flammable Storage Air Pollution Control Devices Unit Heaters or other Gas Fired HVAC Units ¥ Y Unfired Pressure Vessel (Air Tanks, Heat Exchanger, Paint Spray Booth or Paint Spray Area X Hot Storage Tanks) X Commercial Cooking Equipment or Food Preparation Paint Spray Booth or Paint Spray Area in Motor X × Unit Vehicle Repair Shop **Emergency Generator** X X New Incinerator or Afterburner Equipment Underground/Aboveground Storage Tank Unit (Apply Sandblasting, Grinding of Masonry, or Chemical X X at DOE) Cleaning of Any Architectural Surface Compactor or Bailer X

		8. REMARI	KS AND API	PROVALS		ia zai i	
Remarks By:					Date		
Remarks By:					Date		
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Remarks By:					Date:		
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[12] A. S. M.							
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Remarks By:				U.S.B. 1	Date		
Remarks By:				3.31 3.31 3.31 3.31 3.31 3.31 3.31 3.31	Date		
				3.31 3.31 3.31 3.31 3.31 3.31 3.31 3.31			

9. CONTACT INFORM	TATION	
Owner/Tenant/Agent: Samvel Palumbo (Manasch Pa	reel)	
Lic. #	city <u>Hillside</u>	
Address: 321 Center Street		
E-mail:	705 644	
Emergency Contact:	Telephone No.:	
Arch./Eng.:	City:	
Address:		
E-mail:		
General Contractor: CH2M Hill Constructors, Inc.		
Lic. #: TG-C04805	City: Englewood	
Address: 9191 South Jamaica St.	State: (cloracio	Zin Code: 80112
E-mail:	Telephone No: 720-281cm	
Mason Contractor:	C Citv:	
Address:		
E-mail:		
Electrical Contractor:	City:	
Address:		
E-mail:	Telephone No:	
Vent/Heat Contractor:	City:	
Address:		
E-mail:		
Refrig./AC Contractor: Lic. #:	City:	
Address:		
E-mail:	Telephone No:	•
Plumbing Contractor:Lic. #:	City:	
Address:		
E-mail:		•
Expeditor:		
Lic. #:		
Address:		
E-mail:		
Local Arch./Eng.*:		·
Lic. #:		
Address:		
E-mail:		

(*If your licensed Architect is not located in the State of Illinois, you have the option to identify a local Illinois Architect to represent you at DOB to attend meetings and attend Open Plan Review.)

WARNING TO PROPERTY OWNER/TENANT AND GENERAL CONTRACTOR

1, Samuel S. Palumbo, Ir, as property owner/tenant, and	d I,,	as general contractor, understand that it is
against the law to exceed the scope of a building permit. I understand that	at if I build, or allow anyone else to b	uild, any building, room addition, structure or
other object that differs from, or in any way exceeds, what this permit au ceed, or allow anyone else to exceed, the scope of this building permit,		
ہ to \$5,000.00 per day; imprisoned for up to six months; required to do		• • • •
pense all completed work; and, in addition to any other penalties provided	d by law, required to reimburse the	City up to three times any damages incurred
for providing any false or inaccurate information in this building permit app		
conform to the requirements of the Chicago Building Code and, if it does		
Owner Signature -or- Samuels. Palumgo, Jr., Proceed.	Monarch Asahall Co	
Tenant Signature (if applicable)and-		Date
General Contractor Signature		Date
	•	
Sanuel S. Paluala Is	ROPERTY OWNER/TENANT	- Parking and American Discount of the Control of t
1, Sanual S. Palundo Jr. as property owner/tenant, hereb to do the work authorized by this proposed permit on the property identification of the property i	y certify that the statements in this a fied in this Application: that all const	pplication are true; that I have legal authority
conform to the requirements of the Chicago Building Code under possible		
proposed permit does not conform to the requirements of the Chicago Bui		
stand that any false or inaccurate information contained in this Application	n may result in revocation of the buil	ding permit in addition to any other penalties
provided by law. A false statement of material fact made on this Application	•	
ing such a statement to a range of civil and criminal penalties, such as a damages incurred. In addition, persons who submit false information are		•
Owner Signature	subject to definal of the requested C	Date 8/08/08
-or- SAMUEL S. PALUMBO, Jr. President, 7	monarch Asphalt.	Co.
Owner Signature Owner Signature Or- Tenant Signature (if applicable)		Date
Does the Owner require a Residential Real Estate Developer's License to	o do the proposed work at this addre	ess? Yes No
If yes, license number		
CERTIFICATION	ON BY EXPEDITOR	
I,, as expeditor, hereby certify that the		ue. I understand that any false or inaccurate
information contained in this permit Application may result in revocation		
statement of material fact made on this Application may violate federal,	•	
a range of civil and criminal penalties, such as a period of incarceration		up to three times any damages incurred. In
addition, persons who provide false information are subject to denial of the	ne requested City action.	
Signature of Expeditor	Expeditor No.	Date
CEPTIFIC ATION BY	DESIGN PROFESSIONAL	
I. KEITH MOCKENHAUNT, as design professional, he	reby certify that all information conta	ained in this Application under item numbers
1, 2, 3A, 3B, 3C, 5, 6 and 7 is complete and accurate to the best of my kn		
Application may result in revocation of the building permit in addition to an		
Application may violate federal, state and/or local law, and may subject ar		
as a period of incarceration, fines, and an award to the City of up to three are subject to denial of the requested City action.	times any damages incurred. In ad-	dition, persons who provide false information
are subject to definal of the requested only action.		
S. Dannel M		08/10/02
- July 4 upr		
Signature of Licensed Architect of Structural Engineer of Record		Date
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091-005457		
License Number		081-00545/7 Scholal Seal
		LICENSEL LICENSEL
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WARNING TO PROPERTY OWNER/TENANT AND GENERAL CONTRACTOR

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1. Sumuch S. Palumbo	as property owner/tenant, a	and I. CH2M	HILL as qu	eneral contractor, unde	erstand that it is
against the law to exceed the scope	of a building permit. I understand	that if I build, or allow	w anyone else to build, a	any building, room addi	tion, structure or
other object that differs from, or in a	ny way exceeds, what this permit a	authorizes me to bu	ild, I can and will be se	verely punished. I un	derstand that if I
exceed, or allow anyone else to exce	,			•	
up to \$5,000.00 per day; imprisoned		=	•	=	•
pense all completed work; and, in a for providing any false or inaccurate	• • •	,	•	•	J
conform to the very in-	Chicago Building Code and it is do		and this been and that or		•
Owner Signature	Salalafe			Date 8/01	3/08
-or- SAMUELS.	ALUMBO, Jr., Prosident	, Monarch A	sphall Co.		
Tenant Signature (if applicable)				Date	
Owner Signature or- Tenant Signature (if applicable) and- General Contractor Signature	matthew D. Kl	uge, CH	am HTLL	Date	3/68
	C				
	CEDTIEIC ATION BY		ED/TENIANT		
to do the work authorized by this pi	11. as property ownermenant, her	eby certify that the s	statements in this applications: that all construction	ation are true; that I hav	e legal authority
conform to the requirements of the		• •			
proposed permit does not conform to					
stand that any false or inaccurate in	formation contained in this Applicat	tion may result in rev	vocation of the building	permit in addition to an	y other penalties
provided by law. A false statement	of material fact made on this Applic	ation may violate fe	deral, state and/or local	law, and may subject a	any person mak-
ing such a statement to a range of	•	•		• .	three times any
damages incurred. In addition, pers		•	, ,		100
Owner Signature	nBo, Jr. President,	mana a cet 1	Asahalt Co	Date _ 8 /0	0/00
Tenant Signature (if applicable)	indi, on, pregenting	77.07, 43 OC 7		Date	
Does the Owner require a Resident	ial Basi Estata Davalagaria Ligana	e to do the proposed	d work at this addraga?		
If yes, license number	·	e to do the proposet	work at this address?	res No	
	CERTIFICA as expeditor, hereby certify that t	TION BY EXPEDIT			
information contained in this permit statement of material fact made on a range of civil and criminal penalt addition, persons who provide false	this Application may violate federaties, such as a period of incarcerati	al, state and/or local ion, fines, and an av	I law, and may subject a ward to the City of up to	any person making suc	h a statement to
	•	•		Data	
Signature of Expeditor		Expeditor i	No	Date	
· // A	CERTIFICATION E	BY DESIGN PROFE	SSIONAL		
Keine Modernia	as design professional,	hereby certify that a	all information contained	in this Application und	er item numbers
1, 2, 3A, 3B, 3C, 5, 6 and 7 is com					
Application may result in revocation	J ,				
Application may violate federal, sta as a period of incarceration, fines,				-	=
are subject to denial of the request	, ,	lee tilles any damaç	ges incurred. In addition	i, persons who provide	raise information
20 000,000 10 201112/	1 11				
The Man	l			03/19/03	
Signature of Licensed Architect or	Structural Services of Bosond				
Signature of Licensed Architect or	Structural Engineer of Hecord		Da	ne Hillimminion	
081-00545	٦		Hillie	NOCKET	
License Number			Hilling.	2.000000	
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				SOPILLINA	
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9. CONTACT INFORMATION				
Owner/Tenant/Agent: Rich Usso (Sacrarnento Pance)				
Lic. #	City Chicago			
Address: 4222 South Knox Avenue	State: /L			
E-mail:	Telephone No: <u>173-585-</u>			
Emergency Contact:	Telephone No.:			
Arch./Eng.:	City:			
Address:	City:State:			
E-mail:	Telephone No:			
General Contractor: CHDM Hill Constructors, Inc. Lic. #: TGC04805	City: Englewood			
Lic. #: TG-C04805 Address: 9191 South Jamaica St.	State: Colorado			
E-mail:	Telephone No: 720-266-2	2422		
Mason Contractor:A, B, or C	C City:			
Address:	State:			
E-mail:	Telephone No:			
Electrical Contractor:	City			
Address:	City:State:			
E-mail:	Telephone No:	-		
Vent/Heat Contractor:	City			
Address:	City:State:			
E-mail:	Telephone No:			
Refrig./AC Contractor:Lic. #:	City:			
	State:			
Address:E-mail:	Telephone No:			
Plumbing Contractor:	City:			
Address:	State:			
E-mail:	Telephone No:	_ ·		
Expeditor:	City:			
Address:	City:State:			
E-mail:	Telephone No:	•		
Local Arch./Eng.*:	City			
Address:	City:State:			
E-mail:	Telephone No:	•		

(*If your licensed Architect is not located in the State of Illinois, you have the option to identify a local Illinois Architect to represent you at DOB to attend meetings and attend Open Plan Review.)

WARNING TO PROPERTY OWNER/TENANT AND GENERAL CONTRACTOR

I, Richard Lorso, as property owner/tenant, and I,	, as general contractor, understand the	hat it is
against the law to exceed the scope of a building permit. I understand that if I other object that differs from, or in any way exceeds, what this permit authorizeed, or allow anyone else to exceed, the scope of this building permit, I call	build, or allow anyone else to build, any building, room addition, struzes me to build, I can and will be severely punished. I understand	cture or that if I
up to \$5,000.00 per day; imprisoned for up to six months; required to do up t	100 hours of community service; required to tear down at my o	wn ex-
pense all completed work; and, in addition to any other penalties provided by		
for providing any false or inaccurate information in this building permit applica conform to the requirements of the Chicago Building Code and, if it does not,	,	nit must
Owner Signature		
-or-	Date ·	
Tenant Signature (if applicable)	Date	
and- General Contractor Signature	Date	
CERTIFICATION BY PROP	ERTY OWNER/TENANT	
I. アバートに しいても as property owner/tenant, hereby ce	tify that the statements in this application are true; that I have legal a	uthority
to do the work authorized by this proposed permit on the property identified		
conform to the requirements of the Chicago Building Code under possible per		
proposed permit does not conform to the requirements of the Chicago Building stand that any false or inaccurate information contained in this Application may	•	
provided by law. A false statement of material fact made on this Application r		
ing such a statement to a range of civil and criminal penalties, such as a per		
damages incurred. In addition, persons who submit false information are sub-		
Owner Signature	Date 8-3-69	<u>`</u>
-or-		
Tenant Signature (if applicable)	Date	
Does the Owner require a Residential Real Estate Developer's License to do ves, license number	the proposed work at this address? Yes No	
CERTIFICATION	DV EVDEDITOD	
CERTIFICATION I as expeditor, hereby certify that the state	ements in this Application are true. I understand that any false or ina	ccurate
information contained in this permit Application may result in revocation of the		
statement of material fact made on this Application may violate federal, state	and/or local law, and may subject any person making such a state	ment to
a range of civil and criminal penalties, such as a period of incarceration, fin	• •	ırred. İn
addition, persons who provide false information are subject to denial of the re-	quested City action.	
Signature of Expeditor	Expeditor No Date	
CERTIFICATION BY DES	IGN PROFESSIONAL	
CERTIFICATION BY DES	certify that all information contained in this Application under item n	umbers
1, 2, 3A, 3B, 3C, 5, 6 and 7 is complete and accurate to the best of my know	edge. I understand that any false or inaccurate information containe	d in this
Application may result in revocation of the building permit in addition to any ot		
Application may violate federal, state and/or local law, and may subject any po	-	
as a period of incarceration, fines, and an award to the City of up to three time are subject to denial of the requested City action.	s any damages incurred. In addition, persons who provide false into	rmation
In much fl	80/01/60	
Signature of Licensed Architect or Structural Engineer of Record		
031-005457		
License Number	081-005457	\
	LICENSED Properties	1)
	STRUCTURAL :	/
	ENGINEER	•

WARNING TO PROPERTY OWNER/TENANT AND GENERAL CONTRACTOR

1. Richard UKS . as pro	operly owner/tenant, and I,	CH2M HILL as	general contractor, understand that it is
against the law to exceed the scope of a building			
other object that differs from, or in any way exce	•		• •
exceed, or allow anyone else to exceed, the scop up to \$5,000.00 per day; imprisoned for up to six	•	* *	• •
pense all completed work; and, in addition to any		· · · · · · · · · · · · · · · · · · ·	
for providing any talse or inaccurate information is		•	•
conform to the requirements of the Chicago Build			
Owner Signature			Date
-or- Tenant Signature (if applicable)			Date
and- General Contractor Signature	thur D. Kluge ,	CHAM HTW	Date
	V		
Duckey War	CERTIFICATION BY PROP	ERTY OWNER/TENANT	
to do the work authorized by this proposed perm	erty owner/tenant, hereby ce nit on the property identified	nity that the statements in this appli in this Application: that all construct	tion work under this proposed permit will
conform to the requirements of the Chicago Buil	,		
proposed permit does not conform to the requirer	•		
stand that any false or inaccurate information co			
provided by law. A false statement of material fa			
ing such a statement to a range of civil and crim damages incurred. In addition, persons who sub	·		
Owner Signature		sport to domar or the requested only	Date
-or-			Jake
Tenant Signature (if applicable)			Date
Does the Owner require a Residential Real Esta If yes, license number	•	• •	
	CERTIFICATION I	BY EXPEDITOR	
			I understand that any false or inaccurate
information contained in this permit Application			
statement of material fact made on this Applicat a range of civil and criminal penalties, such as			
addition, persons who provide false information			to thee times any damages medired.
,	,	•	
Signature of Expeditor		Expeditor No	Date
V	CERTIFICATION BY DES	SIGN PROFESSIONAL	
1 Kerry Mockennapr as	s design professional, hereby	y certify that all information contains	ed in this Application under item numbers
1, 2, 3A, 3B, 3C, 5, 6 and 7 is complete and acc	curate to the best of my know	ledge. I understand that any false of	or inaccurate information contained in this
Application may result in revocation of the building	•		
Application may violate federal, state and/or local	, , , , , , , , , , , , , , , , , , , ,	3	
as a period of incarceration, fines, and an award are subject to denial of the requested City action		es any damages incurred. In addition	on, persons who provide talse information
are subject to demay of the requested City action			
V / and I		•	08/19/09
Signature of Licensed Architect or Structural En	unineer of Record		Date
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031-005457		Millian DACC	KENIM.
License Number		111120000	
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Property address 3031 South Albany Ave. Chicago, 12 60623 App. #:

I. NOTICE AND POSTING REQUIREMENTS

At least 30 days prior to beginning the excavation work, the owner or the property where the work is to be done shall notify the owners of adjacent properties of the anticipated starting date and three-dimensional measurement of the excavation work. The notice shall be in writing, and shall be delivered by certified mail, return receipt requested, or by personal delivery to the person entitled to receive the notice, accompanied by a receipt for delivery. The receipt and a copy of the notice shall be available for inspection at the excavation site.

This form, signed and sealed by the design professional, shall be available at the project site. Seventy-two hours prior to excavation, Department of Buildings shall be notified at 312/744-3400.

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The excavator must have an appropriate license from the City of Chicago and maintain a comprehensive liability insurance policy of \$1,000,000 per occurrence.

(Provide following information and attach certificate of insurance.)

Excavator name: (H2MHill (custructors, Dnc License #: TGC04805	
----------------------------------------------------------------	--

I, *the owner*, hereby attest that the foregoing information is true and correct to the best of my knowledge and belief.

	Sullalulof 321 Cen	HerStreet Hillside	_/IL	1 60162
\rightarrow	(Owner signature) (Street add	ress) (City)	(State)	(Zip)
_	(Owner signature) (Street addition SAMUEL 3. PALUMBO, Jr., President.	monarch Asphalt Co.		

III. DESIGN PROFESSIONAL CERTIFICATION

In the opinion of an Illinois licensed architect or structural/professional engineer.

does this project require any reinforcement or bracing of the adjacent property?

(If yes, the rules require that an architect or engineer be responsible for designing such system and obtaining any necessary permit.)

I, the design professional, hereby attest that the foregoing information in paragraph III is true and correct texthe best of my knowledge and belief.

Architect/Engineer signature) (Street address) (City) (State) (Zip)

City of Chicago Richard M. Daley, Mayor

196449-19-EL-11/07

Yes

Property address 2800 S. Sacramento Ave., Chizago, IL App. #:

NOTICE AND POSTING REQUIREMENTS ١.

At least 30 days prior to beginning the excavation work, the owner or the property where the work is to be done shall notify the owners of adjacent properties of the anticipated starting date and three-dimensional measurement of the excavation work. The notice shall be in writing, and shall be delivered by certified mail, return receipt requested, or by personal delivery to the person entitled to receive the notice, accompanied by a receipt for delivery. The receipt and a copy of the notice shall be available for inspection at the excavation site.

This form, signed and sealed by the design professional, shall be available at the project site. Seventy-two hours prior to excavation, Department of Buildings shall be notified at 312/744-3400.

11. INSURANCE

The excavator must have an appropriate license from the City of Chicago and maintain a comprehensive liability insurance policy of \$1,000,000 per occurrence.

(Provide following information and attach certificate of insurance.)

Excavator name: CH2MHII Constructors, Inc. License #: TGC0 4805

I, the owner, hereby attest that the foregoing information is true and correct to the best of my knowledge and belief.

(Owner signature)

DESIGN PROFESSIONAL CERTIFICATION

In the opinion of an Illinois licensed architect or structural/professional engineer, does this project require any reinforcement or bracing of the adjacent property? (If yes, the rules require that an architect or engineer be responsible for designing such system and obtaining any necessary permit.)

Yes

No

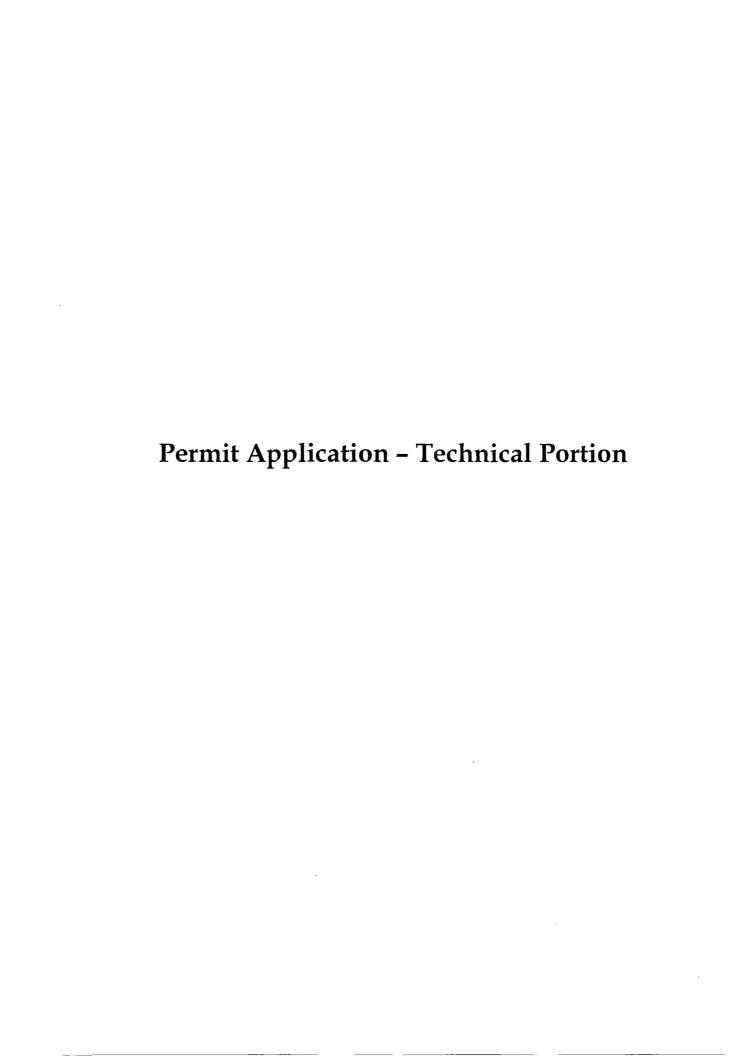
I, the design professional, hereby attest that the foregoing information in paragraph III is true and correct to the best of my knowledge and belief.

(Architect/Engineer signature)

(Street address)

City of Chicago Richard M. Daley, Mayor

196449-19-EL-11/07



Stormwater Permit Application

PREPARED FOR: The Department of Buildings

Sewer Permit Section - City Hall 121 North LaSalle Street, Suite 804

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DATE: August 13, 2008

CC: The Wetlands Initiative: c/o Jill Kostel

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Honeywell International Inc: c/o Chuck Geadelmann, Bill Hague

1.0 Introduction

This technical memorandum, and associated tables and attachments, constitutes the stormwater permit application for the former Celotex Main Site. The objective of this application is to obtain a stormwater permit for a re-grading and capping project at the 2800 South Sacramento Avenue property. The purpose of the project is to place a cover of clean material over the former industrial site to support future use. The project is being conducted by Honeywell International Inc (Honeywell) under directive of USEPA. The project site is not currently owned by Honeywell, but was in the past and they are the responsible party for this work.

The project site is a 21.6 acre former industrial site known as the Celotex site located at 2800 South Sacramento Avenue, Chicago, IL. The site is subdivided into two parcels with two different owners. The larger parcel (approximately 20 acres), located to the north, is referred to as the Sacramento parcel, while the smaller parcel (approximately 2 acres), located to the south (3031 South Albany Avenue) is referred to as the Monarch parcel. The Sacramento parcel currently serves as a compacted gravel parking lot for semi trucks and trailers. The Monarch parcel is currently vacant with a compacted gravel surface.

The main goal of this project is to place a cover of clean material over the Sacramento and Monarch parcels to meet USEPA requirements. Additionally, the City of Chicago Parks Department is attempting to purchase these two parcels to convert them into a park. To meet USEPA requirements, clean material will be added to each parcel so that a 24 inch layer separates the surface from potentially impacted materials. The type of clean material will vary depending upon the location and will include vegetated topsoil and aggregate covers.

The Sacramento parcel's ultimate land use is in question pending the outcome of the City of Chicago Parks Department's efforts to purchase the properties. The construction plan allows for two options for the Sacramento parcel. The first is to have the Sacramento parcel cover material be gravel, similar to what currently exists. The second option is for the Sacramento



parcel cover to be soil and grass. The Monarch parcel is planned to be a parking lot. The Parks Department may install porous pavement in the parking area in the future. This project will lay the base aggregate for a future porous pavement system. An analysis of each of these options has been included to demonstrate the stormwater requirements have been met with either option.

The Sacramento parcel has two drainage catchment areas (1 north and 1 south) in addition to side slope drainage (Attachment 1). The Monarch parcel has one catchment area of 1.6 acres in addition to side slope drainage under proposed conditions. The northern Sacramento catchment is approximately 3.2 acres while the southern catchment is approximately 13.3 acres. The Sacramento parcel has approximately 3.1 acres of side slopes that drain to areas other than the Monarch parcel. Except for the northern and western side slopes of the site, the northern catchment currently drains to the Whipple Street sewer (owned by City of Chicago) to the east of the site. Except for the site side slopes, the southern catchment currently drains to the same sewer as the Monarch catch basin and all flow drains from that point west to the Albany Avenue sewer (owned by the City of Chicago). Under existing conditions, side slopes drain to adjacent properties or rights of way for storms when the perimeter swale overtops.

2.0 Stormwater Project Overview

2.1 Design Intention

The project will abandon existing stormwater pipes on both parcels and install new pipes to direct stormwater to the combined sewer overflow (CSO) outfall #178 to the Collateral channel south of the Monarch parcel. New stormwater pipes will discharge to outfall #178 just downstream of the tide gate (see drawings in Attachment 2). Except for side slope drainage that does not have catch basins, the project will remove all stormwater from the project site from the City's combined sewer system. Existing discharge rates will be met as much as possible to create no negative impact upon the sewer system. Removing the water from the combined sewer system should lead to increased sewer capacity to convey flows upstream of the tide gate near CSO outfall #178.

2.2 Modeling Approach

Because of the large size of the site and potential complexity of calculating flow rates, storage, and combining the drainage from the northern end of Sacramento (Subarea 2) with the flows from Sacramento Subarea 1 and Monarch, the site has been modeled with HEC-HMS. Total area modeled through HEC-HMS is 21.6 acres.

2.3 Rate Control

Restrictors will be placed in each of 6 new catch basins to provide rate control and onsite storage (see drawings in Attachment 2 for restrictor sizes and locations). The maximum release rate from the project site to the constructed wetland will be 10.3 cfs (0.48 cfs/acre) or less for the 100-year return period storm (see attached restrictor calculations in Attachment 3). This release rate meets the City's maximum release rate of 1 cfs/acre for sites discharging to waterways as well as the maximum release rate of 0.75 cfs/acre from open areas conducive to ponding. The maximum release rate from the project site from perimeter



swales not adjacent to street right of way ranges from zero from the 2-year event to 3.0 cfs from the 100-year event. These overflow rates along with the release rate of 10.3 cfs is less than the existing maximum release rate from the site of 19.0 cfs when the discharge to Albany and Whipple are combined.

3.0 Existing Condition

3.1 Land Use

The Sacramento and Monarch parcels are currently covered with compacted gravel. The Sacramento parcel is utilized as a parking area for semi trucks and trailers. The Monarch parcel is currently vacant with compacted gravel. The SCS Curve Number method was used to determine runoff numbers and the TR-55 method was used to determine time of concentration. A minimum value of no less than 6 minutes (0.1 hours) was used for time of concentration, following TR-55 guidance. Table 1 below summarizes these values for each subarea.

TABLE 1
Existing Conditions Land Use

Drainage Area	Curve Number	Time of concentration (min)	Area (acres)
Sacramento Subarea 1	89	10	13.3
Sacramento Subarea 2	89	8	3.2
Monarch	89	6	2.0
SS1	78	6	0.409
SS2	78	6	0.961
SS3N	78	6	0.279
SS3S	78	6	0.317
SS4N	78	6	0.371
SS4S	78	6	0.336
SS5	78	6	0.187
SS8	78	6	0.257

SS = Side slopes.

3.2 Drainage Areas

The following distinct drainage areas exist on the project site.

- 1. Sacramento subarea 1 (13.3 acres) Drains to Albany Avenue Sewer
- 2. Sacramento subarea 2 (3.2 acres) Drains east to Whipple Street Sewer
- 3. Monarch (2.0 acres) Drains to Albany Avenue Sewer

4. Sacramento side slopes (3.1 acres) – Drains to grassed swales and then offsite in various directions when the swales overflow

Total Project Site Area: 21.6 acres

Three general flow paths exist for the site, as shown in the modeling schematics in Attachment 3. Flow leaves north and east of the site both through drainage through a stormsewer inlet as well as when the existing swale overflows.

3.3 Flow Rates

Flow rates were analyzed for Sacramento subarea 1, subarea 2, and Sacramento side slopes as well as Monarch using HEC-HMS running a Huff distribution for precipitation values in Bulletin 70. Storms for the 2-, 10-, 50-, and 100-year return period events over durations of 1-, 3-, 6-, 12-, and 24-hours were analyzed. Input, output, and model schematics are shown in Attachment 3. Restrictions, such as pipe size and slope that could reduce runoff rates from the site were considered along with ponding that could occur at the Sacramento parcel inlets. The existing condition runoff results are shown in Table 2 and Table 3.

Under existing conditions, the side slopes have some small storage capability from a ditch that runs along the perimeter of portions of the site. Once the ditch fills with runoff and overtops, the water runs off onto neighboring properties, including: street rights-of-way, private property, and alley rights-of-way. The runoff from these areas was modeled with HEC-HMS and while some infiltration will occur, for modeling purposes zero infiltration was assumed to be conservative. The major difference between existing and proposed conditions is a larger swale is being constructed under proposed conditions. Under most storm conditions, according to the results in Tables 2 and 3, no overtopping of the swales will occur. While there is some variation of the existing ditch around the site perimeter, the average condition is approximately represented by a two foot wide ditch, one foot deep with 2:1 side slopes.

Under existing conditions, the side slope swales start to overflow for the 10-, 50-, or 100-year storm depending upon the storm duration. Side slope swale calculations assumed a typical swale cross section to determine if overflow would occur. The peak flow rate estimated to leave the site through swale overflow under existing conditions is 4.2 cfs.

Ponding depths include:

- Zero to 2.8 feet between the 2- and 100-year storms in Subarea 1 on Sacramento (south)
- Zero to 2.3 feet between the 2- and 100-year storms for Subarea 2 on Sacramento (north)

TABLE 2
Existing Conditions Peak Flow Rate (cfs)
Former Celotex Main Site

		1 Hou	ır Duratio	n		3 Hou	ır Duratio	n		6 Hou	ır Duratio	n		12 Ho	ur Duratio	on	24 Hour Duration			
Area	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year												
To Albany Avenue Sewer (South West of site)	10.0	10.4	14.4	16.8	10.2	10.1	11.8	13.0	9.0	10.2	10.2	11.1	5.7	9.8	10.2	10.2	3.5	5.9	9.2	10.2
To Whipple Street Sewer through Catch Basin (NE of site)	1.0	1.1	1.1	1.1	1.0	1.1	1.1	1.1	1.0	1.1	1.1	1.1	1.0	1.0	1.1	1.1	0.7	1.0	1.1	1.1
To Whipple Street through Direct Runoff (NE of site side swale overflow)	0.0	0.0	0.0	1.1	0.0	0.0	1.3	2.3	0.0	0.0	1.2	2.1	0.0	0.2	1.1	1.5	0.0	0.2	0.7	0.9
Direct Runoff to South West of Site (side swale runoff)	0.0	0.0	0.0	0.9	0.0	0.0	0.9	1.9	0.0	0.1	0.9	1.8	0.0	0.2	1.0	1.6	0.0	0.2	0.8	0.9
Precip (inches)	1.43	2.1	3.04	3.56	1.94	2.86	4.14	4.85	2.28	3.35	4.85	5.68	2.64	3.89	5.62	6.59	3.04	4.47	6.46	7.58

TABLE 3
Existing Conditions Peak Ponding Elevation
Former Celotex Main Site

		1 Hour Duration				3 Hour Duration			6 Hour Duration				12 Hour Duration				24 Hour Duration			
Area	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year
Existing																				
Subarea1	596.1	596.7	597.2	597.4	596.1	596.7	597.3	597.6	593.5	596.5	597.2	597.5	591.1	594.3	596.9	597.2	590.2	591.2	593.7	596.5
Subarea 2	597.3	597.9	598.2	598.3	597.4	598.0	598.3	598.5	597.2	598.0	598.3	598.5	597.0	597.6	598.2	598.4	594.8	597.1	598.0	598.2
Monarch											n/a								-	
Precip (inches)	1.43	2.1	3.04	3.56	1.94	2.86	4.14	4.85	2.28	3.35	4.85	5.68	2.64	3.89	5.62	6.59	3.04	4.47	6.46	7.58

Note: side slope swale peak overflow is estimated at 4.2 cfs.

4.0 Proposed Condition Sacramento Gravel Cover Alternative

4.1 Land Use

Under this base alternative, the Sacramento subareas 1 and 2 will be covered with gravel. The Monarch parcel will be covered with aggregate for a porous pavement parking lot. The Monarch parcel has side slopes and grass swales under proposed conditions. As reflected by the curve number values, the land use is essentially the same as existing conditions, except Monarch is to be paved in the future. Table 4 below summarizes these parameters.

TABLE 4
Proposed Conditions Land Use (Gravel Surface Option)

Drainage Area	Curve Number	Time of concentration (min)	Area (acres)
Subarea 1	89	10	13.3
Subarea 2	89	8	3.2
Monarch	98	6	1.6
SS1	78	6	0.409
SS2	78	6	0.961
SS3N	78	6	0.279
SS3S	78	6	0.317
SS4N	78	6	0.371
SS4S	78	6	0.336
SS5	78	6	0.187
SS6 (Monarch)	78	6	0.257
SS7 (Monarch)	78	6	0.129
SS8	78	6	0.257

SS = Side slopes.

4.2 Drainage Areas

Under proposed conditions, Monarch as well as Sacramento Subarea 1, Subarea 2, and several side slopes (SS4, SS7, and SS8) are included together and connected to the CSO Outfall #178 downstream of the tide gate. This reduces flow to the combined sewer system and provides wetland treatment of the runoff from the site surface. Other side slopes that are adjacent to public right of way eventually fill up and overflow. Side slope SS1, however, is adjacent to private property and includes an enlarged swale to improve conditions from what currently exists and holds the runoff from a 100-year return period storm. SS1 was evaluated to also be connected to Outfall #178, but this was not feasible. It was not feasible to connect to Outfall #178 because it would have required lowering the enter sewer profile

and would have resulted in clearance conflicts at the downstream end (see drawings in Appendix 4) Consequently, side slope SS4 was enlarged to contain the 100-year runoff.

There are 8 distinct drainage areas on the project site with drainage as identified below

- 1. Sacramento subarea 1 (13.3 acres) Drains to Outfall #178
- 2. Sacramento side slope (SS1 0.409 acres) Drains to enlarged grassed swale and infiltrates or evaporates
- 3. Sacramento side slopes (SS4, SS8 0.964 acres) Drains to Outfall #178
- 4. Sacramento side slopes (SS2, SS3, and SS5 1.744 acres) Contained within enlarged grass swale for small events and overtops for larger events to public right of way
- 5. Sacramento subarea 2 (3.2 acres) Drains to Outfall #178
- 6. Monarch (1.6 acres) Drains to Outfall #178
- 7. Monarch side slope (SS6 0.257 acres) Contained within enlarged grass swale for small events and overtops for larger events to public right of way
- 8. Monarch side slope (SS7 0.129 acres) Drains to Outfall #178

4.3 Flow Rates

Flow rates were again analyzed using HEC-HMS. Restrictions on runoff were designed to limit the runoff to at or below existing conditions whenever practical. Restrictions cause ponding in the porous pavement or on the ground surface. The major difference between existing and proposed conditions is a larger swale is being constructed under proposed conditions. Under the 2-year and smaller storm conditions, no runoff beyond the swales will occur. The maximum total runoff to right of way from the swales is 3.0 cfs. The proposed condition runoff results are shown in Table 5 and Table 6 below.

TABLE 5
Proposed Conditions Peak Flow Rate (cfs) (Gravel Surface Option) (SubArea 1 - 9" restriction, Subarea 2- 4" restriction, Monarch - 6" restrictor, SS4, SS7, and SS8 all have 6" restrictors)
Former Celotex Site

		1 Ho	ur Duratio	on		3 Ho	ur Duratio	n		6 Ho	ur Duratio	n		12 Ho	ur Duratio	on	24 Hour Duration				
Area	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year													
To Outfall #178 (SW of site)	8.5	9.1	10.0	10.3	8.5	9.2	10.0	10.3	7.8	9.0	9.8	10.1	6.9	8.1	9.4	9.7	4.4	7.0	8.2	8.7	
To Whipple Street through Direct Runoff (NE of site side swale overflow)	0.0	0.0	0.0	0.0	0.0	0.0	0.6	1.6	0.0	0.0	0.9	1.5	0.0	0.2	0.8	1.4	0.0	0.1	0.7	0.9	
Direct Runoff to South West of Site (side swale runoff)	0.0	0.0	0.6	0.9	0.0	0.1	0.8	1.4	0.0	0.1	0.6	0.8	0.0	0.2	0.4	0.6	0.0	0.1	0.2	0.3	
Precip (inches)	1.43	2.1	3.04	3.56	1.94	2.86	4.14	4.85	2.28	3.35	4.85	5.68	2.64	3.89	5.62	6.59	3.04	4.47	6.46	7.58	

TABLE 6
Proposed Peak Ponding Elevation (Gravel Surface Option)
Former Celotex Site

		r Duration 6 Hour Duration						12 Ho	ur Duratio	24 Hour Duration										
Area	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year
Subarea1	597.1	597.8	598.3	598.5	597.1	597.9	598.4	598.7	596.9	597.6	598.3	598.6	595.7	597.2	598.1	598.4	592.5	595.8	597.4	597.9
Subarea 2	598.3	598.9	599.2	599.3	598.4	599.0	599.3	599.5	598.2	598.9	599.3	599.5	598.0	598.6	599.2	599.4	595.4	598.1	598.9	599.1
Monarch	592.4	592.6	592.8	592.9	592.3	592.5	592.7	592.8	591.3	592.3	592.5	592.6	590.1	590.9	592.3	592.4	589.7	590.0	590.4	590.9
Precip (inches)	1.43	2.1	3.04	3.56	1.94	2.86	4.14	4.85	2.28	3.35	4.85	5.68	2.64	3.89	5.62	6.59	3.04	4.47	6.46	7.58

4.4 Rate Control

Table 2 shows that the existing peak flow rate to the Albany Avenue sewer for any storm is 16.8 cfs, while the peak flow rate to the Whipple Street sewer to the east is 1.1 cfs. Under proposed conditions there is no direct flow to either of these sewers because connections to those sewers will be abandoned in lieu of a connection to Outfall #178. The peak flow rate to Outfall #178 for any storm from the project site under proposed conditions is 10.3 cfs (Table 5).

Under existing conditions 16.8 cfs from the site would flow to the Albany diversion structure under peak flow conditions. Changing the flow to downstream of the tide gate on Outfall #178 reduces flow at the Albany diversion structure, reduces flow at the tide gate diversion structure, and reduces flow going through the tide gate. The peak flow for the 100-year storm going to Outfall #178 under proposed conditions is also only 61% of the peak flow leaving the site through the Monarch parcel under existing conditions. Ponding draws down in less than 72 hours. Porous pavement drains within 48 hours. Ponding information is shown in Attachment 4.

Ponding depths include:

- Zero to 2.9 feet between the 2- and 100-year storms in Subarea 1 on Sacramento (south)
- Zero to 2.3 feet between the 2- and 100-year storms for Subarea 2 on Sacramento (north)
- Zero on Monarch (never surcharges to within eight inches of catch basin because of porous pavement underdrains); if Monarch does not have porous pavement installed, the estimated ponding depth is 1.0 feet
- Zero to 1.4 feet between the 2- and 100-year storms for Sacramento side slope SS1
- Zero to 0.6 feet between the 2- and 100-year storms for Sacramento side slope SS4
- Zero to 0.4 feet between the 2- and 100-year storms for Sacramento side slope SS7
- The Sacramento side slope area SS1 has been designed to have a larger cross-sectional area than the other side slope areas.

Details of the side slope swales and other design aspects can be seen on the drawings in Attachment 4.

4.5 Volume Control

The project site is exempt from infiltration requirements as it is a contaminated former industrial site. (See 4.1.2 Infiltration Exception of DWM Regulations for Sewer Construction and Stormwater Management).

However, the project plan has included the potential for some volume control by planning for the possibility of porous pavement being utilized on the Monarch parcel.

4.6 Stormwater Quality

Stormwater quality benefits achieved by this project include:

- Filtration of stormwater by porous pavement on the Monarch parcel (the Parks Department may install porous pavement in the future)
- All stormwater will flow to a grassed swale or treatment wetland in the Collateral Channel

Currently, MWRDGC (Joe Schuessler) is working with The Wetland Initiative (TWI – Jill Kostel) to implement a constructed wetland (approximately 1 acre) in the northern portion of the Collateral Channel. We have been in contact with both Joe Schuessler and Jill Kostel about our project and are in agreement, in principle, on sending the stormwater to the treatment wetland. MWRDGC has also been contacted regarding the project.

5.0 Proposed Condition Sacramento Grass Cover Option

5.1 Land Use

Under this second option, the Sacramento subareas 1 and 2 will be covered with soil and grass. The Monarch parcel will be covered with aggregate for a porous pavement parking lot. As reflected by the curve number values, the amount of impervious area is significantly reduced under proposed conditions. Table 7 below summarizes these parameters.

TABLE 7Proposed Conditions Land Use (Grassed Surface Option)

Drainage Area	Curve Number	Time of concentration (min)	Area (acres)
Sacramento Subarea 1	78	41	13.3
Sacramento Subarea 2	78	41	3.2
Monarch	98	6	1.6
SS1	78	6	0.409
SS2	78	6	0.961
SS3N	78	6	0.279
SS3S	78	6	0.317
SS4N	78	6	0.371
SS4S	78	6	0.336
SS5	78	6	0.187
SS6 (Monarch)	78	6	0.257
SS7 (Monarch)	78	6	0.129
SS8	78	6	0.257

TABLE 7Proposed Conditions Land Use (Grassed Surface Option)

Drainage Area	Curve Number	Time of concentration (min)	Area (acres)
Sacramento Subarea 1	78	41	13.3
Sacramento Subarea 2	78	41	3.2
Monarch	98	6	1.6
SS1	78	6	0.409
SS2	78	6	0.961
SS3N	78	6	0.279
SS3S	78	6	0.317
SS4N	78	6	0.371
SS4S	78	6	0.336
SS5	78	6	0.187
SS6 (Monarch)	78	6	0.257
SS7 (Monarch)	78	6	0.129
SS8	78	6	0.257

SS= Side slopes.

5.2 Drainage Areas

The drainage areas and directions are the same as under the gravel surface option.

5.3 Flow Rates

Flow rates were again analyzed using HEC-HMS. Restrictions on runoff were designed to limit the runoff to at or below existing conditions whenever practical. Restrictions cause ponding in the porous pavement or on the ground surface. The major difference between existing and proposed conditions is a larger swale is being constructed under proposed conditions. Under the 2-year and smaller storm conditions, no runoff beyond the swales will occur. The maximum total runoff to right of way from the swales is 3.0 cfs. The proposed condition runoff results are shown in Table 8 and Table 9 below.

TABLE8
Proposed Conditions Peak Flow Rate (Grassed Surface Option) (SubArea 1 - 9" restriction, Subarea 2- 4" restriction, Monarch - 6" restrictor; Side Slopes SS4, SS7, and SS8 have 6" restrictors)
Former Celotex Site

		1 Ho	ur Duratio	n .		3 Hou	ur Duratio	n		6 Ho	ur Duratio	n		12 Ho	ur Duratio	on	24 Hour Duration			
Area	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year												
To Outfall #178 (SW of site)	6.1	8.6	9.5	9.8	6.7	8.8	9.7	10.1	5.5	8.6	9.5	9.9	4.2	7.5	9.1	9.5	2.9	5.4	7.9	8.4
To Whipple Street through Direct Runoff (NE of site side swale overflow)	0.0	0.0	0.0	0.0	0.0	0.0	0.6	1.6	0.0	0.0	0.9	1.5	0.0	0.2	0.8	1.4	0.0	0.1	0.7	0.9
Direct Runoff to South West of Site (side swale runoff)	0.0	0.0	0.6	0.9	0.0	0.1	0.8	1.4	0.0	0.1	0.6	0.8	0.0	0.2	0.4	0.6	0.0	0.1	0.2	0.3
Precip (inches)	1.43	2.1	3.04	3.56	1.94	2.86	4.14	4.85	2.28	3.35	4.85	5.68	2.64	3.89	5.62	6.59	3.04	4.47	6.46	7.58

TABLE 9
Proposed Conditions Peak Ponding Elevation (Grassed Surface Option)
Former Celotex Site

		1 Hour Duration				3 Hour Duration				6 Hou	r Duratio	n	12 Hour Duration				24 Hour Duration			
Area	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year	2- year	10- year	50- year	100- year
Subarea1	593.2	596.8	597.6	598.0	594.2	597.1	598.0	598.2	593.4	597.0	597.7	598.2	592.1	596.0	597.5	598.0	591.4	593.4	596.9	597.4
Subarea 2	596.3	598.2	598.8	599.0	597.3	598.3	599.1	599.2	596.6	598.3	599.1	599.2	594.8	598.1	598.9	599.1	593.6	596.6	598.4	598.9
Monarch	592.4	592.6	592.8	592.9	592.3	592.5	592.7	592.8	591.3	592.3	592.5	592.6	590.1	590.9	592.3	592.4	589.7	590.0	590.4	590.9
Precip (inches)	1.43	2.1	3.04	3.56	1.94	2.86	4.14	4.85	2.28	3.35	4.85	5.68	2.64	3.89	5.62	6.59	3.04	4.47	6.46	7.58

5.4 Rate Control

Table 2 shows that the existing peak flow rate to the Albany Avenue sewer for any storm is 16.8 cfs, while the peak flow rate to the Whipple Street sewer to the east is 1.1 cfs. Under proposed conditions there is no direct flow to either of these sewers because connections to those sewers will be abandoned in lieu of a connection to Outfall #178. The peak flow rate to Outfall #178 for any storm from the project site under proposed conditions is 10.1 cfs (Table 8).

Under existing conditions 16.8 cfs from the site would flow to the Albany diversion structure diversion structure under peak flow conditions. Changing the flow to downstream of the tide gate on Outfall #178 reduces flow at the Albany diversion structure, reduces flow at the tide gate diversion structure, and reduces flow going through the tide gate. The peak flow for the 100-year storm going to Outfall #178 under proposed conditions is also only 60% of the flow leaving the site through the Monarch parcel under existing conditions. Proposed conditions will also result in less ponding area as compared with existing conditions (Attachment 4). Porous pavement drains within 48 hours. Ponding draws down in less than 72 hours.

Ponding depths include:

- Zero to 2.4 feet between the 2- and 100-year storms for Subarea 1 on Sacramento (south)
- Zero to 2.0 feet between the 2- and 100-year storms for Subarea 2 on Sacramento (north)
- Zero on Monarch (never surcharges within eight inches of catch basin because of porous pavement underdrains); if Monarch does not have porous pavement installed, the estimated ponding depth is 1.0 feet
- 0.1 feet to 1.4 feet between the 2- and 100-year storms for Sacramento side slope SS1, with a minimum 0.1 feet of freeboard
- 0.1 feet to 0.6 feet between the 2- and 100-year storms for Sacramento side slope SS4, with a minimum 0.4 feet of freeboard
- Zero to 0.4 feet between the 2- and 100-year storms for Sacramento side slope SS7, with a minimum 0.6 feet of freeboard.

The Sacramento side slope area SS1 has been designed to have a larger cross-sectional area than the other side slope areas. Details of the side slope swales and other design aspects can be seen on the drawings in Attachment 4.

5.5 Volume Control

The project site is exempt from infiltration requirements as it is a contaminated former industrial site. (See 4.1.2 Infiltration Exception of DWM Regulations for Sewer Construction and Stormwater Management).

However, the project plan with the end use as a park will still provide volume control by reducing the impervious area by more than 15%. The proposed Sacramento parcel conditions will have no impervious area. Soil and grass will be placed on the Sacramento parcel, where compacted gravel currently exists. The project plan has included the potential

for some volume control by planning for the possibility of porous pavement being utilized on the Monarch parcel.

5.6 Stormwater Quality

Stormwater quality benefits achieved by this project include:

- Replacement of existing compacted gravel surface with grassy surface
- Filtration of stormwater by porous pavement on the Monarch parcel (the Parks Department may install porous pavement in the future)
- All stormwater will flow to a grassed swale or treatment wetland in the Collateral Channel

Currently, MWRDGC (Joe Schuessler) is working with The Wetland Initiative (TWI – Jill Kostel) to implement a constructed wetland (approximately 1 acre) in the northern portion of the Collateral Channel. We have been in contact with both Joe Schuessler and Jill Kostel about our project and are in agreement, in principle, on sending the stormwater to the treatment wetland. The city of Chicago Department of Water Management (DWM) has also been contacted regarding the project.

6.0 Construction Plans

6.1 Construction Details and Standards

Standard DWM details have been used for sewers and manholes as shown in the attached drawings (Attachment 4) with several exceptions as follows:

- For very shallow cover or deep pipe cover where the clay pipe properties are not strong enough for the loads, Illinois Department of Transportation (IDOT) recommendations for reinforced concrete pipe were used.
- For sewer runs with depths greater than 10 feet, reinforced concrete pipe was used instead of clay pipe following IDOT recommendations.
- Half-traps were originally excluded in the original design because the connection is not
 to the combined sewer system because the stormsewer connects downstream of the
 CSO tide gate which flows to the Collateral channel. However, half-traps were added
 back in (see Modification #1 in Attachment 4) to minimize clogging of the restrictors.
- Drop manholes were not used in the original design because the new connection to the wetland does not contain any sanitary flow enabling easy maintenance during dry weather conditions and the drop is relatively low at between two and three feet. However, a pre-cast concrete drop manhole has been added back in for Manhole 1 and the drops at Manhole 3 have been lowered to be less than 2 feet by adjusting pipe slopes. See Modification #1 in Attachment 4.
- The outfall to the CSO pipe has standing water making a drop manhole to minimize scour unnecessary.

• The separation between the new stormsewer and the existing CSO outfall pipe is less than 18 inches (approximately 75 feet upstream of Manhole 1), however the stormsewer pipe has been designed to be as high as possible in order to maximize the separation between pipes by using minimum pipe slopes and minimizing drops at manholes.

The pavement on the Monarch parcel will be implemented by the Parks Department. The area has been designed so that permeable pavement could be installed by providing 24 inches of IDOT CA-1 specification aggregate. Underdrains to draw down the water are also provided in advance of the pavement that will be placed on the Monarch parcel. Should the Parks department choose to place impervious pavement on the site, ponding would occur greater than 10 inches on the Monarch parcel.

6.2 Sediment and Erosion Control Plan

A sediment and erosion control plan, in the form of a stormwater pollution prevention plan (SWPPP), is required by the State of Illinois because the site disturbs more then 1 acre. The plan showing the location of sediment and erosion control best management practices (BMPs) is provided here as Attachment 5. Areas to be vegetated are shown in the details.

The project will comply with all NPDES requirements for construction activities and a copy of the SWPPP, Notice of Intent (NOI), and permit will be kept on site during construction and made available upon request from DOE or DWM personnel.

6.3 Operation and Maintenance Plan

The operation and maintenance plan (O&M Plan) for the site is described. There are no structures on the property; consequently, the plan cannot be kept on-site after construction activities are completed. During construction, the plan will be kept at the construction manager's office.

Contact Information

During the construction phase, the contact information will be different from the post-construction phase.

Construction Phase Contact Information:

Alan Jones CH2M HILL 135 South 84th Street, Suite 325 Milwaukee, WI 53214 (414) 272-2426

Post-Construction Phase Contact Information:

While not the property owner, Honeywell is responsible for the construction at the site. Consequently, Honeywell will inform the owners of the O&M responsibilities. Current property owner contacts are as follows:

- Rich Urso, Sacramento parcel
- Samuel Palumbo, Monarch parcel

Future contact is expected to be:

Bob Foster, Chicago Parks Department

Site Map

The site map is provided in Attachment 1 with expected ponding depths shown in Attachment 4.

Operations and Maintenance Practices

The site has been developed to be low maintenance by using vegetative practices and porous pavement that reduce peak runoff rates. In addition, there is no sidewalk or driveway pavement on the site. Any problems, such as inlet clogging, that could reduce system capacity do not put any structures or infrastructure at risk because of the large ponding area available for the large drainage basins on the Sacramento and Monarch parcels.

Consequently, an O&M Plan that takes into account these factors has been developed. The O&M Plan, to be implemented by the property owner(s), includes:

- The O&M Plan procedures and practices will be reviewed and assessed annually.
- There are no roadways or sidewalks on the site to be maintained.
- The drainage catch basins and flow restrictors will be inspected and cleaned if drainage problems are reported.
- There are no volume control BMPs on-site. Consequently, no inspection is needed for volume control BMPs.
- The owner shall keep an updated log book documenting the performance of the required O&M Plan activities for perpetuity. Log books will be produced upon request by the City inspector.
- Vegetation shall be regularly maintained.
- Should insects or rodent populations reach nuisance levels, control measures will be implemented.
- Because the only infrastructure is inlets and stormsewers, no signage or fencing is planned for the stormwater system.
- Underground vaults (manholes and catch basins) are designed to facilitate cleaning and maintenance. Confined space safety procedures must be followed when entering.

Employee Training

New employees responsible for maintenance will be informed of the O&M Plan procedures and requirements. General guidance relevant to the site inspections and maintenance will be provided.

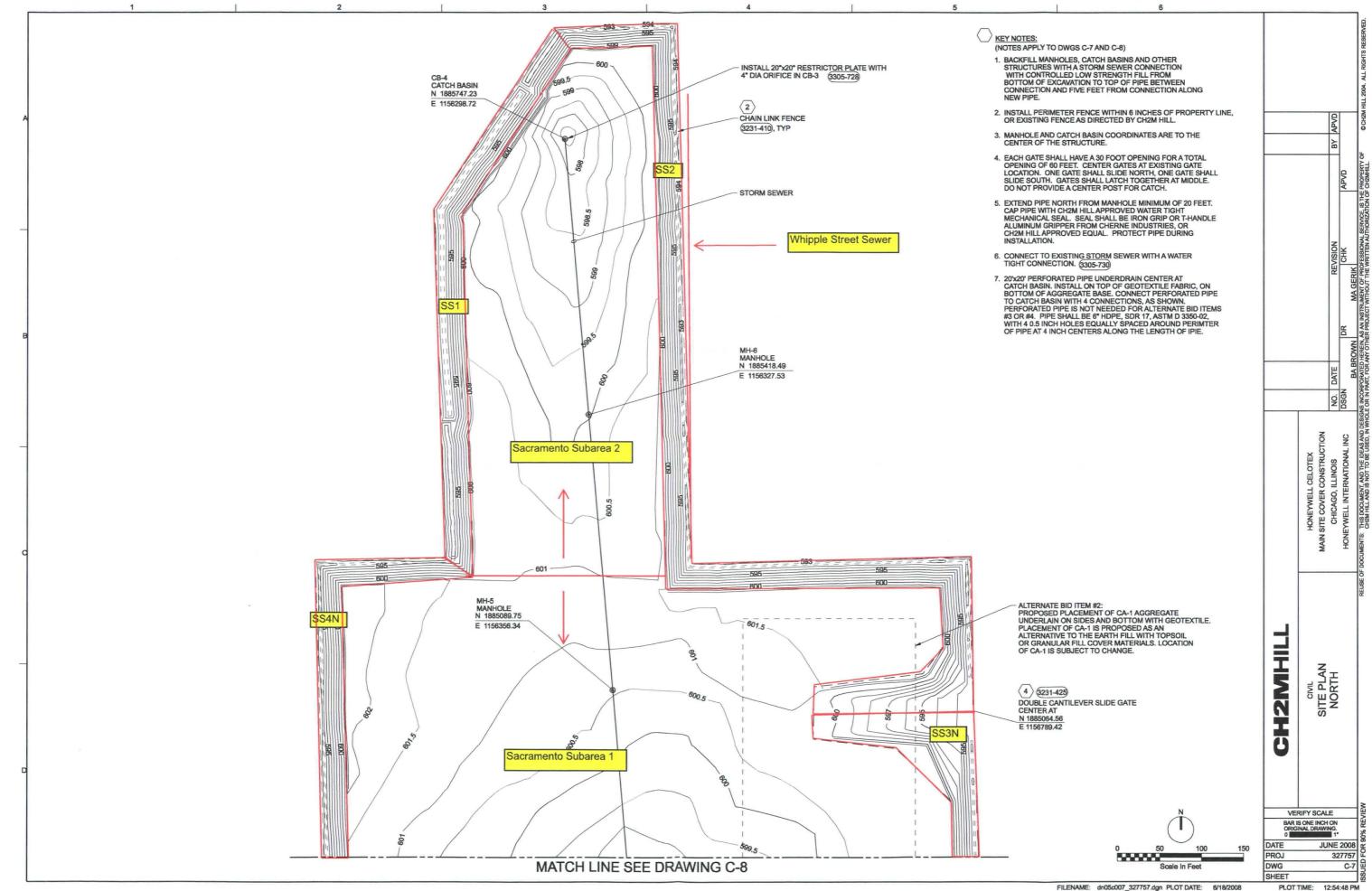
Operation and Maintenance Plan Modifications

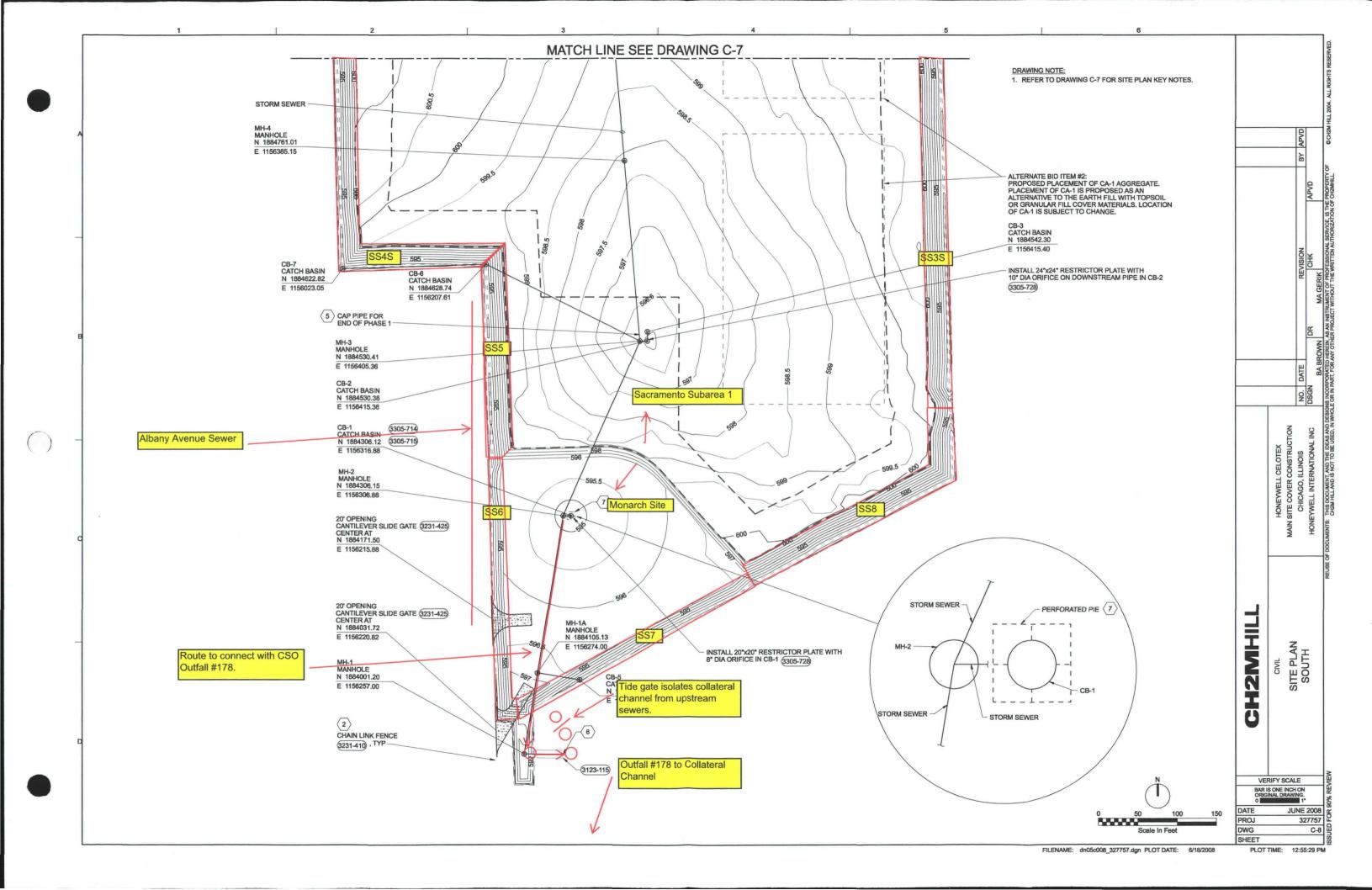
Proposed modification to the O&M Plan must be submitted to the DWM-Sewer Design Section for review and approval. The existing and proposed O&M Plans and a copy of the original DWM approval letter are required for the modification and must be submitted simultaneously with the proposed amendments.

Other Submittals and Requirements

A copy of final as-built plans will be submitted to the Department of Water Management sewer inspector for approval within 14 days after completion of construction.

Attachment 1 – Site Map





Attachment 2 – Design Plan Drawings

Three original signed copies of the design plan drawings were included in the original application to the City of Chicago Building Department. One copy of those drawings is included here.

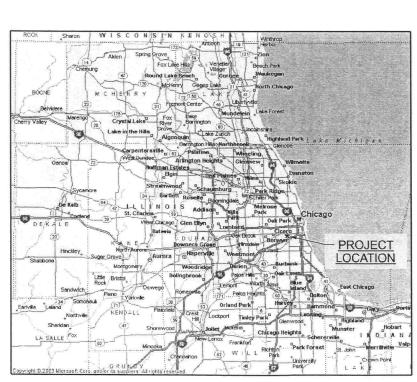
HONEYWELL CELOTEX MAIN SITE COVER CONSTRUCTION CHICAGO, ILLINOIS FINAL DESIGN (JUNE 27, 2008)

I HEARBY CERTIFY THAT THESE PLANS WERE PREPARED BY ME AND TO THE BEST OF MY PROFFESIONAL KNOWLEDGE COMPLY WITH THE CHICAGO BUILDING CODE:

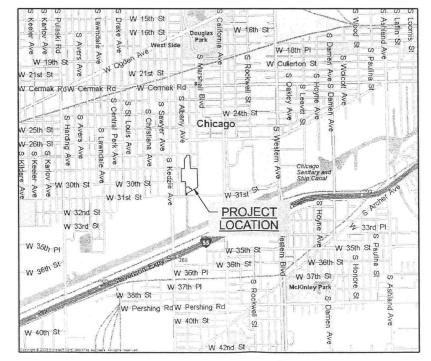


INDEX OF DRAWINGS

	SHEET	DRAWING	TITLE
	NO.	NO.	
	GENERAL		
	1	G-1	TITLE SHEET, INDEX OF DRAWINGS AND AREA/VICINITY/LOCATION MAPS
	2	G-2	CIVIL AND DESIGNATION LEGENDS, ABBREVIATIONS AND GENERAL NOTES
	CIVIL		
	3	C-1	DEMOLITION PLAN - NORTH
	4	C-2	DEMOLITION PLAN - SOUTH
	5	C-3	PHASING AND GRADING PLAN - NORTH
A	6	C-4	PHASING AND GRADING PLAN - SOUTH
717	7	C-5	SEDIMENTATION AND EROSION CONTROL PLAN - NORTH
	8	C-6	SEDIMENTATION AND EROSION CONTROL PLAN - SOUTH
	9	C-7	SITE PLAN - NORTH
	10	C-8	SITE PLAN - SOUTH
	11	C-9	STORM SEWER PROFILES
	12	C-10	TYPICAL SECTIONS AND STORM SEWER PROFILES
	13	C-11	DETAILS
	14	C-12	DETAILS
	15	C-13	DECONTAMINATION PAD DETAIL

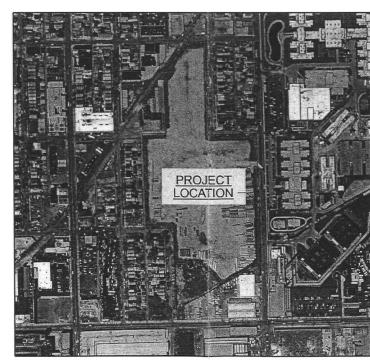


AREA MAP



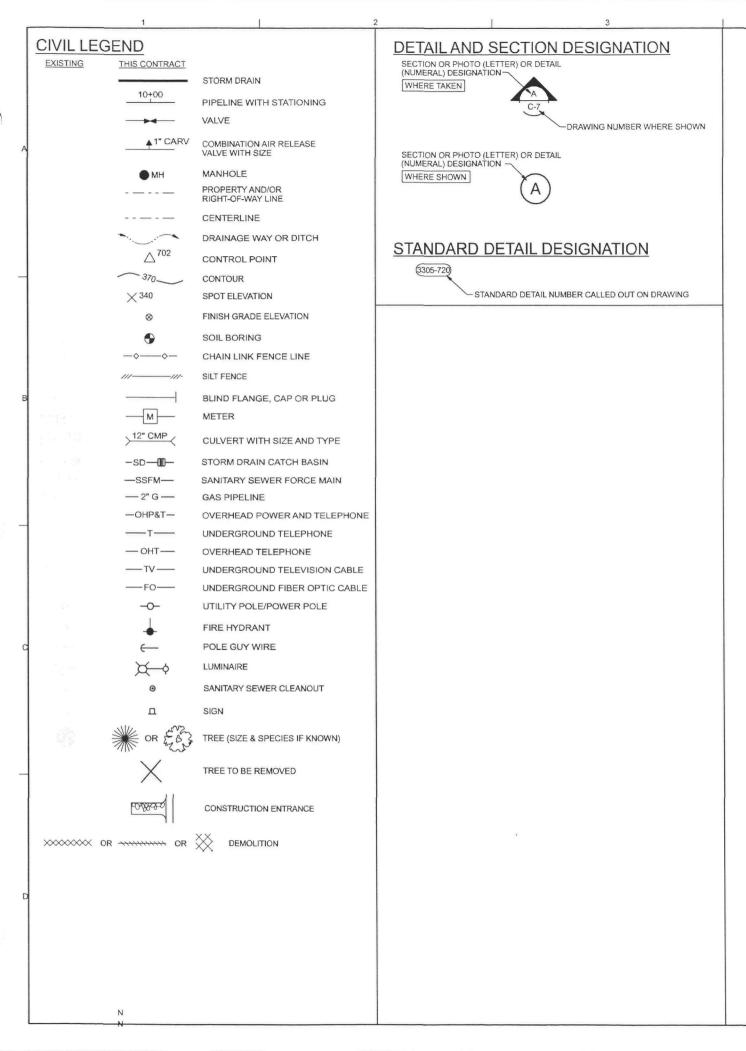
VICINITY MAP





LOCATION MAP





ABBREVIATIONS

AVE **AVENUE** BOTTOM BOT CAST IRON PIPE CIP CMP CORRUGATED METAL PIPE

CL CENTERLINE CONC CONCRETE DIA DIAMETER

DIP DUCTILE IRON PIPE DND DO NOT DISTURB

DR DRIVE OR DIMENSION RATIO FAST

EL **ELEVATION ESVCF** EXTRA STRENGTH VITRIFIED CLAY PIPE

EXST **EXISTING** EW EACH WAY FORCE MAIN FM FO FIBER OPTIC G GAS GM

GRAVITY MAIN HDPE HIGH DENSITY POLYETHYLENE

HORIZ HORIZONTAL INV **INVERT** IRON POST IP LT LEFT MAXIMUM MAX MANHOLE MH MINIMINA MIN

MJ MECHANICAL JOINT

N NORTH

NCP NON REINFORCED CONCRETE PIPE

NO NUMBER NTS NOT TO SCALE OC ON CENTER OD OUTSIDE DIAMETER OHP OVERHEAD POWER PE PERMANENT FASEMENT PL PROPERTY LINE PP POWER POLE

POLYVINYL CHLORIDE PVC. RCP REINFORCED CONCRETE PIPE RD

ROAD REQD REQUIRED R.J RESTRAINED JOIN RT RIGHT

RR RAILROAD RIGHT OF WAY R/W SOUTH STORM DRAIN SD

SDR STANDARD DIMENSION RATIO SEWER MANHOLE NUMBER SN

SPECD SPECIFIED SS SANITARY SEWER

SST STAINLESS STEEL STA STATION

TBR&R TO BE REMOVED AND REPLACED

T, TEL TELEPHONE

TEMPORARY EASEMENT TE

TV **TELEVISION** TYP TYPICAL

UGP UNDERGROUND POWER

VERT VERTICAL WATER, WEST W WI WT WEIGHT

GENERAL SITE NOTES:

- SOURCE OF TOPOGRAPHY SHOWN ON THE CIVIL PLANS ARE BASE MAPS PROVIDED BY BOLLINGER, LACH AND ASSOCIATES, INC. ADDITIONAL MAPPING HAS BEEN ADDED FROM AS-BUILT DATA. EXISTING CONDITIONS MAY VARY FROM THOSE SHOWN ON THESE PLANS. THE CONTRACTOR SHALL VERIFY EXISTING CONDITIONS AND ADJUST WORK PLAN ACCORDINGLY PRIOR TO BEGINNING CONSTRUCTION.
- EXISTING TOPOGRAPHY, STRUCTURES, AND SITE FEATURES ARE SHOWN SCREENED AND/OR LIGHT-LINED. NEW FINISH GRADE, STRUCTURES, AND SITE FEATURES ARE SHOWN HEAVY-LINED.
- 3 HORIZONTAL DATUM: NAD 83
- 4. VERTICAL DATUM: NAVD 88.
- 5. STAGING AREA SHALL BE FOR CONTRACTOR'S EMPLOYEE PARKING, CONTRACTOR'S TRAILERS AND ON-SITE STORAGE OF MATERIALS.
- 6. PROVIDE TEMPORARY FENCING AS NECESSARY TO MAINTAIN SECURITY
- 7. ELEVATIONS GIVEN ARE TO FINISH GRADE UNLESS OTHERWISE SHOWN.
- 8. SLOPE UNIFORMLY BETWEEN CONTOURS AND SPOT ELEVATIONS SHOWN.
- CONTRACTOR SHALL BE RESPONSIBLE FOR IMPLEMENTING AND MAINTAINING EROSION CONTROL DEVICES DURING CONSTRUCTION.

GENERAL YARD PIPING AND **UTILITIES NOTE:**

. ALL PIPES SHALL HAVE A CONSTANT SLOPE BETWEEN INVERT ELEVATIONS

GENERAL NOTES

GENERAL NOTE

- PIPELINE STATIONING AND LENGTHS OF PIPE INDICATED ARE BASED ON HORIZONTAL PROJECTION OF THE PIPE CENTERLINE
- INDICATED SCALES ARE BASED ON FULL-SIZE DRAWINGS, AND IF DRAWINGS ARE REDUCED, SCALES MUST BE ADJUSTED ACCORDINGLY.
- 3. GEOTECHNICAL INFORMATION AND BORING LOGS ARE AS INDICATED.
- 4. EXISTING UTILITIES ARE SHOWN ON THESE PLANS FOR CONVENIENCE OF THE CONTRACTOR. THE EXISTENCE AND LOCATION OF UNDERGROUND UTILITY PIPE AND/OR STRUCTURES, AS SHOWN, ARE BASED ON INFORMATION OBTAINED FROM AVAILABLE AGENCY STANDARDS. TAKE PRECAUTIONARY MEASURES TO PROTECT UTILITY LINES AND STRUCTURES SHOWN AS WELL AS ANY AND ALL OTHERS NOT OF RECORD OR NOT SHOWN ON THESE PLANS. EXISTING UTILITY SERVICE LATERALS ARE TYPICALLY NOT SHOWN ON THESE PLANS UNLESS OTHERWISE INDICATED.
- . VERIFY THE ACTUAL LOCATION, ELEVATION AND CONDITION OF POINTS OF CONNECTION TO EXISTING FACILITIES AND PROVIDE NOTICE OF ANY DISCREPANCIES AS INDICATED.
- . PRESERVE ALL SURVEY MARKERS AND MONUMENTATION WHEREVER POSSIBLE. RE-ESTABLISH THOSE REQUIRING REMOVAL IN ACCORDANCE WITH THE LOCAL GOVERNING AUTHORITY.
- LIMIT CONSTRUCTION OPERATIONS TO WITHIN THE RIGHT-OF-WAY, EASEMENTS AND ANY OTHER DESIGNATED WORK AREAS AS INDICATED. THE CONTRACTOR IS SOLELY RESPONSIBLE FOR ANY DAMAGES AS A RESULT OF CONSTRUCTION ACTIVITIES OUTSIDE OF RIGHT-OF-WAYS, EASEMENTS AND ANY OTHER DESIGNATED WORK AREAS SHOWN ON THE DRAWINGS.
- RESTORE ALL AREAS DISTURBED BY CONSTRUCTION ACTIVITIES AS INDICATED. TOPSOIL AREAS ARE TO BE VEGETATED WITH GRASS
- ALL SPECIFICATIONS, DRAWINGS, AND DETAILS INCLUDED IN THE CONTRACT DOCUMENTS SHALL FULLY APPLY TO THE WORK WHETHER SPECIFICALLY REFERENCED OR NOT
- LAY PIPE TO CONTINUOUS LIPWARD OR DOWNWARD SLOPE BETWEEN INDICATED ELEVATION POINTS WHILE MAINTAINING MINIMUM CLEARANCE WITH EXISTING UTILITIES.

1. THIS IS A STANDARD LEGEND SHEET. THEREFORE, NOT ALL OF THE

8-19

IGNATION LEGENDS, AND GENERAL NOTES

CIVIL AND DESIGNABLE

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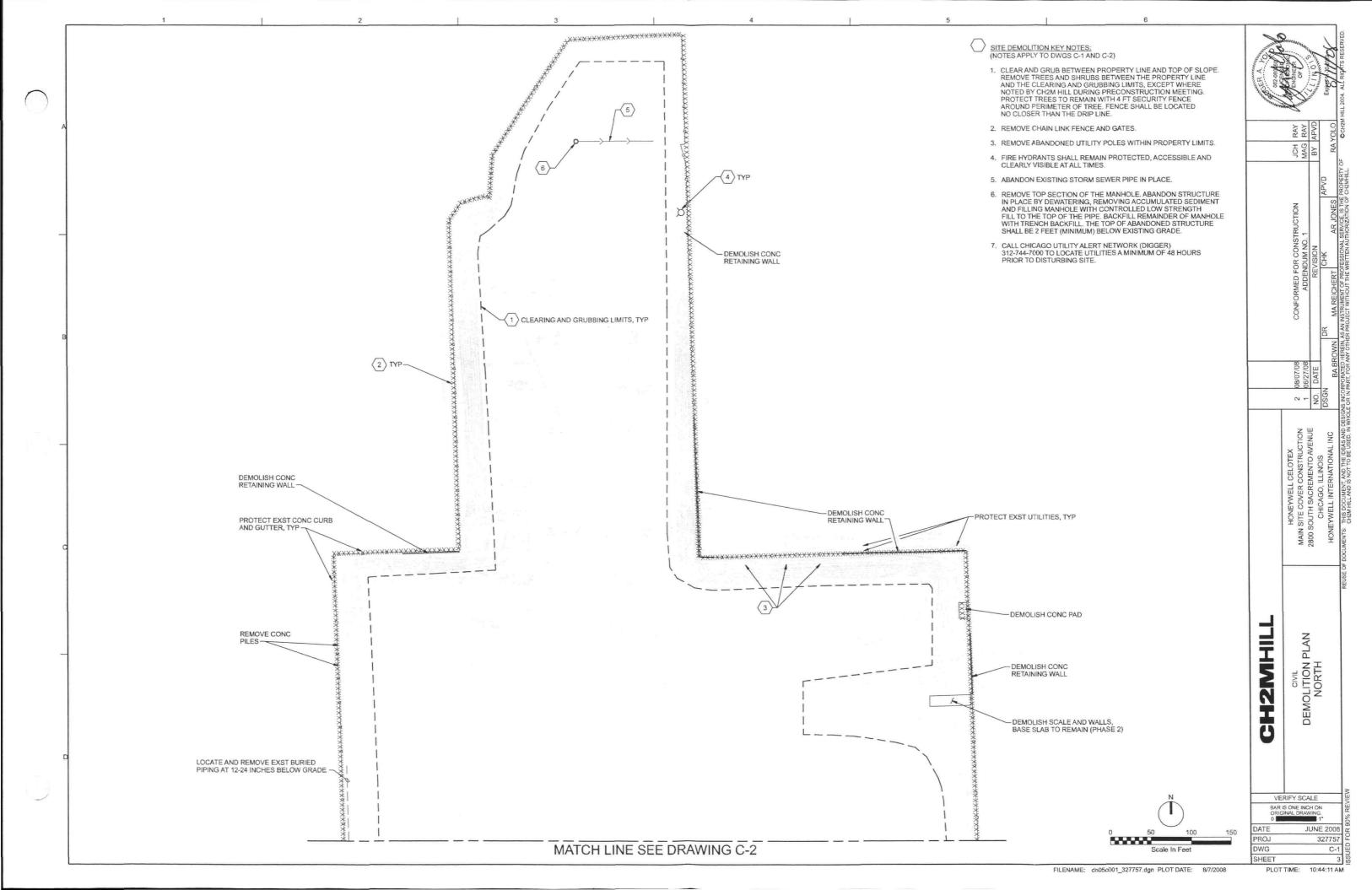
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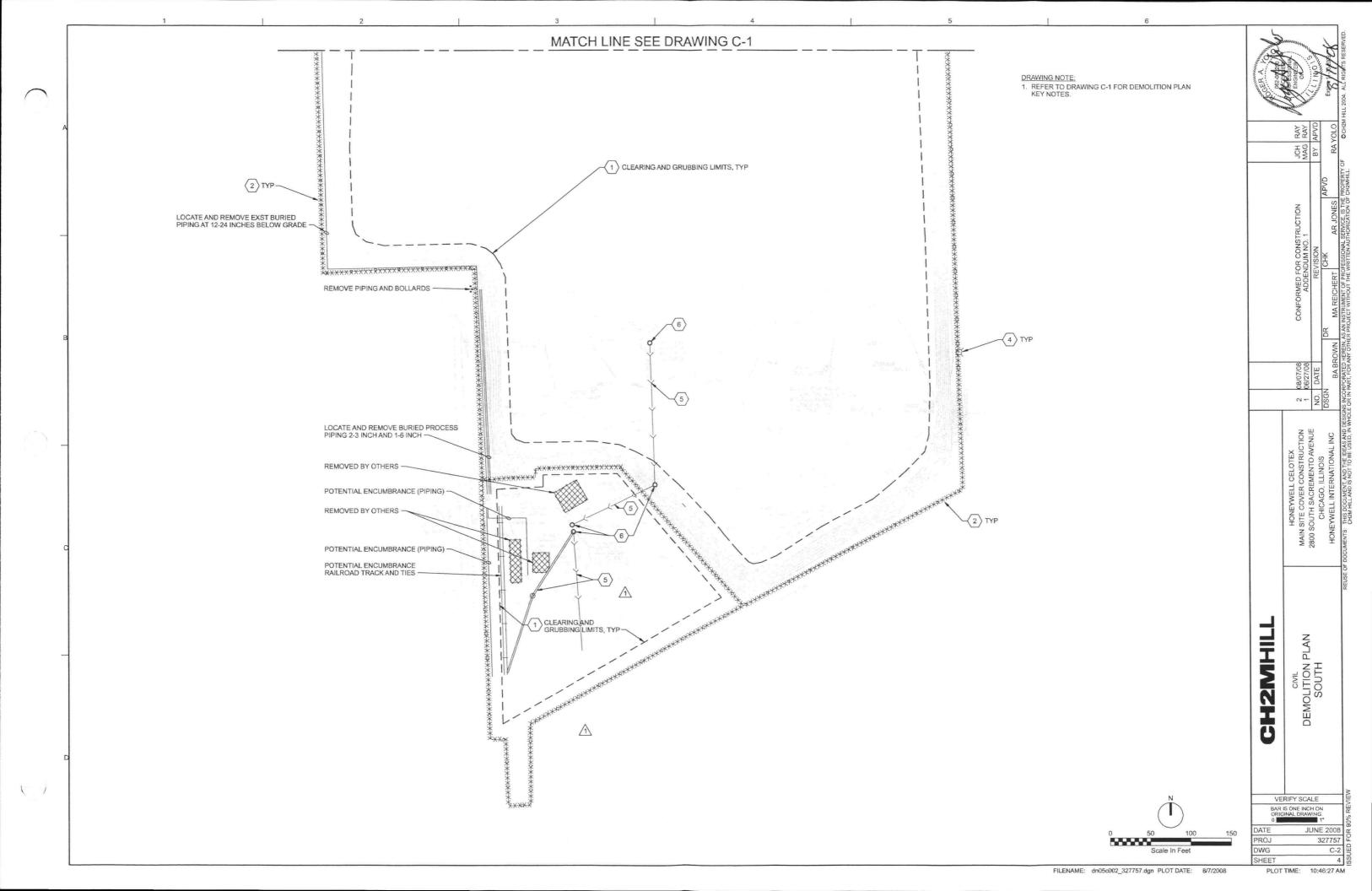
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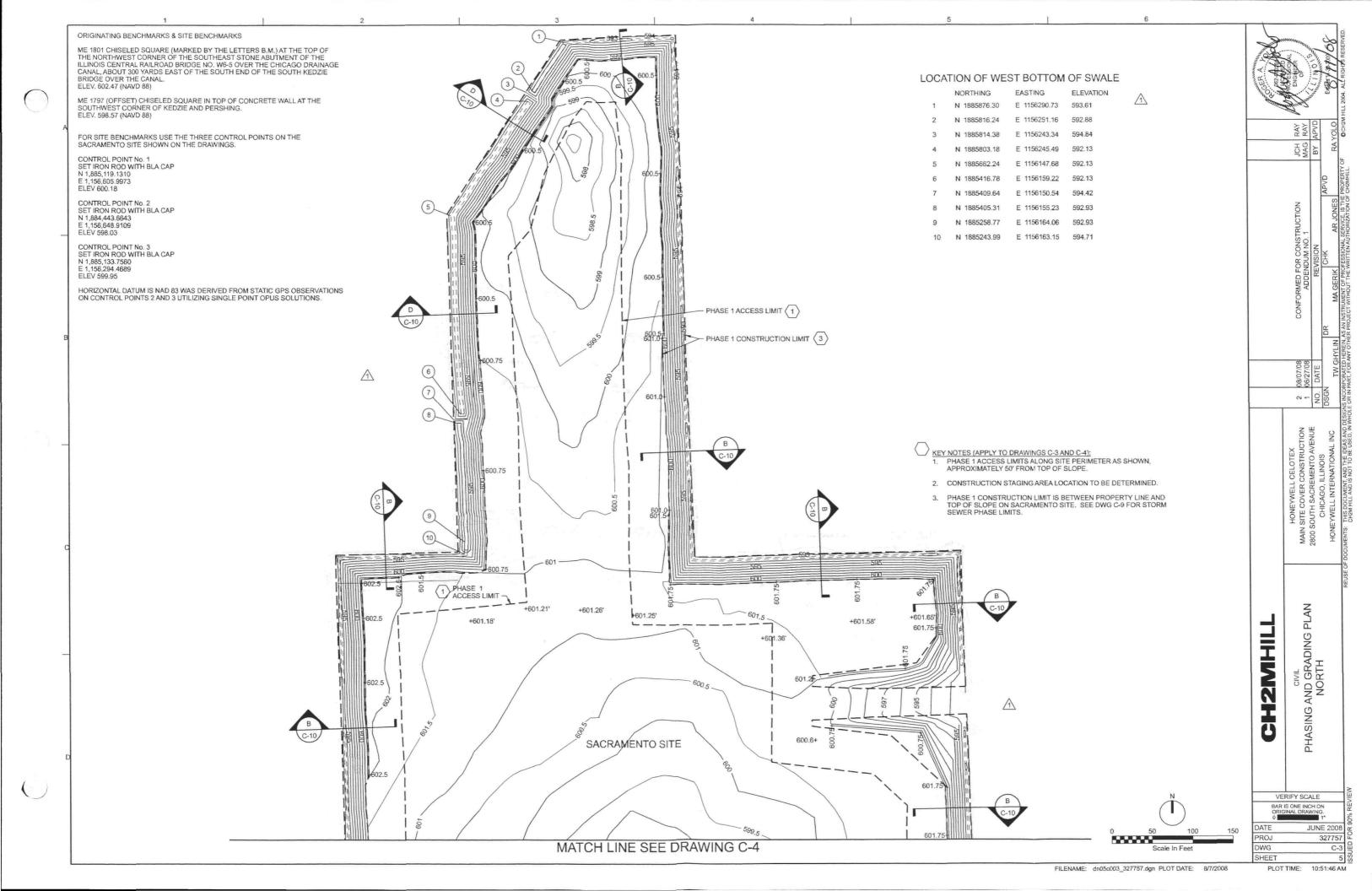
VERIFY SCALE

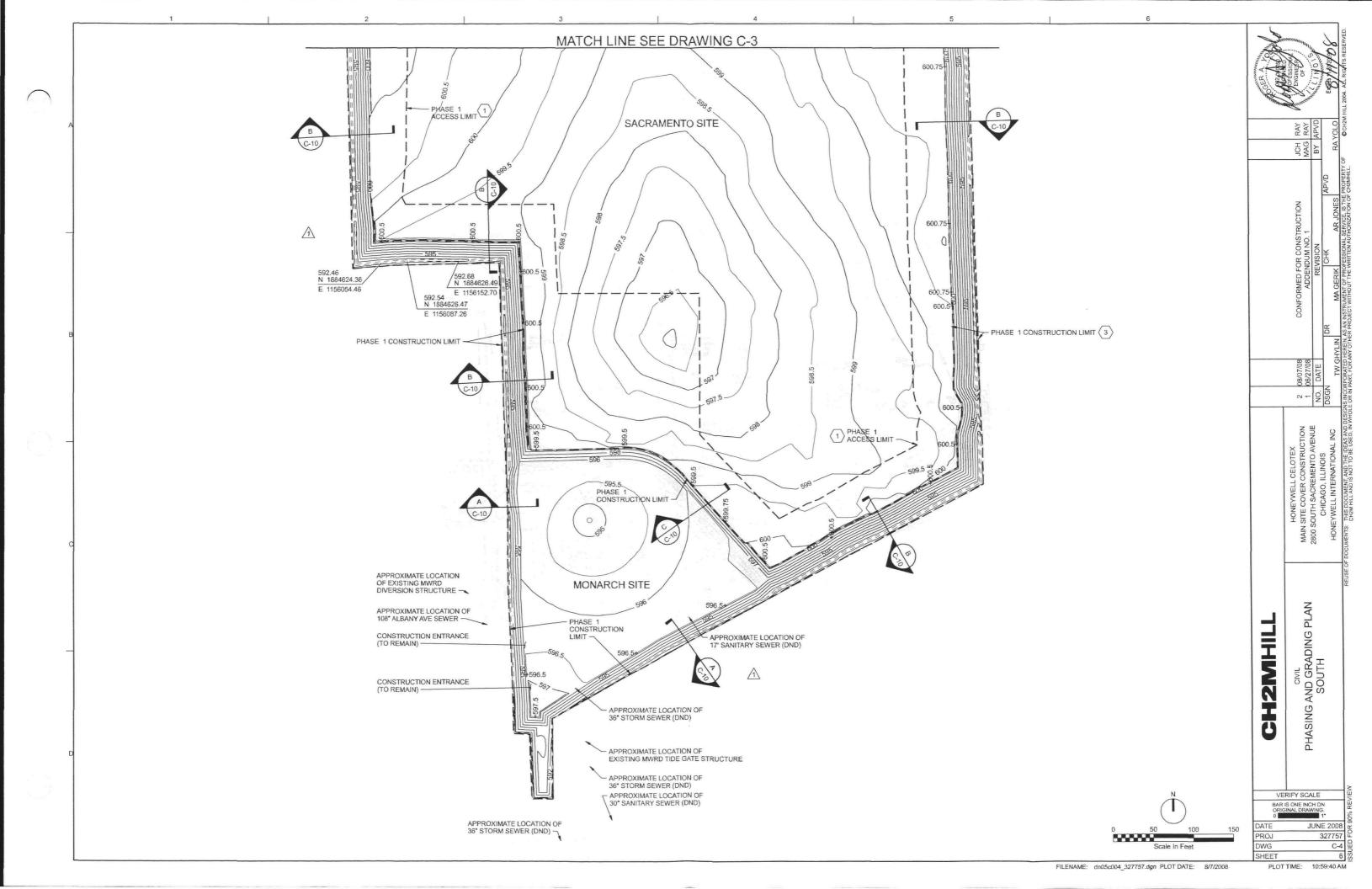
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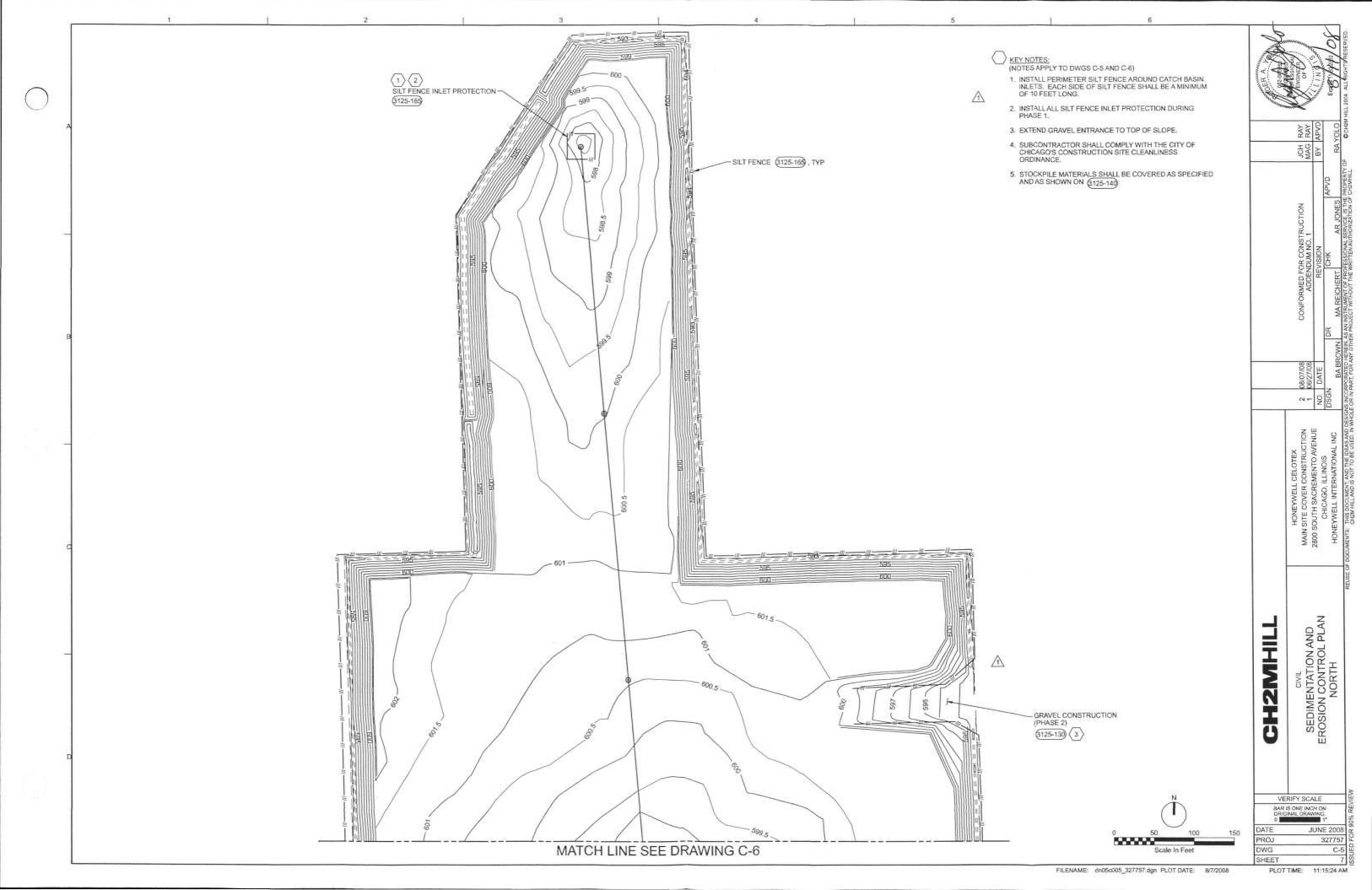
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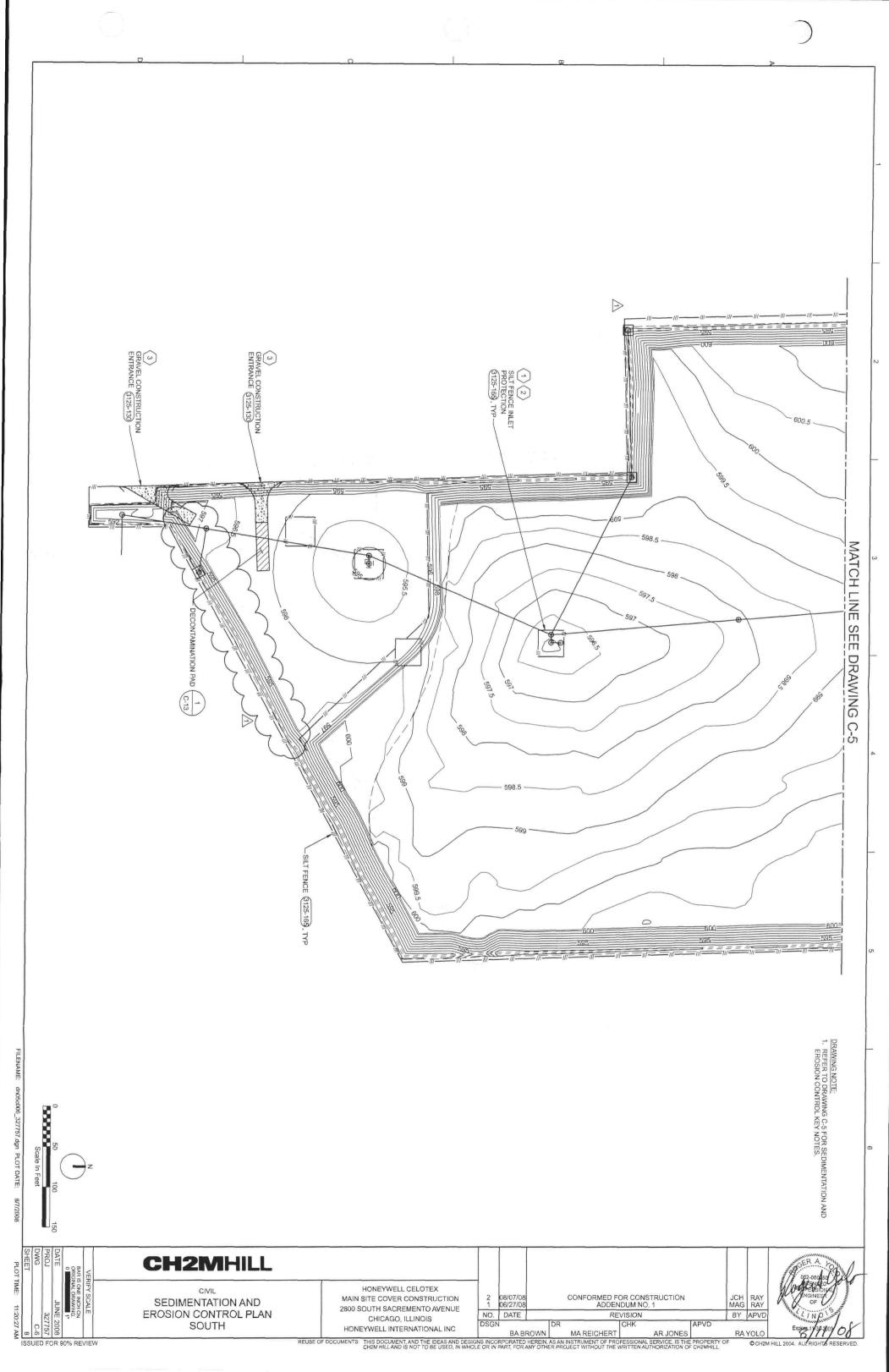


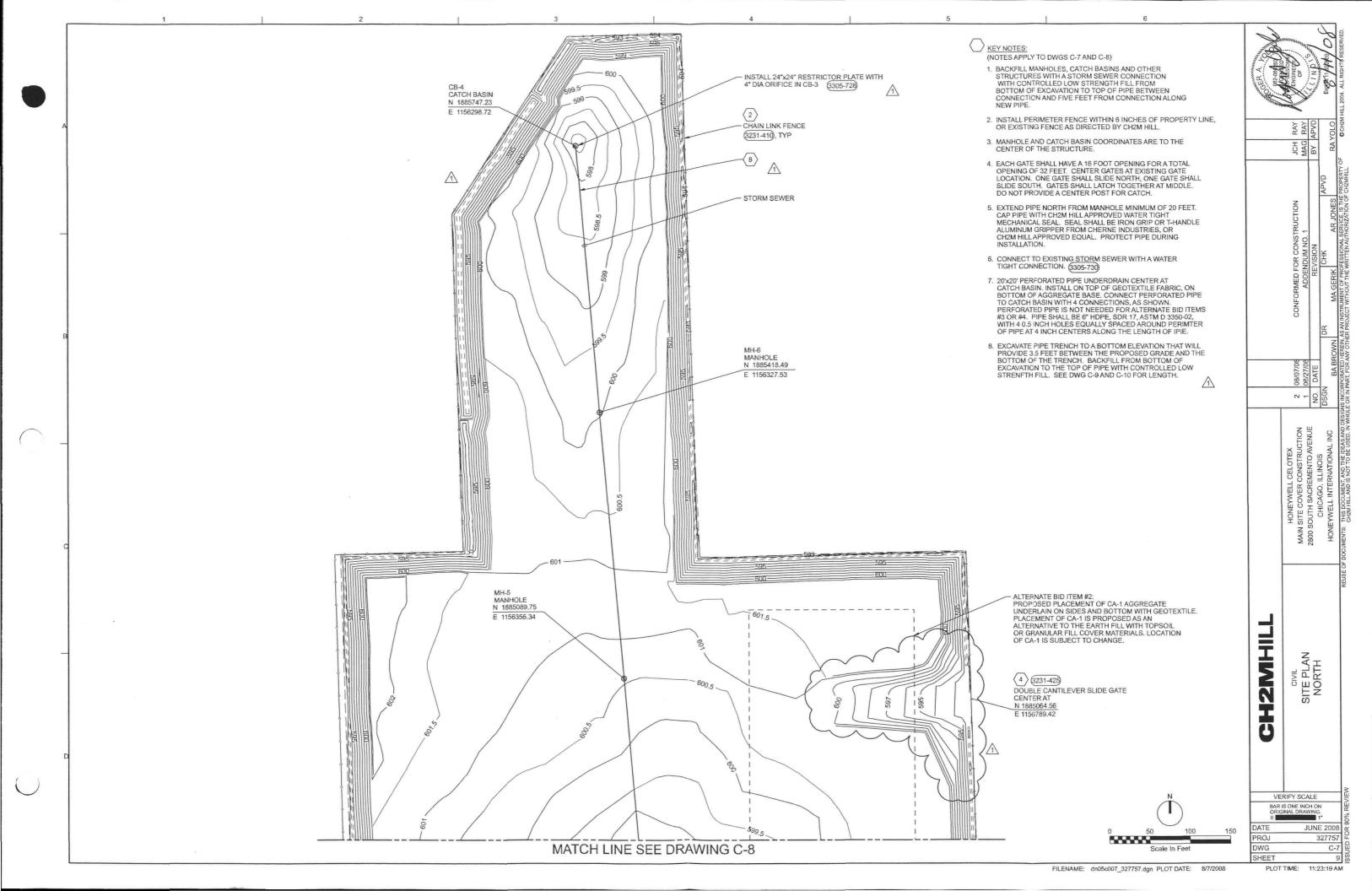


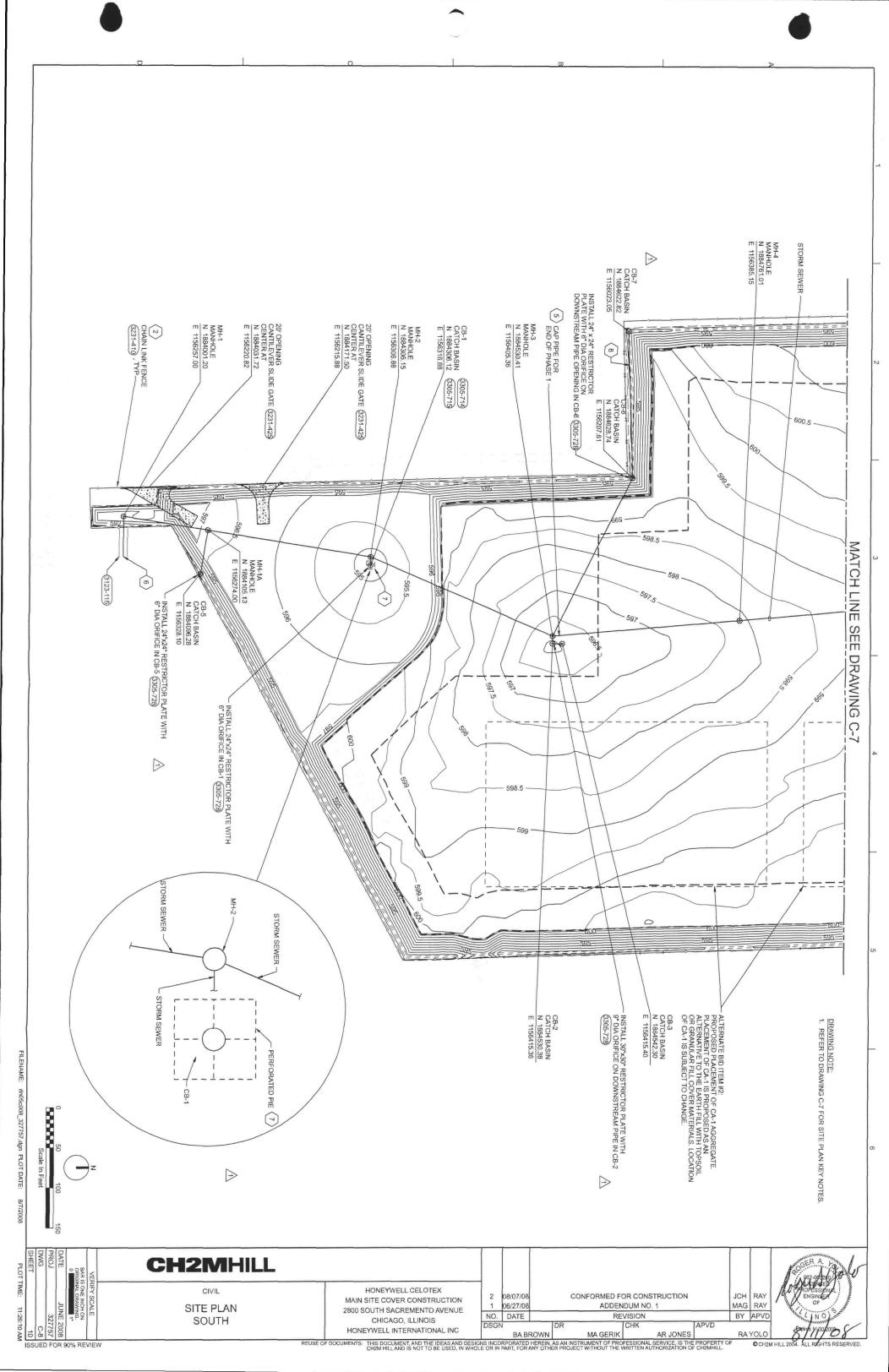


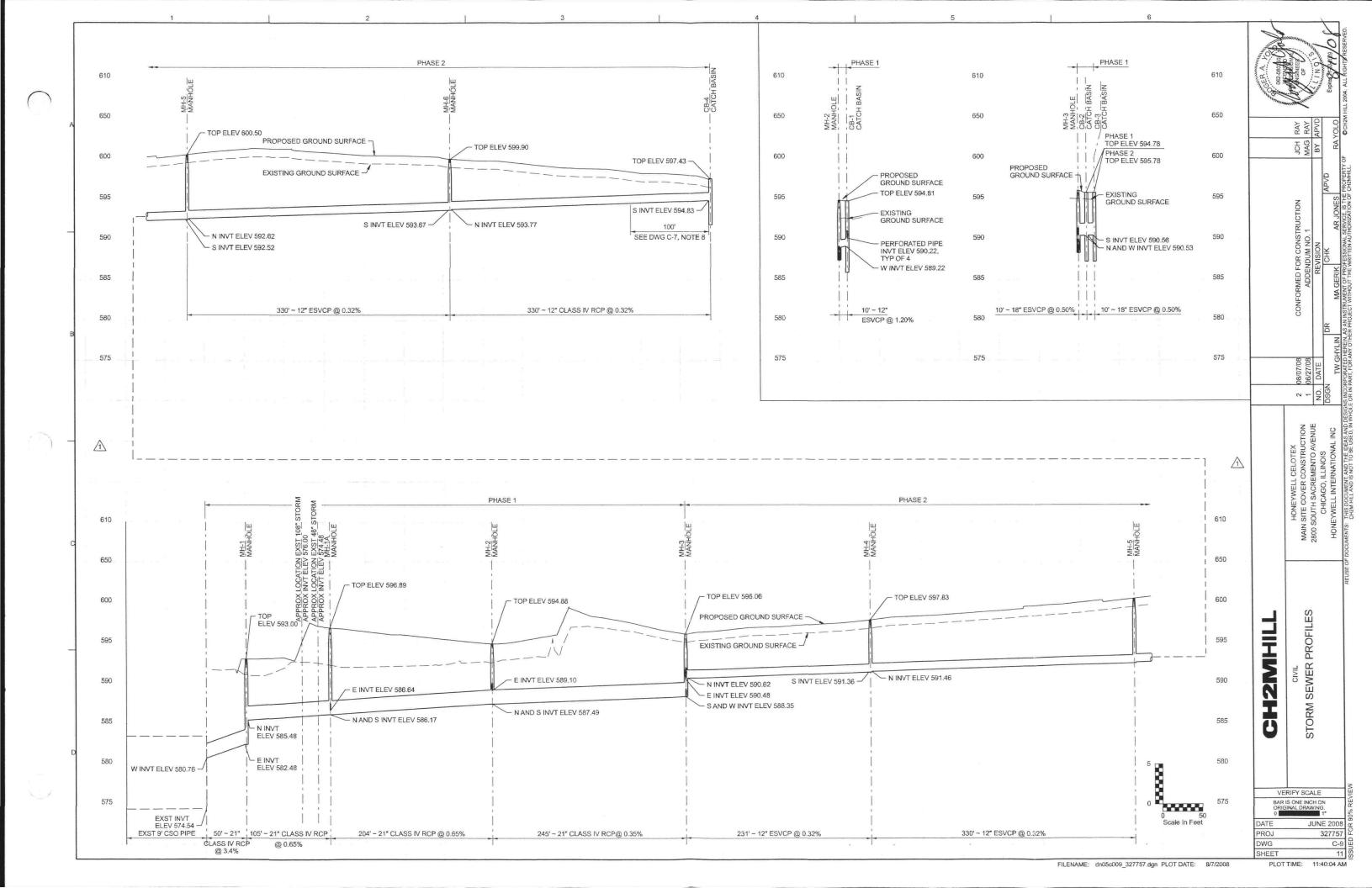


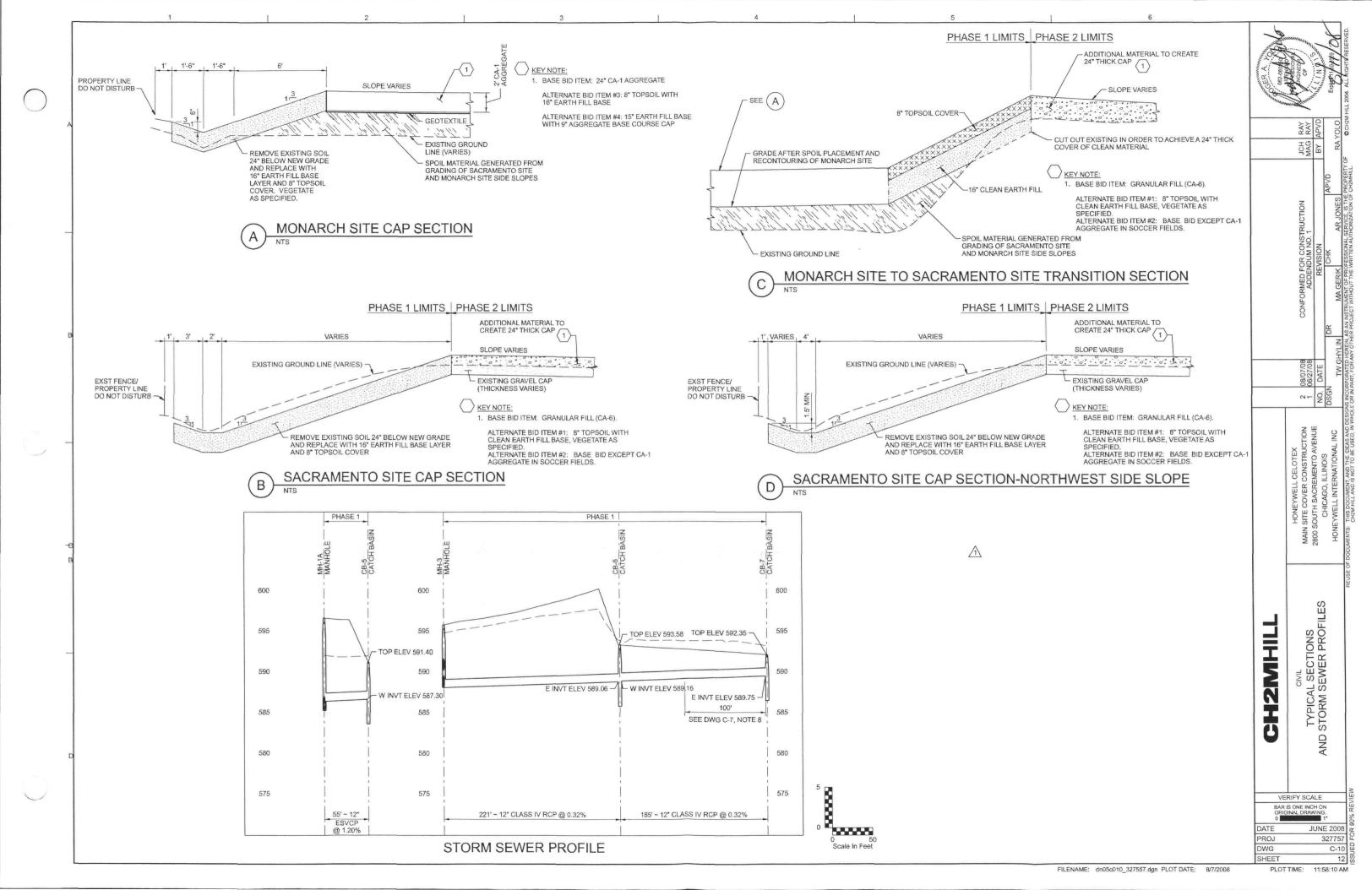


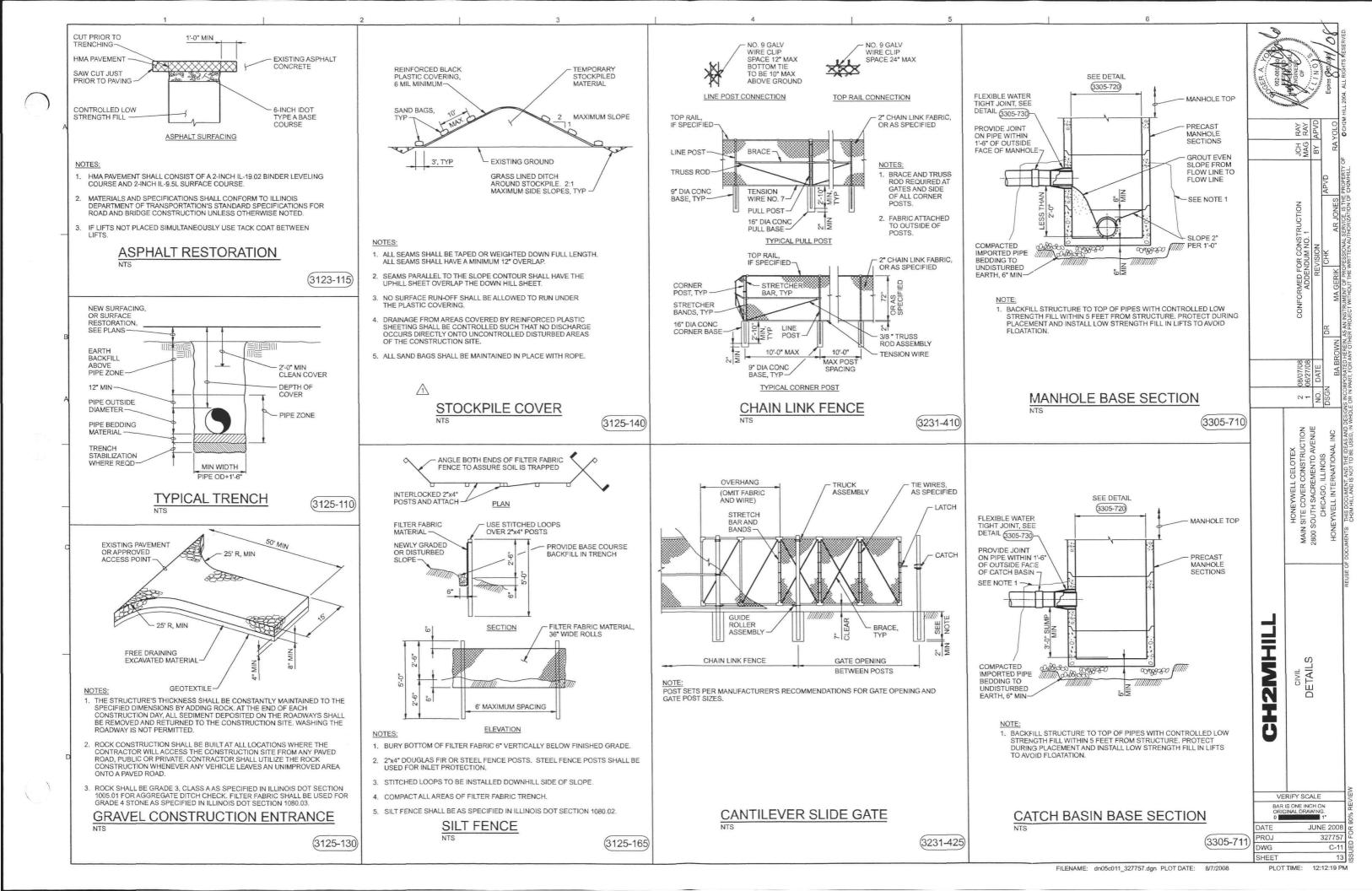


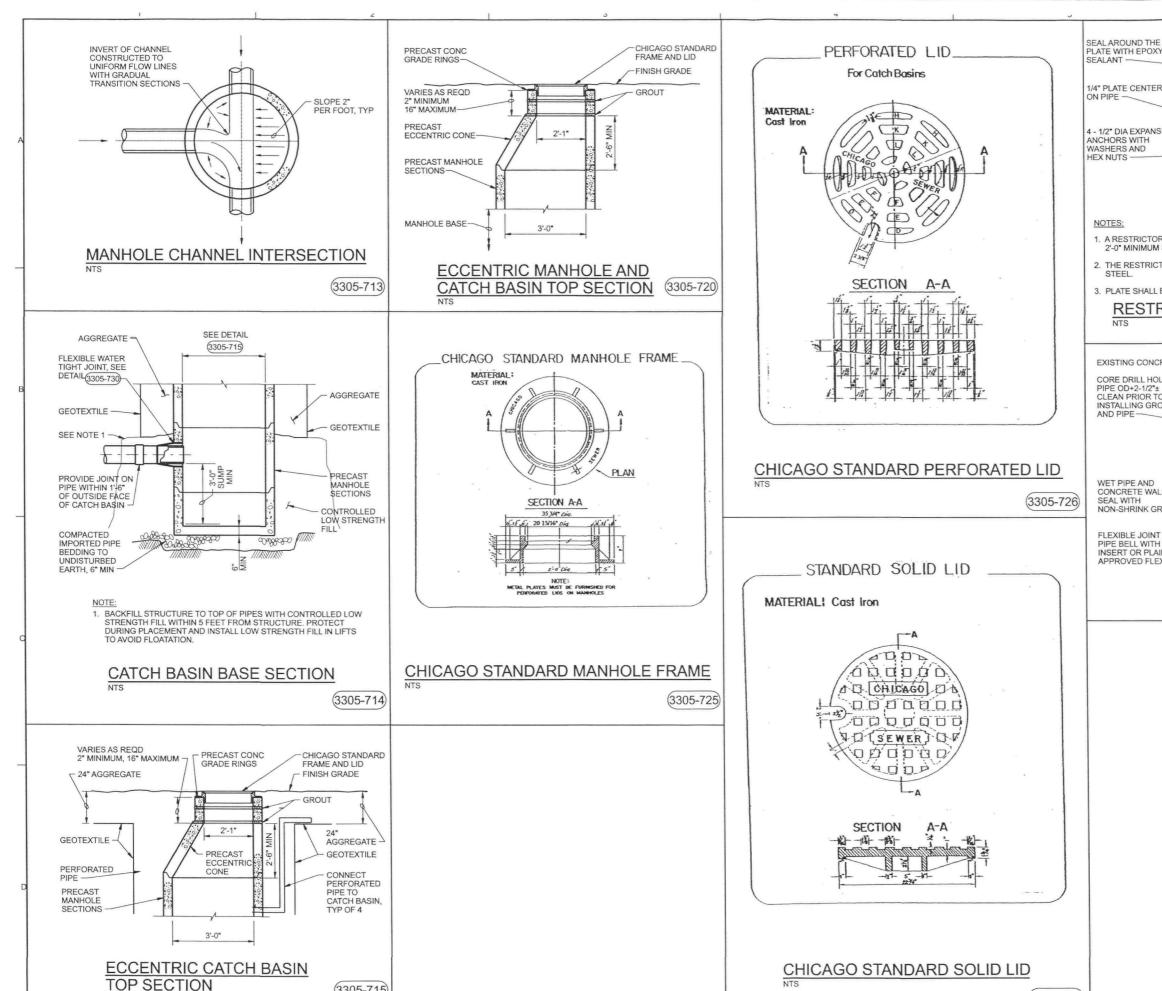




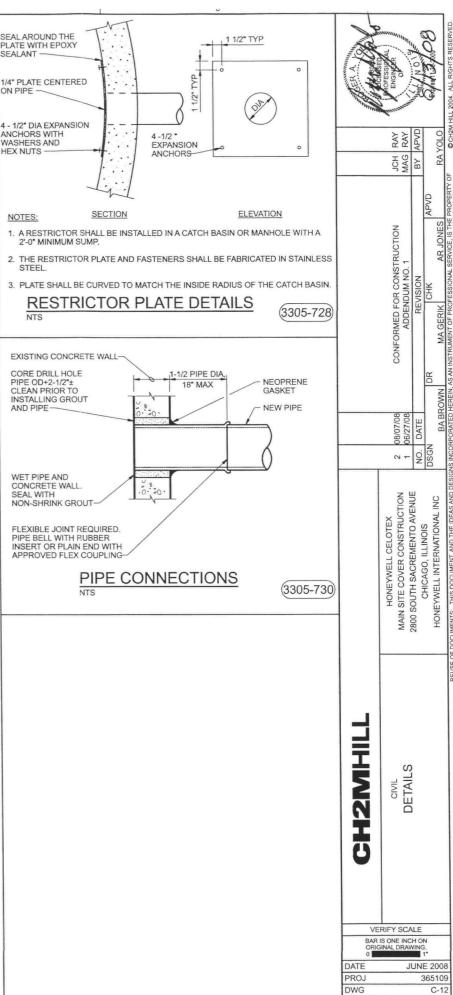








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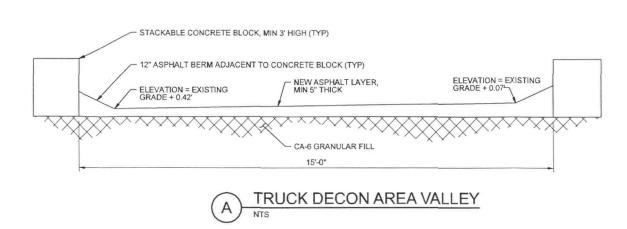
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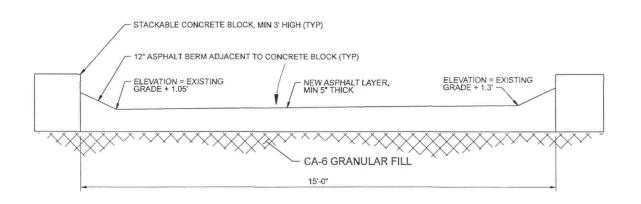
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SHEET

TRUCK APPROACH LOADING AREA ASPHALT SLOPE TO MEET EXISTING STONE SURFACE STACKABLE CONCRETE BLOCKS (TYP) RIDGE 1% MIN TRUCK AREA VALLEY 1% MIN RIDGE ASPHALT SLOPE TO MEET EXISTING STONE SURFACE

 $\frac{\mathsf{TRUCK}\;\mathsf{LOADING/DECON}\;\mathsf{AREA}\;\mathsf{PLAN}}{\mathsf{\tiny NTS}}$





NOTES:

TRUCK DECON AREA RIDGE

 TRUCK DECON AREA TO BE CONSTRUCTED AND MAINTAINED BY CONTRACTOR.

- NEW ASPHALT LAYER IS MINIMUM 5" THICK. MATERIAL BETWEEN NEW ASPHALT LAYER AND STONE SURFACE CAN BE APPROPRIATELY GRADED AND COMPACTED AGGREGATE.
- 3. MATERIALS AND SPECIFICATIONS FOR HEAVY VOLUME MIX SHALL CONFORM TO IDOT STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION UNLESS OTHERWISE NOTED.

1 DECONTAMINATION AREA

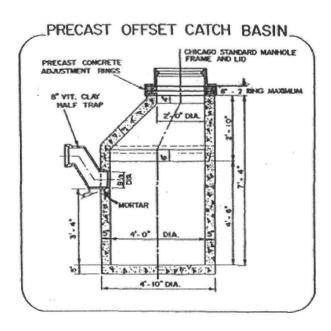
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Modification #1

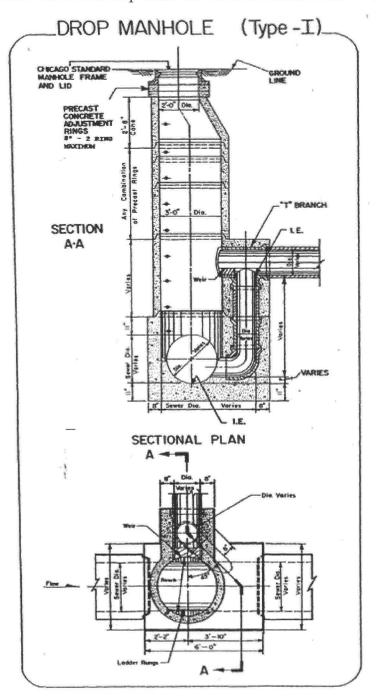
Issued August 13, 2008

Item #1: Catch Basin Section Detail 3305-711 is replaced with the precast offset catch basin with half-trap shown below, except that the sump will be a minimum of 2 feet. Inverts shown on the plans shall be for the main pipe segment immediately down slope of the half-trap.



Item #2: At Manhole 3, the north and east inverts will be changed as follows. The N INVT elevation will be lowered 590.32. The E INVT will be lowered to 590.34. The pipe slope between Manhole 4 and Manhole 3 will be increased to 0.0045 feet per foot. The pipe slope between Catch Basin 2 and Manhole 3 will be increased to 0.019 feet per foot.

Item #3: For Manhole 1, the manhole detail will be replaced with the Type I Drop Manhole shown below. The drop diameter will be 12 inches made of Class IV RCP.



Item #4: The pipe slope between Catch Basin 3 and Catch Basin 2 is changed to 0.35%. The invert elevations at Catch Basins 3 and 2 remain the same.

Documentation of Plan Modifications

All modifications will be documented on the final as-built plans that will be submitted to the Department of Water Management sewer inspector for approval within 14 days after completion of construction.

Attachment 3 - Modeling Calculations

Stage, Storage Discharge Calculations

Area 1

/									
		Depth			Above			Discharge	Total
		Above MH	Depth	Manhole	ground	Total		through	Discharg
	Stage	Invert	above Rim	Storage	Storage	Storage	Discharge CB	12" Pipe	e 12"
	(ft)	(ft)	(ft)	(acre-ft)	(acre-ft)	(acre-ft)	(cfs)	cfs	(cfs)
	589.38	0	0	0.0000		0.0000		0.0	0.0
	590.38	1	0	0.0003		0.0003		3.8	3.8
	591.38	2	0	0.0006		0.0006		5.4	5.4
	592.38	3	0	0.0009		0.0009		6.7	6.7
	593.38	4	0	0.0012		0.0012		7.7	7.7
	594.38	5	0	0.0014		0.0014		8.6	8.6
	594.78	5.4	0	0.0016	0	0.0016		8.9	8.9
	595.5	6.12	0.72	0.0016	0.08	0.0816	4.1	9.5	4.1
	596	6.62	1.22	0.0016	0.16	0.1616	5.3	9.9	5.3
	597	7.62	2.22	0.0016	1.03	1.0316	7.2	10.6	7.2
	598	8.62	3.22	0.0016	3.52	3.5216	8.6	11.3	8.6

No additional MH storage above the rim elevation

Orifice = 0.61*A*SQRT(2*g*h)

Restrictor

Diameter

(inches) Area (sf)

12 0.79 C = 0.61 per chicago regulations

-- Inlet Grate Capacities Menu -- * Jump to: >HOME >BACK

- Inlet Grate Capacities Menu -- 💌 PHOME PEACE

Weir & Orifice Flow Comparison

 $Q = 0.6A \sqrt{2gh}$ (Orifice Flow Equation)

Q = Capacity in CFS
A = Free open area of grate in sq. ft
g = 32.2 (feet per sec/sec)
h = Head in feet

Either Select catalog number (will automatically fill in Open Area and Perimeter) or enter your own values Enter head value

 Press CALCULATE The results will determine automatically if your situation falls into a Weir, Transitional or Orifice flow. Additionally, a pop-up window will offer Neenah grates which fall within the parameters chosen.

Orifice Information

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

Q = Capacity in CFS P = Feet perimeter h = Head in feet

Weir Information

 $Q = 0.6A\sqrt{2gh}$ (Orifice Flow Equation)

A = Free open area of grate in sq. ft. g = 32.2 (feet per sec/sec) h = Head in feet

Orifice Information

Catalog number and grate type

nstructions

 Either Select catalog number (will automatically fill in Open Area and Perimeter) or enter your own values

Weir & Orifice Flow Comparison

 Enter head value Press CALCULATE

The results will determine automatically if your situation falls into a Weir, Transitional or Orifice flow. Additionally, a pop-up window will offer Neenah grates which fall within the parameters chosen.

Calculate

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

Q = Capacity in CFS P = Feet perimeter h = Head in feet

Weir Information

Catalog n	umber	and	grate	type:
R-4370-15				

Feet perimeter (P): Weir capacity in cfs:

Transitional flow in cfs:

Calculate

Head in feet (h): 0.72

4.1

Free open area in sq. ft. (/Feet perimeter (P):

Orifice capacity in cfs:

Weir capacity in cfs:

R-4370-15 D

Transitional flow in cfs

Head in feet (h):

Free open area in sq. ft. (A):

Orifice capacity in cfs. 5.3



800-558-5075

FAX: 920-729-3661

-- Inlet Grate Capacities Menu -- 🛩 Jump to: >HOME >BACK

Weir & Orifice Flow Comparison

 $Q = 0.6A\sqrt{2gh}$ (Orifice Flow Equation)

Q = Capacity in CFS A = Free open area of grate in sq. ft. g = 32.2 (feet per sec/sec) h = Head in feet

Orifice Information

instructions

- Either Select catalog number (will automatically fill in Open Area and Perimeter) or enter your own values
- Enter head value
- Press CALCULATE

The results will determine automatically if your situation falls into a Weir, Transitional or Orifice flow Additionally, a pop-up window will offer Neenah grates which fall within the parameters chosen.

 $Q = 3.3P(h)^{1.5}$

P = Feet perimeter h = Head in feet

Weir Information

Catalog number and grate type: R-4370-15 D

Feet perimeter (P):

5.9

Weir capacity in cfs:

Calculate

Transitional flow in cfs:

Free open area in sq. ft. (A): 1.0

7.2

(Weir Equation)

Q = Capacity in CFS

Head in feet (h)

Orifice capacity in cfs:

800-558-5075 t Grate Capacities Menu -- 💌

>HOME >BACK

NOTE. The above results do not account for the dome height of Beehive-type grates. Please take note of this when determining the Head (h) value.

For additional information regarding Neenah Inlet Grate Capacities, please contact our Product Engineer, Steve Akkala, at 920-725-7000 or at sakkala@nfco.com

FS A = Free open area of grate in sq. ft g = 32.2 (feet per sec/sec) h = Head in feet

Orifice Information

ħ ation)

Instructions Either Select catalog number (will automatically fill in Open Area and Perimeter) or enter your own values

Weir & Orifice Flow Comparison

Enter head value

Press CALCULATE

The results will determine automatically if your situation falls into a Weir, Transitional or Orifice flow. Additionally, a pop-up window will offer Neenah grates which fall vithin the parameters chosen.

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

FAX: 920-729-3661

r

Q = Capacity in CFS P = Feet perimeter h = Head in feet

Weir Information

Catalog number and grate type R-4370-15 D

Feet perimeter (P): 59

Calculate

3.22 Free open area in sq. ft. (A): 10

Weir capacity in cfs:

Transitional flow in cfs:

Orifice capacity in cfs:

Head in feet (h):

NOTE: The above results do not account for the dome height of Beehive-type grates. Please take note of this when determining the Head (h) value

	Depth							
	Above MH	Depth		Manhole		Discharge	Discharge	Total
Stage	Invert	above Rim	Storage	Storage	Total Storage	CB	Restrictor	Discharge
(ft)	(ft)	(ft)	(acre-ft)	(acre-ft)	(acre-ft)	(cfs)	(cfs)	(cfs)
591.83	0	0		0.0000	0.0000	0	0.00	0.00
592.83	1	0		0.0003	0.0003	0	0.43	0.43
593.83	2	0		0.0006	0.0006	0	0.60	0.60
594.83	3	0		0.0009	0.0009	0	0.74	0.74
595.83	4	0		0.0012	0.0012	0	0.85	0.85
596.23	4.4	0	0	0.0013	0.0013	0	0.90	0.90
597	5.17	0.77	0.01	0.0013	0.0113	4.2	0.97	0.97
598	6.17	1.77	0.24	0.0013	0.2413	6.4	1.06	1.06
599	7.17	2.77	1.17	0.0013	1.1713	8	1.14	1.14

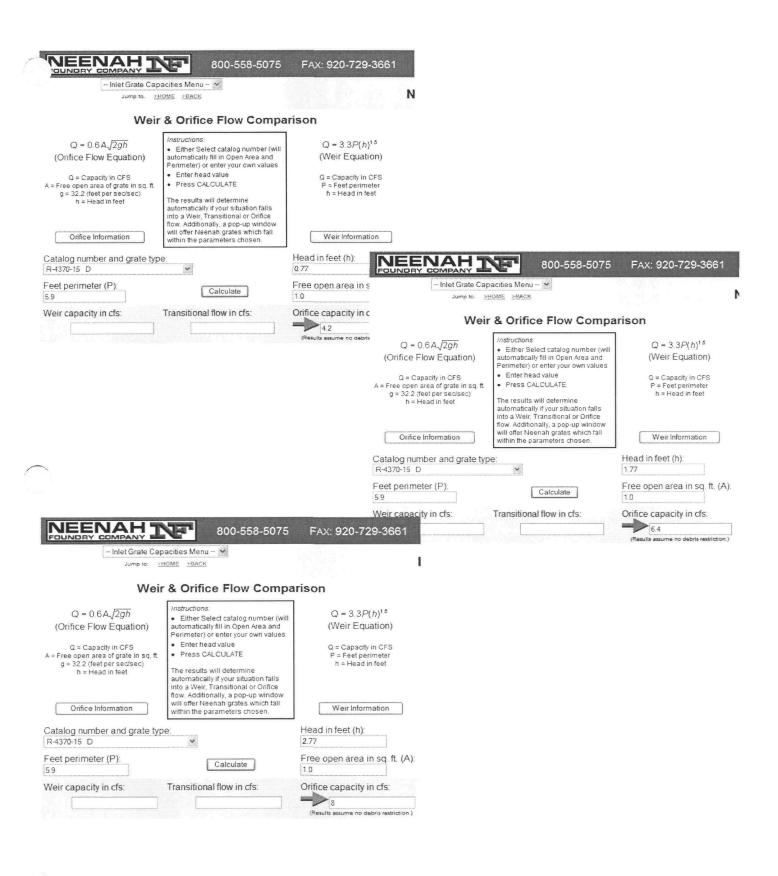
No additional MH storage above the rim elevation

Orifice = 0.61*A*SQRT(2*g*h)

Restrictor Diameter = 4 inches

A = 0.087266 ft^2

C = 0.61 per chicago regulations



No Above ground storage on the monarch site for existing conditions Runoff flows directly into 24" pipe.

-			
S	ideS	lope	1

Area =	0.409	acres
Length =	665	ft

					Above	Above			
		C	Overflow		Ground	Ground	Overflow	Infiltration	Total
Stage	Depth		Depth	XS Area	Storage	Storage	Discharge*	Discharge	Discharge
(ft)	(ft)	(1	ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		(cfs)
5	93	0	0	0	0	0.000	(0.02	0.00 No CB
593	3.5	0.5	0	1.5	997.5	0.023	(0.02	0.02
5	94	1	0	4	2660	0.061	(0.02	0.02 top of channel
594	1.1	1.1	0.1	4.62	3072.3	0.071	10	0.02	10.45
594	1.2	1.2	0.2	5.28	3511.2	0.081	30	0.02	29.53
594	1.3	1.3	0.3	5.98	3976.7	0.091	54	0.02	54.24
594	1.4	1.4	0.4	6.72	4468.8	0.103	83	0.02	83.50
594	1.5	1.5	0.5	7.5	4987.5	0.114	117	0.02	116.69

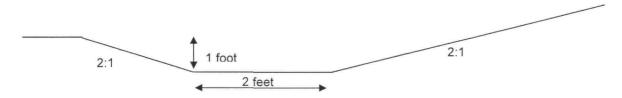
6 ft

0.2 inches/hr

Top width *Overflow Discharge Infiltration

Weir flow

 $Q = 3.3P(h)^{1.5}$ Length = 100



SideSlope 2

Area = 0.961 acres Length ≈ 1281 ft

			•						
					Above	Above			
			Overflow		Ground	Ground	Overflow	Infiltration	Total
Stage	Depth		Depth	XS Area	Storage	Storage	Discharge*	Discharge	Discharge
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		(cfs)
593		0	0	0	0	0.00	0	0.04	0.00 No CB
593.5	(0.5	0	1.5	1921.5	0.04	0	0.04	0.04
594		1	0	4	5124	0.12	0	0.04	0.04 top of channel
594.1		1.1	0.1	4.62	5918.2	0.14	10	0.04	10.47
594.2		1.2	0.2	5.28	6763.7	0.16	30	0.04	29.55
594.3		1.3	0.3	5.98	7660.4	0.18	54	0.04	54.26
594.4		1.4	0.4	6.72	8608.3	0.20	83	0.04	83.52
594.5		1.5	0.5	7.5	9607.5	0.22	117	0.04	116.71

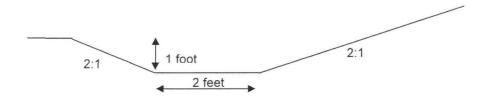
*Overflow Discharge

Weir flow

 $Q = 3.3P(h)^1.5$ Length =

100

Top width 6 ft Infiltration 0.2 inches/hr



SideSlope 3

Area =	0.596	acres
Length =	701	ft

						Above	Above				
				Overflow		Ground	Ground	Overflow	Infiltration	Total	
5	Stage	Depth		Depth	XS Area	Storage	Storage	Discharge*	Discharge	Discharge	
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		(cfs)	
	593		0	0	0	0	0.00		0.02	0.00	No CB
	593.5		0.5	0	1.5	1051.5	0.02		0.02	0.02	
	594		1	0	4	2804	0.06		0.02	0.02	top of channel
	594.1		1.1	0.1	4.62	3238.6	0.07	1	0.02	10.45	
	594.2		1.2	0.2	5.28	3701.3	0.08	3	0.02	29.54	
	594.3		1.3	0.3	5.98	4192	0.10	5	4 0.02	54.24	
	594.4		1.4	0.4	6.72	4710.7	0.11	8	3 0.02	83.50	
	594.5		1.5	0.5	7.5	5257.5	0.12	11	7 0.02	116.69	

*Overflow Discharge

CB - Orifice Flow

Q = 0.6*A*(sqrt(2*g*h))Weir flow

Top width 6 ft

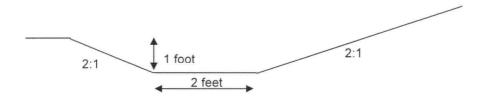
 $Q = 3.3P(h)^1.5$

A =

1.000 R-4370-17D Neenah Grate

Infiltration 0.2 inches/hr

Length = 100



C:	4 -	C		ne	2
21	CI E	c	ЮI	ne.	

Area =	1.557	acres
Length =	1982	ft

9									
					Above	Above			
			Overflow		Ground	Ground	Overflow	Infiltration	Total
Stage	Depth		Depth	XS Area	Storage	Storage	Discharge*	Discharge	Discharge
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		(cfs)
593		0	0	0	0	0.00	0	0.06	0.00 No CB
593.5		0.5	0	1.5	2973	0.07	0	0.06	0.06
594		1	0	4	7928	0.18	0	0.06	0.06 top of channel
594.1		1.1	0.1	4.62	9156.8	0.21	10	0.06	10.49
594.2		1.2	0.2	5.28	10465	0.24	30	0.06	29.57
594.3		1.3	0.3	5.98	11852	0.27	54	0.06	54.28
594.4		1.4	0.4	6.72	13319	0.31	83	0.06	83.54
594.5		1.5	0.5	7.5	14865	0.34	117	0.06	116.73

*Overflow Discharge

CB - Orifice Flow

Weir flow

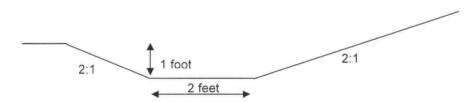
Q = 0.6*A*(sqrt(2*g*h))

A =

rt(2*g*h)) Top width 1.000 R-4370-17D Neenah Grate Infiltration 6 ft

0.2 inches/hr

 $Q = 3.3P(h)^{1.5}$ Length = 100



SideSlope 4

Area =	0.707	acres
Length =	916	ft

					Above	Above				
			Overflow		Ground	Ground	Overflow	Infiltration	Total	
Stage	Depth		Depth	XS Area	Storage	Storage	Discharge*	Discharge	Discharge	
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		(cfs)	
593		0	0	0	0	0.00	(0.03	0.00 No (CB
593.5	5	0.5	0	1.5	1374	0.03	(0.03	0.03	
594	1	1	0	4	3664	0.08	(0.03	0.03 top	of channel
594.	1	1.1	0.1	4.62	4231.9	0.10	10	0.03	10.46	
594.2	2	1.2	0.2	5.28	4836.5	0.11	30	0.03	29.54	
594.3	3	1.3	0.3	5.98	5477.7	0.13	54	1 0.03	54.25	
594.4	4	1.4	0.4	6.72	6155.5	0.14	83	0.03	83.51	
594.	5	1.5	0.5	7.5	6870	0.16	117	7 0.03	116.70	

*Overflow Discharge

CB - Orifice Flow

Weir flow

Q = 0.6*A*(sqrt(2*g*h))

Top width

6 ft

 $Q = 3.3P(h)^{1.5}$ Length =

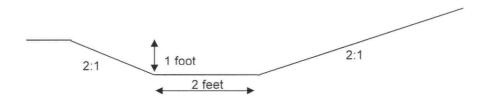
A =

1.000 R-4370-17D Neenah Grate

Infiltration

0.2 inches/hr

100



0	- 1-	-	-	-	_
	ide	 ĸ	n	e	2

Area =	0.187	acres
Length =	250	ft

					Above	Above			
			Overflow		Ground	Ground	Overflow	Infiltration	Total
Stage	Depth		Depth	XS Area	Storage	Storage	Discharge*	Discharge	Discharge
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		(cfs)
593	}	0	0	0	0	0.000		0 0.01	0.00 No CB
593.5	j	0.5	0	1.5	375	0.009		0 0.01	0.01
594		1	0	4	1000	0.023		0 0.01	0.01 top of channel
594.1		1.1	0.1	4.62	1155	0.027	1	0 0.01	10.44
594.2	?	1.2	0.2	5.28	1320	0.030	3	0.01	29.52
594.3	}	1.3	0.3	5.98	1495	0.034	5	4 0.01	54.23
594.4		1.4	0.4	6.72	1680	0.039	8	3 0.01	83.49
594.5	j	1.5	0.5	7.5	1875	0.043	11	7 0.01	116.68

*Overflow Discharge

CB - Orifice Flow

Weir flow

Q = 0.6*A*(sqrt(2*g*h))

Top width

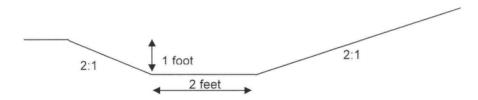
6 ft

 $Q = 3.3P(h)^1.5$

A =

1.000 R-4370-17D Neenah Grate Infiltration 0.2 inches/hr

Length = 100



-		_	40	
9	M	20	lope	1
0	ıu	60	lobe	

Area =	0.257	acres
Length =	350	ft

					Above	Above					
			Overflow		Ground	Ground	Overflow		Infiltration	Total	
Stage	Depth		Depth	XS Area	Storage	Storage	Discharge*		Discharge	Discharge	
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)			(cfs)	
593		0	0	0	0	0.000		0	0.010	0.00	No CB
593.5		0.5	0	1.5	525	0.012		0	0.01	0.01	
594		1	0	4	1400	0.032		0	0.01	0.01	top of channel
594.1		1.1	0.1	4.62	1617	0.037	•	10	0.01	10.45	
594.2		1.2	0.2	5.28	1848	0.042		30	0.01	29.53	
594.3		1.3	0.3	5.98	2093	0.048		54	0.01	54.23	
594.4		1.4	0.4	6.72	2352	0.054	8	83	0.01	83.49	
594.5		1.5	0.5	7.5	2625	0.060	11	17	0.01	116.68	

*Overflow Discharge

CB - Orifice Flow

Weir flow Q = 0.6*A*(sqrt(2*g*h)) Top width

6 ft

 $Q = 3.3P(h)^1.5$

A =

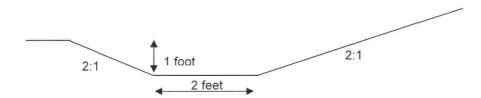
1.000 R-4370-17D Neenah Grate

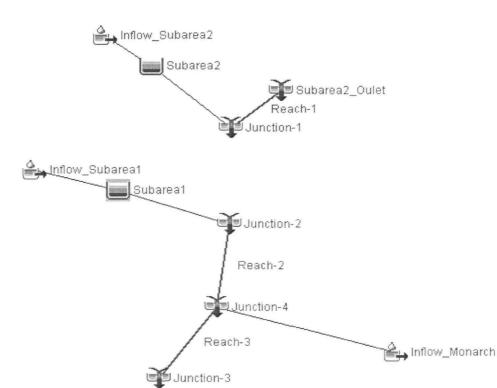
Infiltration

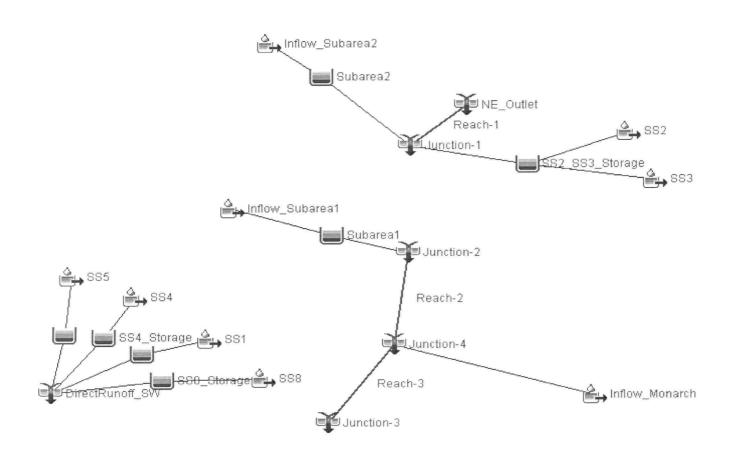
0.2 inches/hr

Length =

100







Stage, Storage Discharge Calculations

			Above Ground	Manhole		Discharge	CB -	Discharge 8"	Total Discharge		Dis -	Discharge 9"	Total	Discharge 6"	Total Dis
Stage	Depth	Depth	Storage	Storage	Total Storage	CB	DOUBLE	Restrictor	8''	Restrictor	10"	Restrictor	Dis 9"	Restrictor	6"
(ft)	(ft)	(ft)	(acre-ft)	(acre-ft)	(acre-ft)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
590.53	0	0	0	0.0000	0.0000	0	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
591.53	1	0	0	0.0003	0.0003	0	0	1.7	1.7	2.7	2.7	2.2	2.2	1.0	1.0
592.53	2	0	0	0.0006	0.0006	0	0	2.4	2.4	3.8	3.8	3.1	3.1	1.4	1.4
593.53	3	0	0	0.0009	0.0009	0	0	3.0	3.0	4.6	4.6	3.7	3.7	1.7	1.7
594.53	4	0	0	0.0012	0.0012	0	0	3.4	3.4	5.3	5.3	4.3	4.3	1.9	1.9
595.53	5	0	0	0.0014	0.0014	0	0	3.8	3.8	6.0	6.0	4.8	4.8	2.1	2.1
595.78	5.25	0	0	0.0015	0.0015	0	0	3.9	3.9	6.1	6.1	5.0	5.0	2.2	2.2
596.5	5.97	0.72	0.08	0.0015	0.0815	4.1	8.2	4.2	4.10	6.5	6.52	5.3	5.28	2.3	2.35
597	6.47	1.22	0.16	0.0015	0.1615	5.3	10.6	4.3	4.35	6.8	6.79	5.5	5.50	2.4	2.44
598	7.47	2.22	1.03	0.0015	1.0315	7.2	14.4	4.7	4.67	7.3	7.30	5.9	5.91	2.6	2.63
599	8.47	3.22	3.52	0.0015	3.5215	8.6	17.2	5.0	4.97	7.8	7.77	6.3	6.29	2.8	2.80

No additional MH storage above the rim elevation

Orifice = 0.6*A*SQRT(2*g*h)

Restrictor Diameter

Diameter		
(inches)		Area (sf)
	8	0.35
	10	0.55
	9	0.44
	6	0.20



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FAX: 920-729-3661

-- Inlet Grate Capacities Menu -- 💌 Jump to: >HOME >BACK

Weir & Orifice Flow Comparison

 $Q = 0.6A\sqrt{2gh}$ (Orifice Flow Equation)

Q = Capacity in CFS A = Free open area of grate in sq. ft. g = 32.2 (feet per sec/sec) h = Head in feet

Orifice Information

instructions:

- · Either Select catalog number (will automatically fill in Open Area and Perimeter) or enter your own values
- Enter head value
- Press CALCULATE

The results will determine automatically if your situation falls into a Weir, Transitional or Orifice flow. Additionally, a pop-up window will offer Neenah grates which fall within the parameters chosen.

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

Q = Capacity in CFS P = Feet nerimeter h = Head in feet

Weir Information

Catalog number and grate type

R-4370-15 D

Feet perimeter (P): 5.9 Weir capacity in cfs:

Calculate

Transitional flow in cfs:

Orifice capacity in cfs:

Head in feet (h):

0.72

(Results assume no debris restriction.)

Free open area in sq. ft. (A):

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 $Q = 3.3P(h)^{1.5}$

(Weir Equation)

Q = Capacity in CFS

P = Feet perimeter

h = Head in feet

-- Inlet Grate Capacities Menu -- 💌 Jump to: >HOME >BACK

Weir & Orifice Flow Comparison

Q = 0.6A /2gh (Orifice Flow Equation)

Q = Capacity in CFS A = Free open area of grate in sq. ft. g = 32.2 (feet per sec/sec) h = Head in feet

Orifice Information

Instructions

- Either Select catalog number (will automatically fill in Open Area and Perimeter) or enter your own values
- Enter head value
- · Press CALCULATE

The results will determine automatically if your situation falls into a Weir, Transitional or Orifice flow Additionally, a pop-up window will offer Neenah grates which fall within the parameters chosen.

Weir Information

Catalog number and grate type R-4370-15 D

Feet perimeter (P): 5.9

Weir capacity in cfs:

Calculate

Transitional flow in cfs

Free open area in sq. ft. (A) 1.0

Orifice capacity in cfs:

Orifice Information

Head in feet (h):

Weir capacity in cfs:

Feet perimeter (P)

R-4370-15 D

Transitional flow in cfs:

Calculate

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

FAX: 920-729-3661

Q = Capacity in CFS P = Feet perimeter h = Head in feet

Weir Information

Catalog number and grate type R-4370-15 D

NEENAH

Q = 0.6A /2ah

(Orifice Flow Equation)

Q = Capacity in CFS

A = Free open area of grate in sq. ft.

g = 32.2 (feet per sec/sec)

h = Head in feet

Orifice Information

FOUNDRY COMPANY

Feet perimeter (P):

Weir capacity in cfs:

Calculate

Transitional flow in cfs.

Orifice capacity in cfs:

1.22

Head in feet (h):

(Results assume no debris restriction.)

Free open area in sq. ft. (A):

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800-558-5075

Weir & Orifice Flow Comparison

· Either Select catalog number (will

automatically fill in Open Area and

Perimeter) or enter your own values

automatically if your situation falls

into a Weir, Transitional or Orifice

flow. Additionally, a pop-up window

will offer Neenah grates which fall

within the parameters chosen.

FAX: 920-729-3661

Inlet Grate Capacities Menu -- 💌

Jump to: <u>>HOME</u> >BACK

-- Inlet Grate Capacities Menu -- 🛰

Jump to >HOME >BACK

instructions

· Enter head value

Press CALCULATE

The results will determine

Weir & Orifice Flow Comparison

 $Q = 0.6A\sqrt{2gh}$ (Orifice Flow Equation)

Q = Capacity in CFS A = Free open area of grate in sq. ft. g = 32.2 (feet per sec/sec) h = Head in feet

Catalog number and grate type

instructions:

- · Either Select catalog number (will automatically fill in Open Area and Perimeter) or enter your own values
- Enter head value
- Press CALCULATE

The results will determine automatically if your situation falls into a Weir, Transitional or Orifice flow. Additionally, a pop-up window will offer Neenah grates which fall within the parameters chosen

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

Q = Capacity in CFS P = Feet perimeter h = Head in feet

Weir Information

Head in feet (h):

3.22

Free open area in sq. ft. (A):

Orifice capacity in cfs:

(Results assume no debris restriction.)

100		1000
Λ		2
~	100	/

							Discharge	lotal	Discharge	lotal
				Manhole		Discharge	2.5"	Discharge	4"	Discharge ·
Stage	Depth	Depth	Storage	Storage	Total Storage	CB	Restrictor	2.5"	Restrictor	4"
(ft)	(ft)	(ft)	(acre-ft)	(acre-ft)	(acre-ft)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
592.48	0	0	0	0.0000	0.0000	0	0.00	0.00	0.00	0.00
593.48	1	0	0	0.0003	0.0003	0	0.17	0.17	0.43	0.43
594.48	2	0	0	0.0006	0.0006	0	0.24	0.24	0.60	0.60
595.48	3	0	0	0.0009	0.0009	0	0.29	0.29	0.74	0.74
596.48	4	0	0	0.0012	0.0012	0	0.33	0.33	0.85	0.85
597.23	4.75	0	0	0.0014	0.0014	0	0.36	0.36	0.93	0.93
598	5.52	0.77	0.01	0.0014	0.0114	4.2	0.39	0.39	1.00	1.00
599	6.52	1.77	0.24	0.0014	0.2414	6.4	0.43	0.43	1.09	1.09
600	7.52	2.77	1.17	0.0014	1.1714	8	0.46	0.46	1.17	1.17
				No addition	onal MH storage	e above the	rim elevation			

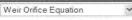
Orifice = 0.6*A*SQRT(2*g*h)
Restrictor
Diameter
(inches) Area (sf)
2.5 0.03

4 0.09



800-558-5075

FAX: 920-729-3661



Jump to: >HOME >BACK

Weir & Orifice Flow Comparison

 $Q = 0.6A\sqrt{2gh}$ (Orifice Flow Equation)

Q = Capacity in CFS A = Free open area of grate in sq. ft. g = 32.2 (feet per sec/sec) h = Head in feet

Instructions · Either Select catalog number (will

automatically fill in Open Area and Perimeter) or enter your own values

- · Enter head value
- Press CALCULATE

The results will determine automatically if your situation falls

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

Q = Capacity in CFS P = Feet perimeter h = Head in feet

***************************************	Jump to: >HOME >BA	CK		
Weir	Orifice Equation			
NEENA FOUNDRY COME	ΉŒ	800-558-507	5 FAX: 920-7	729-3661
			(Results assume no d	lebris restriction.)
			4.2	
Weir capacity in cfs:	Transitional	flow in cfs:	Orifice capacity	in cfs:
6.0		arculate J	1.0	
Feet perimeter (P):	[[Calculate	Free open area	in sq. ft. (A)
R-4370-17 D	*		0.77	
Catalog number and grate	e type:		Head in feet (h):	
Orifice Information	flow. Additiona will offer Neen	ansitional or Orifice Ily, a pop-up window ah grates which fall ameters chosen.	WeirInfor	mation

Weir & Orifice Flow Comparison · Either Select catalog number (will

automatically fill in Open Area and Perimeter) or enter your own values Enter head value

automatically if your situation falls into a Weir, Transitional or Orifice flow. Additionally, a pop-up window will offer Neenah grates which fall

within the parameters chosen

Calculate

· Press CALCULATE

The results will determine

 $Q = 0.6 A \sqrt{2gh}$ (Orifice Flow Equation)

Q = Capacity in CFS A = Free open area of grate in sq. ft. g = 32.2 (feet per sec/sec) h = Head in feet

Orifice Information

Catalog number and grate type: R-4370-17 D

Feet perimeter (P): 6.0

Weir capacity in cfs: Transitional flow in cfs:

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

Q = Capacity in CFS P = Feet perimeter h = Head in feet

Weir Information

Head in feet (h).

Free open area in sq. ft (A): 1.0

(Results assume no debris restriction.)

Orifice capacity in cfs:

800-558-5075

FAX: 920-729-3661

Weir Orifice Equation Jump to: >HOME >BACK

Weir & Orifice Flow Comparison

 $Q = 0.6A\sqrt{2gh}$ (Orifice Flow Equation)

Q = Capacity in CFS A = Free open area of grate in sq. ft. g = 32.2 (feet per sec/sec) h = Head in feet

· Either Select catalog number (will automatically fill in Open Area and Perimeter) or enter your own values

· Enter head value

Instructions:

Press CALCULATE

The results will determine automatically if your situation falls into a Weir, Transitional or Orifice flow. Additionally, a pop-up window will offer Neenah grates which fall within the parameters chosen.

 $Q = 3.3P(h)^{1.5}$ (Weir Equation)

Q = Capacity in CFS P = Feet perimeter h = Head in feet

Weir Information

	Catalog	number	and	grate	type:
--	---------	--------	-----	-------	-------

R-4370-17 D

Orifice Information

Feet perimeter (P)

Weir capacity in cfs:

Transitional flow in cfs:

Calculate

Head in feet (h):

Free open area in sq. ft. (A):

Orifice capacity in cfs:

(Results assume no debris restriction.)

Monarch Area = 1.6 acres

			PP	Above Ground	Manhole	Total Storage	Total Storage	Discharge	Discharge	Total	
Stage	Depth	Depth	Storage	Storage	Storage	w/ PP	w/ No PP	CB	Restrictor	Discharge	
(ft)	(ft)	(ft)	(acre-ft)	(acre-ft)	(acre-ft)	(acre-ft)	(acre-ft)	(cfs)	(cfs)	(cfs)	
589.22	0	0	0	0	0.0000	0.0000	0.0000	0	0	0	
590.22	1	0	0	0	0.0003	0.0003	0.0003	0	0.96	0.96	
591.22	2	0	0	0	0.0006	0.0006	0.0006	0	1.36	1.36	
592.31	3.09	0	0	0	0.0009	0.0009	0.0009	0	1.69	1.69 Bottom of Porous Pavement	t
593.31	4.09	0	0.48	0	0.0012	0.4812	0.0012	0	1.94	1.94	
594.31	5.09	0	0.96	0	0.0015	0.9615	0.0015	0	2.17	2.17 PP 6" thick	
594.81	5.59	0	1.04	0	0.0015	1.0415	0.0015	0	2.27	2.27 CB Rim	
595	5.78	0.19	1.04	0	0.0015	1.0415	0.0015	1.6	2.31	2.31	
596	6.78	1.19	1.04	0.34	0.0015	1.3815	0.3415	5.3	2.50	2.50	

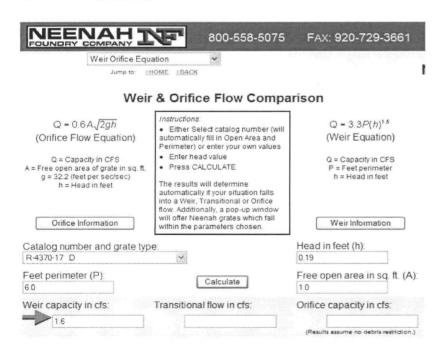
No additional MH storage above the rim elevation

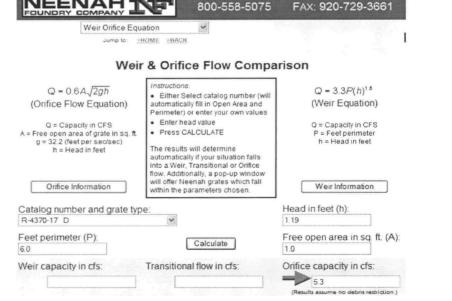
Orifice = 0.6*A*SQRT(2*g*h)

Restrictor Diameter =

6 inches

A = 0.196 ft^2





Area = 0.409 acres Length = 665 ft

0														
			Underg	r	Above	Above								
		Overflow	ound		Ground	Ground	Under	ground	Total	Discharge	Overflow	Infiltration	Total	
Stage	Depth	Depth	Depth	XS Area	Storage	Storage	Sto	rage	Storage	CB	Discharge*	Discharge	Discharge	
(ft)	(ft)	(ft)	(ft)	(ft^2)	(ft^3)	(acre-ft)	(ft^3)	(acre-ft)	(acre-ft)	(cfs)	(cfs)	(cfs)	(cfs)	
591	0	0		0 0	0	0	0	0.00	0.00	0.00	0	0.03	0	
592	. 0	0		1 (0	0	798	0.02	0.02	0.00	0	0.03	0.03	
593	0	0		2 0	0	0.00	1596	0.04	0.04	0.00	0	0.03	0.03 No CB	
593.5	0.5	0		1.75	1163.75	0.03	1596	0.04	0.06	3.40	0	0.03	0.03	
594	1	0		5	3325	0.08	1596	0.04	0.11	4.81	0	0.03	0.03 top of channel	
594.1	1.1	0.1		5.83	3876.95	0.09	1596	0.04	0.13	5.05	10	0.03	10.47	
594.2	1.2	0.2		6.72	4468.8	0.10	1596	0.04	0.14	5.27	30	0.03	29.55	
594.3	1.3	0.3		7.67	5100.55	0.12	1596	0.04	0.15	5.49	54	0.03	54.26	
594.4	1.4	0.4		8.68	5772.2	0.13	1596	0.04	0.17	5.70	83	0.03	83.51	
594.5	1.5	0.5		9.75	6483.75	0.15	1596	0.04	0.19	5.90	117	0.03	116.70	

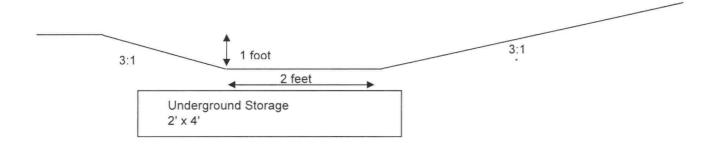
*Overflow Discharg CB - Orifice Flow

Weir flow Q = 0.6*A*(sqrt(2*g*h))

 $Q = 3.3P(h)^{1.5}$ A = 1.000 R-4370-17D Neenah Grate

Length = 100

Top width 8 ft
Infiltration 0.25 inches/hr



SideSlope	1
Aroa =	

Length =

0.409 acres 665 ft

1.9

2

					Above	Above			
		(Overflow		Ground	Ground	Overflow	Infiltration	Total
Stage	Depth	1	Depth	XS Area	Storage	Storage	Discharge*	Discharge	Discharge
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		
593		0	0	0	0	0.00	0	0.05	0.00 No CB
593.5	().5	0	2.75	1828.8	0.04	0	0.05	0.05
594		1	0	7	4655	0.11	0	0.05	0.05
594.5	1	1.5	0	12.75	8478.8	0.19	0	0.05	0.05 top of channel
594.6	1	1.6	0.1	14.08	9363.2	0.21	10	0.05	10.49
594.7	1	1.7	0.2	15.47	10288	0.24	30	0.05	29.57
594.8	1	1.8	0.3	16.92	11252	0.26	54	0.05	54.27

12256

13300

*Overflow Discharge

CB - Orifice Flow

Top width Infiltration

0.05

0.05

83

117

13 ft

0.25 inches/hr

83.53

116.72

Weir flow $Q = 3.3P(h)^{1.5}$

594.9

595

Q = 0.6*A*(sqrt(2*g*h))A =

18.43

20

0.4

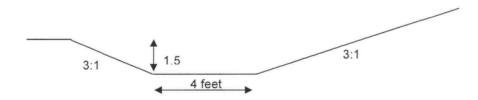
0.5

1.000 R-4370-17D Neenah Grate

0.28

0.31

Length = 100



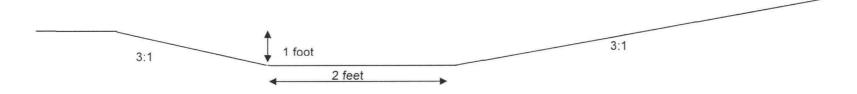
Area = 0.961 acres Length = 1281 ft

					Above	Above					Total
			Overflow		Ground	Ground	Discharge	Overflow	Infiltration	Total	Discharge
Stage	Depth		Depth	XS Area	Storage	Storage	CB	Discharge*	Discharge	Discharge	No CB
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
593		0	0	C	0	0.00	0.00	0	0.06	0.06	CB on botte 0.06
593.5	5	0.5	0	1.75	2241.8	0.05	3.40	0	0.06	3.46	0.06
594	ļ.	1	0	5	6405	0.15	4.81	0	0.06	4.87	top of chan 0.06
594.1		1.1	0.1	5.83	7468.2	0.17	5.05	10	0.06	15.54	10.49
594.2	2	1.2	0.2	6.72	8608.3	0.20	5.27	30	0.06	34.85	29.58
594.3	3	1.3	0.3	7.67	9825.3	0.23	5.49	54	0.06	59.77	54.28
594.4	1	1.4	0.4	8.68	11119	0.26	5.70	83	0.06	89.24	83.54
594.5	5	1.5	0.5	9.75	12490	0.29	5.90	117	0.06	122.63	116.73

*Overflow Discharge CB - Orifice Flow Weir flow Q = 0.6*A*(sqrt(2*g*h

Weir flow Q = 0.6*A*(sqrt(2*g*h)) Top width 8 ft $Q = 3.3P(h)^{1.5}$ A = 1.000 R-4370-17D Neenah Grate Infiltration 0.25 inches/hr

Length = 100 Estimate



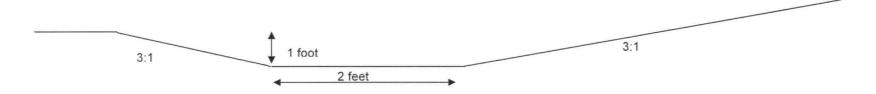
Area =	0.596	acres
Length =	701	ft

					Above	Above					Total
			Overflow		Ground	Ground		Overflow	Infiltration	Total	Discharge
Stage	Depth		Depth	XS Area	Storage	Storage	Discharge CB	Discharge*	Discharge	Discharge	No CB
(ft)	(ft)		(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)	(cfs)		(cfs)	(cfs)
592		0	0	0	0	0.00	0.00	0	0.03	0.03 CB on bot	ttı 0.03
592.5		0.5	0	1.75	1226.8	0.03	3.40	0	0.03	3.44	0.03
593		1	0	5	3505	0.08	4.81	0	0.03	4.85 top of cha	n 0.03
593.1		1.1	0.1	5.83	4086.8	0.09	5.05	10	0.03	15.52	10.47
593.2		1.2	0.2	6.72	4710.7	0.11	5.27	30	0.03	34.82	29.55
593.3		1.3	0.3	7.67	5376.7	0.12	5.49	54	0.03	59.75	54.26
593.4		1.4	0.4	8.68	6084.7	0.14	5.70	83	0.03	89.21	83.52
593.5		1.5	0.5	9.75	6834.8	0.16	5.90	117	0.03	122.60	116.71

*Overflow Discharge CB - Orifice Flow Weir flow Q = 0.6*A*(sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2*sqrt(2

Q = 0.6*A*(sqrt(2*g*h)) Q = 0.6*A*(sqrt(2*g*h)) A = 1.000 R-4370-17D Neenah Grate O.25 inches/hr

 $Q = 3.3P(h)^{1.5}$ Length = 100



SideSlope 2 and 3

Area =	1.557	acres
Length =	1982	ft

3									
				Above	Above	Overflow			
		Overflow	1	Ground	Ground	Discharge	Infiltration	Total	
Stage	Depth	Depth	XS Area	Storage	Storage	*	Discharge	Discharge	
(ft)	(ft)	(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		(cfs)	
593		0 0	0	0	0.00	0	0.09	0.00 No Catch Basin	
593.5	0.	5 0	1.75	3468.5	0.08	0	0.09	0.09	
594		1 0	5	9910	0.23	0	0.09	0.09 top of channel	
594.1	1.	1 0.1	5.83	11555	0.27	10	0.09	10.53	
594.2	1.	2 0.2	6.72	13319	0.31	30	0.09	29.61	
594.3	1.	3 0.3	7.67	15202	0.35	54	0.09	54.32	
594.4	1.	4 0.4	8.68	17204	0.39	83	0.09	83.58	
594.5	1.	5 0.5	9.75	19325	0.44	117	0.09	116.76	

*Overflow Discharge CB - Orifice Flow

Weir flow Q = 0.6*A*(sqrt(2*g*h)) Top width 8 ft $Q = 3.3P(h)^1.5$ A = 1.000 R-4370-17D Neenah Grate Infiltration 0.25 inches/hr

Length = 100 Estimate



Area = 0.707 acres Length = 916 ft

			Underg	r		Above	Above									
		Overflow	ound	XS	3	Ground	Ground	Under	ground	Total	Overflow	Total	Infiltration	Total		
Stage	Depth	Depth	Depth	Are	ea	Storage	Storage	Sto	rage	Storage	Discharge*	Dis - 6"	Discharge	Discharge	No CB	
(ft)	(ft)	(ft)	(ft)	(ft ^r	^2)	(ft^3)	(acre-ft)	(ft^3)	(acre-ft)	(acre-ft)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	
591				0	0	0	0.00	0	0.00	0.00	C	0	0.04	0	0	
592				1	0	0	0.00	1099.2	0.03	0.03	C	0	0.04	0.04	0.04	
593	0	0	1	2	0	0	0.00	2198.4	0.05	0.05	C	0.00	0.04	0.04	0.04 No	CB
593.5	0.5	0			1.75	1603	0.04	2198.4	0.05	0.09	C	0.68	0.04	0.72	0.04	
594	1	0	1		5	4580	0.11	2198.4	0.05	0.16	C	0.96	0.04	1.00	0.04 Top	o Chann
594.1	1.1	0.1			5.83	5340.28	0.12	2198.4	0.05	0.17	10	1.01	0.04	11.49	10.48	
594.2	1.2	0.2	!		6.72	6155.52	0.14	2198.4	0.05	0.19	30	1.05	0.04	30.61	29.56	
594.3	1.3	0.3		5	7.67	7025.72	0.16	2198.4	0.05	0.21	54	1.10	0.04	55.36	54.27	
594.4	1.4	0.4		-	8.68	7950.88	0.18	2198.4	0.05	0.23	83	1.14	0.04	84.66	83.53	
594.5	1.5	0.5			9.75	8931	0.21	2198.4	0.05	0.26	117	1.18	0.04	117.89	116.72	

*Overflow Discharg CB - Orifice Flow

100

Q = 0.6*A*(sqrt(2*g*h))Weir flow

 $Q = 3.3P(h)^1.5$ A =

Length =

1.000 R-4370-17D Neenah Grate

Top width

8 ft

Infiltration

0.25 inches/hr

0.20

Proposed Conditions Sacramento SS Cross-Section

2' x 4' - 30% voids

Orifice = Restrictor Diameter

(inches) Area (sf) 6

2.1 2 feet Underground Storage

Area =	0.187	acres
Length =	250	ft

						Above	Above					
			0	verflow		Ground	Ground		Overflow	Infiltration	Total	
Sta	age	Depth	D	epth	XS Area	Storage	Storage	Discharge CB	Discharge*	Discharge	Discharge	No CB Discharge
(ft))	(ft)	(ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
	593		0	0	0	0	0.00	0.00	C	0.01	0.01 CB on bott	0.012
	593.5		0.5	0	1.75	437.5	0.01	3.40	C	0.01	3.42	0.012
	594		1	0	5	1250	0.03	4.81	C	0.01	4.83 top of char	0.012
	594.1		1.1	0.1	5.83	1457.5	0.03	5.05	10	0.01	15.50	10.447
	594.2		1.2	0.2	6.72	1680	0.04	5.27	30	0.01	34.80	29.528
	594.3		1.3	0.3	7.67	1917.5	0.04	5.49	54	0.01	59.73	54.236
	594.4		1.4	0.4	8.68	2170	0.05	5.70	83	0.01	89.19	83.496
	594.5		1.5	0.5	9.75	2437.5	0.06	5.90	117	0.01	122.58	116.684

*Overflow Discharge Weir flow

CB - Orifice Flow

Q = 0.6*A*(sqrt(2*g*h))

1.000 R-4370-17D Neenah Grate A =

 $Q = 3.3P(h)^1.5$

Length = 100

Top width 8 ft Infiltration 0.25 inches/hr



Area = 0.257 acres Length = 412 ft

					Above	Above					
		Ov	erflow		Ground	Ground		Overflow	Infiltration	Total	
Stage	Depth	De	pth X	S Area	Storage	Storage	Discharge CB	Discharge*	Discharge	Discharge	No CB Discharge
(ft)	(ft)	(ft)	(ft	t^2)	(ft^3)	(acre-ft)	(cfs)	(cfs)		(cfs)	(cfs)
592	2	0	0	0	0	0.000	0.00		0.01	0.01 CB on bot	ti 0.014
592.5	5	0.5	0	0.375	154.5	0.004	3.40	1	0.01	3.42	0.014
593	3	1	0	1.5	618	0.014	4.81		0.01	4.83 top of cha	n 0.014
593.1	1	1.1	0.1	1.815	747.78	0.017	5.05	1	0.01	15.50	10.450
593.2	2	1.2	0.2	2.16	889.92	0.020	5.27	3	0.01	34.80	29.530
593.3	3	1.3	0.3	2.535	1044.4	0.024	5.49	5-	4 0.01	59.73	54.239
593.4	1	1.4	0.4	2.94	1211.3	0.028	5.70	8	3 0.01	89.20	83.498
593.5	5	1.5	0.5	3.375	1390.5	0.032	5.90	11	7 0.01	122.58	116.687

*Overflow Discharge

CB - Orifice Flow

Weir flow $Q = 3.3P(h)^{1.5}$

Length =

Q = 0.6*A*(sqrt(2*g*h))

A =

100

1.000 R-4370-17D Neenah Grate

Top width Infiltration 6 ft

0.25 inches/hr



SideSlope 5 and 6

Area = 0.187 acres Length = 250 ft

						Above	Above			
		(Overflow	XS Area	XS Area	Ground	Ground	Overflow	Infiltration	Total
Stage	Depth	[Depth	Sacramento	Monarch	Storage	Storage	Discharge*	Discharge	Discharge
(ft)	(ft)	((ft)	(ft^2)	(ft^2)	(ft^3)	(acre-ft)	(cfs)		(cfs)
593	3	0	0	0	0	0	0.000	(0.03	0.00 No CB
593.5	5	0.5	0	1.75	0.375	531.25	0.012		0.03	0.03
594	1	1	0	5	1.5	1625	0.037	(0.03	0.03 top of channel
594.1	I	1.1	0.1	5.83	1.815	1911.3	0.044	10	0.03	10.46
594.2	2	1.2	0.2	6.72	2.16	2220	0.051	30	0.03	29.54
594.3	3	1.3	0.3	7.67	2.535	2551.2	0.059	54	1 0.03	54.25
594.4	1	1.4	0.4	8.68	2.94	2905	0.067	83	0.03	83.51
594.5	5	1.5	0.5	9.75	3.375	3281.3	0.075	11	7 0.03	116.70

*Overflow Discharge

CB - Orifice Flow

Weir flow Q = 0.6*A*(sqrt(2*g*h))

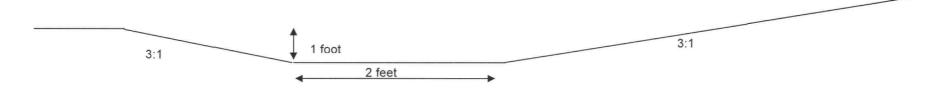
 $Q = 3.3P(h)^1.5$

A =

1.000 R-4370-17D Neenah Grate

Length = 100

Proposed Conditions Sacramento SS Cross-Section





Area = 0.129 acres Length = 320 ft

					Above	Above						
		O	erflow		Ground	Ground		Overflow	Inf	iltration	Total	
Stage D	epth	De	epth XS	Area	Storage	Storage	Discharge CB	Discharge*	Dis	scharge	Discharge	No CB Discharge
(ft) (ft	t)	(ft)) (ft^	2)	(ft^3)	(acre-ft)	(cfs)	(cfs)			(cfs)	(cfs)
593		0	0	0	0	0.000	0.00		0	0.01	0.01 CB on bot	t ₁ 0.011
593.5		0.5	0	0.375	120	0.003	3.40		0	0.01	3.42	0.011
594		1	0	1.5	480	0.011	4.81		0	0.01	4.83 top of cha	n 0.011
594.1		1.1	0.1	1.815	580.8	0.013	5.05		1	0.01	6.10	1.055
594.2		1.2	0.2	2.16	691.2	0.016	5.27		3	0.01	8.24	2.963
594.3		1.3	0.3	2.535	811.2	0.019	5.49		5	0.01	10.92	5.434
594.4		1.4	0.4	2.94	940.8	0.022	5.70		8	0.01	14.06	8.360
594.5		1.5	0.5	3.375	1080	0.025	5.90	1	2	0.01	17.58	11.678

*Overflow Discharge Weir flow

CB - Orifice Flow

Q = 0.6*A*(sqrt(2*g*h))

A = 1.000 R-4370-17D Neenah Grate

 $Q = 3.3P(h)^1.5$ 10 Top width Infiltration

6 ft 0.25 inches/hr

Length =

			-
Sid	eS	ope	1

Area =	0.257	acres
Length =	350	ft

					Above	Above					
		C	verflow		Ground	Ground		Overflow	Infiltration	Total	
Stage	Depth		epth 2	XS Area	Storage	Storage	Discharge CB	Discharge*	Discharge	Discharge	No CB Discharge
(ft)	(ft)	(1	ft)	(ft^2)	(ft^3)	(acre-ft)	(cfs)	(cfs)		(cfs)	(cfs)
59	93	0	0	0	0	0.000	0.00	0	0.02	0.02 CB on bott	0.016
593.	.5	0.5	0	1.75	612.5	0.014	3.40	0	0.02	3.42	0.016
59	4	1	0	5	1750	0.040	4.81	0	0.02	4.83 top of char	0.016
594.	.1	1.1	0.1	5.83	2040.5	0.047	5.05	1	0.02	6.11	1.060
594.	.2	1.2	0.2	6.72	2352	0.054	5.27	3	0.02	8.24	2.968
594.	.3	1.3	0.3	7.67	2684.5	0.062	5.49	5	0.02	10.93	5.439
594.	.4	1.4	0.4	8.68	3038	0.070	5.70	8	0.02	14.06	8.365
594.	.5	1.5	0.5	9.75	3412.5	0.078	5.90	12	0.02	17.58	11.683

Top width

Infiltration

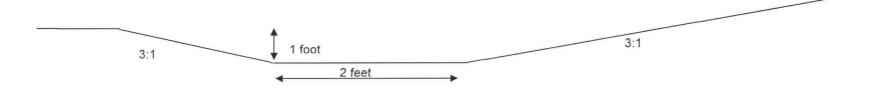
8 ft

0.25 inches/hr

*Overflow Discharge CB - Orifice Flow
Weir flow Q = 0.6*A*(sqrt(2*g*h))

 $Q = 3.3P(h)^{1.5}$ A = 1.000 R-4370-17D Neenah Grate

Length = 10



SideSlope 7 and 8

Area = 0.386 acres Length = 670 ft

			Un	derar			Above	Above								
		Ov	erflow our	nd	XS Area	XS Area	Ground	Ground	Under	ground	Total	Overflow	Infiltration	Total	No CB	
Stage	Depth	De	pth De	pth	Sacramento	Monarch	Storage	Storage	Sto	rage	Storage	Discharge*	Discharge	Discharge	Discharge	
(ft)	(ft)	(ft)	(ft)		(ft^2)	(ft^2)	(ft^3)	(acre-ft)		_	(acre-ft)	(cfs)		(cfs)	(cfs)	
591		0	0	0	0	0	0	0	0	0.00	0.00	0	0.03	0	0	
592		0	0	1	0	0	0	0	804	0.02	0.02	0	0.03	0.03	0.027	
593		0	0	2	C	0	0	0.000	1608	0.04	0.04	0	0.03	0.03	0.027 No CB	
593.5	0.	5	0		1.75	0.375	1423.75	0.033	1608	0.04	0.07	0	0.03	0.71	0.027	
594		1	0		5	1.5	4355	0.100	1608	0.04	0.14	0	0.03	0.99	0.027 Top Channel	
594.1	1.	1	0.1		5.83	1.815	5122.15	0.118	1608	0.04	0.15	10	0.03	11.47	10.463	
594.2	1.	2	0.2		6.72	2.16	5949.6	0.137	1608	0.04	0.17	30	0.03	30.60	29.543	
594.3	1.	3	0.3		7.67	2.535	6837.35	0.157	1608	0.04	0.19	54	0.03	55.35	54.252	
594.4	1.	4	0.4		8.68	2.94	7785.4	0.179	1608	0.04	0.22	83	0.03	84.65	83.511	
594.5	1.	5	0.5		9.75	3.375	8793.75	0.202	1608	0.04	0.24	116.7	0.03	117.88	116.700	

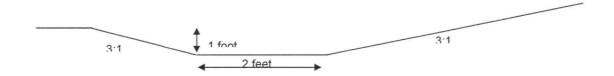
*Overflow Discharge CB - Orifice Flow

Weir flow Q = 0.6*A*(sqrt(2*g*h))

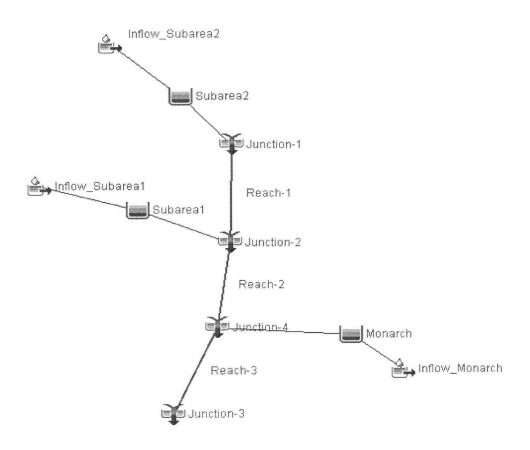
 $Q = 3.3P(h)^{\Lambda}1.5$ $A = 1.000 R-4370-17D Neenah Grate Orifice = <math>0.6^{\star}A^{\star}SQRT(2^{\star}g^{\star}h)$ Length = 100 Restrictor Area (sf)

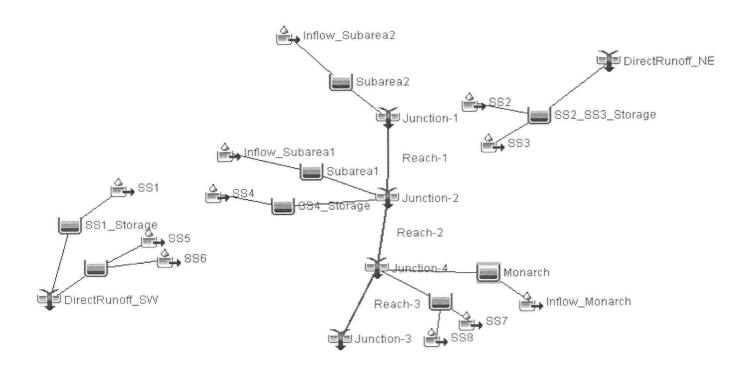
6 0.20

Proposed Conditions Sacramento SS Cross-Section









Pipe Design Calculations

			ell Celotex					green	cells a	re differe	nt than s	hown on o	frawings							
	Mittag/MK																			
	gust 12, 20																			
Project: I	loneywell (Celotex																		
Structure	RIM (ft.)	Depth of Cover (ft.)	Upstream invert (ft.)		(ft.)	Slope (ft./ft.)	Manning's n	size	Pipe area (ft.^2)		Design flow (cfs)	(ft./s.)	Calculated flow (cfs)		Length (ft)		Pipe Material	# Manholes	# CBs	# Connections
CB-4	597.43		594.83			0.0032	0.012				1.1	2.79		Class IV	736		Class IV RCCP	7	7	1
MH-6	599.90	5.23	593.67			0.0032	0.012	12				2.79		ESVCP	956		ESCVP			
MH-5	600.50	6.98	592.52			0.0032	0.012		0.79		1.1	2.79		ESVCP	20		ESCVP			
MH-4	597.83	5.47	591.36	590.32	231	0.0045	0.012	12	0.79	591.52	1.1	3.31	2.60	ESVCP	604	21	Class IV RCCP			-
CB-7	592.35	1.60	589.75	589.16	185	0.0032	0.012	12	0.79	590.36	1.1	2.79	2.19	Class IV	2316					
CB-6	593.58	3.52	589.06	588.35	221	0.0032	0.012	12	0.79	589.55	1.1	2.79	2.19	Class IV						
CB-3	595.78	3.72	590.56	590.53	10	0.0035	0.012	18	1.77	592.23	3.5	3.82	6.75	ESVCP	desgin flow = half over	all flow				
CB-2	595.78	3.76	590.53	590.34	10	0.0190	0.012	18	1.77	592.04	7	8.90	15.73	ESVCP						
MH-3	596.06	5.96	588.35	587.49	245	0.0035	0.012	21	2.41	589.44	8.1	4.23	10.18	Class IV						
CB-1	594,81	4.59	589.22	589.10	10	0.0120	0.012	12	0.79	590.30	4.1	5.40	4.24	ESVCP						
MH-2	594.88	5.64	587.49	586.17	204	0.0065	0.012	21	2.41	588.12	12.2	5.77	13.88	Class IV						
CB-5	591.40	3.10	587.30	586.64	55	0.0120	0.012	12	0.79	587.84	1.1	5.40	4.24	ESVCP						
MH-1A	596.89	8.97	586.17	585.48	105	0.0065	0.012	21	2.41	587.43	12.2	5.77	13.88	Class IV						
MH-1	593.00	8.77	582.48	580.76	50	0.0344	0.012	21	2.41	582.71	12.2	13.27	31.92	Class IV						
					2316															

Time of Concentration Calculations

Time of Concentration & Travel T	ime Workshee	t			
Note: Space for as many as tw			for each workshe	eet.	
Include a map, schematic				2004-0.00	
		_			
Sheet Flow (Applicable to T c only)		Segment ID			
1.) Surface Description (use code A-J, table 3-1)			Α		
2.) Manning's roughness coeff., n (table 3-1)			0.011	0	
3.) Flow length, L (total L <= 300 ft)		ft	300		
4.) Two-yr 24-hr rainfall, P ₂ (Si	oux Falls IDF)	in	3.04	2.688	
5.) Land Slope, s		ft/ft	0.0077		
6.)	Compute T _t	hr	0.073093054 +	0	= 0.073093
$T_{r} = \frac{0.007 (nL)^{0.8}}{P_{2}^{0.5} s^{0.4}}$					
1 2 3					
Shallow concentrated flow		Segment ID			
7.) Surface description (P=paved or U=unpaved)			U		
8.) Flow length, L		ft	480		
9.) Watercourse slope, s		ft/ft	0.0077		
10.) Average velocity, v (figure 3-1)		ft/s	1.415796629		
11.)	Compute T _t	hr	0.094175484 +	0	= 0.094175
$T_{t} = \frac{L}{3600 \text{ v}}$		1			
3600 v					
					v.
(Channel Flow (transzoidal channel)		Segment ID			
Channel Flow (trapezoidal channel)		Segment ID			
12a.) Ditch side slope 1		Segment ID			
12a.) Ditch side slope 1 12b.) Ditch side slope 2		Segment ID			
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width					
12a.) Ditch side slope 1 12b.) Ditch side slope 2		ft	0	0	
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a		ft ft	0	0	
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w	Compute r	ft ft ft² ft	0		
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w 14.) Hydraulic Radius, r = a/P _w	Compute r	ft ft' ft'² ft ft			
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w 14.) Hydraulic Radius, r = a/P _w 15.) Channel Slope, s	Compute r	ft ft ft² ft	0		
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w 14.) Hydraulic Radius, r = a/P _w 15.) Channel Slope, s 16.) Manning's roughness coeff., n	Compute r	ft ft' ft'² ft ft	0		
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w 14.) Hydraulic Radius, r = a/P _w 15.) Channel Slope, s 16.) Manning's roughness coeff., n	Security of Province Co.	ft ft ft² ft ft	0	0	
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w 14.) Hydraulic Radius, r = a/P _w 15.) Channel Slope, s	Compute r Compute v	ft ft' ft'² ft ft	0		
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P_w 14.) Hydraulic Radius, $r = a/P_w$ 15.) Channel Slope, s 16.) Manning's roughness coeff., n 17.) $v = \frac{1.49r^{2/3}s^{1/2}}{n}$	Security of Province Co.	ft ft ft² ft ft	0	0	
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w 14.) Hydraulic Radius, $r = a/P_w$ 15.) Channel Slope, s 16.) Manning's roughness coeff., n 17.) $v = \frac{1.49r^{2/3}s^{1/2}}{n}$ 18.) Flow Length, L	Compute v	ft ft ² ft ft ft/ft	0	0	
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w 14.) Hydraulic Radius, $r = a/P_w$ 15.) Channel Slope, s 16.) Manning's roughness coeff., n 17.) $v = \frac{1.49r^{2/3}s^{1/2}}{n}$ 18.) Flow Length, L	Security of Province Co.	ft ft ² ft ft ft/ft	0	0	= 0
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P_w 14.) Hydraulic Radius, $r = a/P_w$ 15.) Channel Slope, s 16.) Manning's roughness coeff., n 17.) $v = \frac{1.49r^{2/3}s^{1/2}}{n}$ 18.) Flow Length, L 19.) $T_r = \frac{L}{3600 \ v}$	Compute v Compute T_t	ft ft² ft ft/ft ft/s ft/s	0	0	= 0
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P _w 14.) Hydraulic Radius, $r = a/P_w$ 15.) Channel Slope, s 16.) Manning's roughness coeff., n 17.) $v = \frac{1.49r^{2/3}s^{1/2}}{n}$ 18.) Flow Length, L	Compute v Compute T_t	ft ft² ft ft/ft ft/s ft/s	0	0	= 0 hr 0.167269
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P_w 14.) Hydraulic Radius, $r = a/P_w$ 15.) Channel Slope, s 16.) Manning's roughness coeff., n 17.) $v = \frac{1.49r^{2/3}s^{1/2}}{n}$ 18.) Flow Length, L 19.) $T_r = \frac{L}{3600 v}$	Compute v Compute T_t	ft ft² ft ft/ft ft/s ft/s	0	0 0	
12a.) Ditch side slope 1 12b.) Ditch side slope 2 12c.) Bottom width 12d.) Depth of flow 12.) Cross sectional flow area, a 13.) Wetted Perimeter, P_w 14.) Hydraulic Radius, $r = a/P_w$ 15.) Channel Slope, s 16.) Manning's roughness coeff., n 17.) $v = \frac{1.49r^{2/3}s^{1/2}}{n}$ 18.) Flow Length, L 19.) $T_r = \frac{L}{3600 \ v}$	Compute v Compute T_t	ft ft² ft ft/ft ft/s ft/s	0	0 0	hr 0.167269

Time of Concentration & Travel 1	ime Workshee	t		
Note: Space for as many as tw	o segments per flow t	ype can be used	for each worksheet.	
Include a map, schemati	c, or description of flo	w segments		
Sheet Flow (Applicable to T _c only)		Segment ID		
1.) Surface Description (use code A-J, table 3-1)		<u>oogmone 15</u>	A	
2.) Manning's roughness coeff., n (table 3-1)		i	0.011	0
3.) Flow length, L (total L <= 300 ft)		ft	300	
	oux Falls IDF)	in	3.04	2.688
5.) Land Slope, s		ft/ft	0.0064	
6.) $0.007 (nL)^{0.8}$	Compute T _t	hr	0.078704653 +	0 = 0.078705
$T_{t} = \frac{0.007 (nL)^{0.8}}{P_{2}^{0.5} s^{0.4}}$				
P_2 S				
Shallow concentrated flow		Segment ID		
7.) Surface description (P=paved or U=unpaved)			U	
8.) Flow length, L		ft	250	
9.) Watercourse slope, s		ft/ft	0.0064	
10.) Average velocity, v (figure 3-1)		ft/s	1.29076	
11.) <i>L</i>	Compute T _t	hr	0.053801206 +	0 = 0.053801
$T_{i} = \frac{L}{3600 \text{ v}}$				
3000 7				
Channel Flow (trapezoidal channel)		Segment ID		
12a.) Ditch side slope 1				
12b.) Ditch side slope 2				
12c.) Bottom width		ft		
12d.) Depth of flow		ft		
12.) Cross sectional flow area, a		ft ²	0	0
13.) Wetted Perimeter, P _w		ft	0	0
14.) Hydraulic Radius, r = a/P _w	Compute r	ft	0	0
15.) Channel Slope, s		ft/ft		
16.) Manning's roughness coeff., n				
$v = \frac{1.49r^{2/3}s^{1/2}}{17.0}$				
$ 17.\rangle v = \frac{1}{12}$	Compute v	ft/s	0	0
40) 51				
18.) Flow Length, L		ft	<u> </u>	
$ 19.\rangle _{T} = L$	Compute T _t	hr	0 +	0 = 0
$ T_{i} = \frac{L}{3600 \text{ v}}$				
20.) Watershed or subarea T _c or T _t (add	T, in steps 6, 11,	19)		hr 0.132506
				min 8
				222223

(210-VI-TR-55, Second Ed., June 1986)

p					
Time of Concentration & Trave	I Time Workshee	<u>et</u>			
Note: Space for as many a	s two segments per flow	type can be used	for each workshe	eet.	
Include a map, scher	natic, or description of flo	w segments			- 1
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					
Sheet Flow (Applicable to T c only)		Segment ID			
1.) Surface Description (use code A-J, table 3	-1)		Α		
2.) Manning's roughness coeff., n (table 3-1)			0.011	0	
3.) Flow length, L (total L <= 300 ft)		ft	230		
4.) Two-yr 24-hr rainfall, P ₂	(Sioux Falls IDF)	in	3.04	2.688	
5.) Land Slope, s		ft/ft	0.0077		
6.) $0.007 (nL)^{0.8}$	Compute T _t	hr	0.059096448 +	0	= 0.059096
$T_{t} = \frac{0.007 (nL)^{0.8}}{P_{2}^{0.5} s^{0.4}}$					
P_2 S					
Shallow concentrated flow		Segment ID			
7.) Surface description (P=paved or U=unpav	ed)	Segment ID			
8.) Flow length, L	eu)	ft			
9.) Watercourse slope, s		ft/ft			
10.) Average velocity, v (figure 3-1)		ft/s			
141)	Compute T _t	hr	0 +	. 0	= 0
$T_t = \frac{L}{3600 \text{ v}}$	00pato 1	""		U	
3600 v					
Channel Flow (trapezoidal channel)		Segment ID			
12a.) Ditch side slope 1					
12b.) Ditch side slope 2					
12c.) Bottom width		ft			
12d.) Depth of flow		ft			
12.) Cross sectional flow area, a		ft ²	0	0	
13.) Wetted Perimeter, P _w		ft	0	0	
14.) Hydraulic Radius, r = a/P _w	Compute r	ft	0	0	
15.) Channel Slope, s		ft/ft			
16.) Manning's roughness coeff., n					
1 A Ore 2/3 c 1/2					
$v = \frac{1.49r^{2/3}s^{1/2}}{17.0}$	Compute v	ft/s	l ol	0	
n					
18.) Flow Length, L		ft			
I I	Commute T				
$ T_{t} = \frac{L}{3600 \text{ v}} $	Compute T _t	hr	0 +	0	= 0
20.) Watershed or subarea T_c or T_t (add T_t in steps 6, 11,	19)		i	0.059096
				mi	13 4

I	(210-VI-TR-55, Second	Ed lune 1000)			

Time of Concentration & Trav	vel Time Workshee	<u>et</u>			
	as two segments per flow		for each worksh	eet.	
Include a map, sch	ematic, or description of flo	w segments			
Sheet Flow (Applicable to T c only)		Segment ID			
1.) Surface Description (use code A-J, table	3-1)		E		
2.) Manning's roughness coeff., n (table 3-1)		0.15	0	
3.) Flow length, L (total L <= 300 ft)		ft	300		
4.) Two-yr 24-hr rainfall, P ₂	(Sioux Falls IDF)	in	3.04	2.688	
5.) Land Slope, s		ft/ft	0.0077		
$T_{t} = \frac{0.007 (nL)^{0.8}}{P_{2}^{0.5} s^{0.4}}$	Compute T _t	hr	0.591064627	0	= 0.591065
$P_2^{0.5} S^{0.4}$					
Shallow concentrated flow		Segment ID			
7.) Surface description (P=paved or U=unp	aved)		U		
8.) Flow length, L		ft	480		
9.) Watercourse slope, s		ft/ft	0.0077		
10.) Average velocity, v (figure 3-1)		ft/s	1.415796629		
$T_{t} = \frac{L}{3600 \text{ y}}$	Compute T _t	hr	0.094175484	0	= 0.094175
3600 v					
Channel Flow (trapezoidal channel)		Segment ID			
12a.) Ditch side slope 1					
12b.) Ditch side slope 2					
12c.) Bottom width		ft			
12d.) Depth of flow		ft			
12.) Cross sectional flow area, a		ft ²	0	0	
13.) Wetted Perimeter, P _w		ft	0	0	
14.) Hydraulic Radius, r = a/P _w	Compute r	ft	0	0	
15.) Channel Slope, s		ft/ft			
16.) Manning's roughness coeff., n					
$\begin{vmatrix} 17. & v = \frac{1.49r^{2/3}s^{1/2}}{17.} \end{vmatrix}$					
$ 17. v = \frac{1}{n}$	Compute v	ft/s	0	0	
18.) Flow Length, L		ft			
T = L	Compute T _t	hr	0 +	- 0	= 0
$[19.) \ T_t = \frac{L}{3600 \ v}$					
20.) Watershed or subarea T_c or T_t	(add T _t in steps 6, 11,	19)			hr 0.68524
				m	in 41
	(210-VI-TR-55, Second	Ed., June 1986)			

Time of Concentration & Trav	el Time Workshee	<u>et</u>			
Note: Space for as many	the second of th	• 1	d for each workshe	et.	
Include a map, sche	ematic, or description of flo	w segments			
Sheet Flow (Applicable to T only)	5.43	Segment ID			
1.) Surface Description (use code A-J, table			E 0.15		
 Manning's roughness coeff., n (table 3-1) Flow length, L (total L <= 300 ft) 		ft	300	-	
4.) Two-yr 24-hr rainfall, P ₂	(Sioux Falls IDF)	in	3.04	2,688	
	(SIDUX FAIIS IDF)	ft/ft	0.0064	2.000	
5.) Land Slope, s	Compute T			0	= 0.636443
$T_{t} = \frac{0.007 (nL)^{0.8}}{P_{2}^{0.5} s^{0.4}}$	Compute T _t	hr	0.636442642 +	U	= 0.636443
$P_2^{0.5} s^{0.4}$					
Shallow concentrated flow		Segment ID			
7.) Surface description (P=paved or U=unpa	ived)		U		
8.) Flow length, L		ft	250		
9.) Watercourse slope, s		ft/ft ft/s	0.0064 1.29076		
10.) Average velocity, v (figure 3-1)	Compute T,				- 0.052004
$T_{t} = \frac{L}{3600 \text{ y}}$	Compute It	hr	0.053801206 +	0	= 0.053801
$I_{t} = \frac{1}{3600 \text{ v}}$					
Channel Flow (trapezoidal channel)		Segment ID			
12a.) Ditch side slope 1					
12b.) Ditch side slope 2					
12c.) Bottom width		ft			
12d.) Depth of flow		ft			
12.) Cross sectional flow area, a		ft ²	0	0	
13.) Wetted Perimeter, P _w		ft	0	0	
14.) Hydraulic Radius, r = a/P _w	Compute r	ft	0	0	
15.) Channel Slope, s		ft/ft			
16.) Manning's roughness coeff., n					
$v = \frac{1.49r^{2/3}s^{1/2}}{17.0}$					
$ 17.\rangle v = \frac{11.57}{2}$	Compute v	ft/s	0	0	
n					
18.) Flow Length, L		ft			
19) 7 L	Compute T _t	hr	0 +	0	= 0
$ T_{t} = \frac{L}{3600 \text{ v}}$	output II	in .			
	add T in at 0 44	40)		100	
20.) Watershed or subarea T _c or T _t (add I, in steps 6, 11,	19)		1	0.690244
				mi	in 41
	(210-VI-TR-55, Second	Ed., June 1986)			

Time of Concentration 9 Tra	val Tima Markaha				
Time of Concentration & Tra	as two segments per flow		d for each workship	not.	
	nematic, or description of flo		i for each workshe	et.	
molado a map, sor	iornalia, or accompliant of no	w cogments			
Sheet Flow (Applicable to T c only)		Segment ID			
1.) Surface Description (use code A-J, table	e 3-1)		E		
2.) Manning's roughness coeff., n (table 3-	1)		0.15	0	
3.) Flow length, L (total L <= 300 ft)		ft	15		
4.) Two-yr 24-hr rainfall, P ₂	(Sioux Falls IDF)	in	3.04	2.688	
5.) Land Slope, s		ft/ft	0.5		
6.) $0.007 (nL)^{0.8}$	Compute T _t	hr	0.010134895 +	0	= 0.010135
$T_{i} = \frac{0.007 (nL)^{0.8}}{P_{2}^{0.5} s^{0.4}}$					
Γ_2 S					
Shallow concentrated flow		Segment ID			
7.) Surface description (P=paved or U=unp	aved)	ocginent ib	U		
8.) Flow length, L		ft			
9.) Watercourse slope, s		ft/ft			
10.) Average velocity, v (figure 3-1)		ft/s	0		
11.)	Compute T _t	hr	0 +	0 :	= 0
$T_t = \frac{L}{3600 \text{ y}}$		- 1			
3600 V					
Channel Flow (trapezoidal channel)		Segment ID			
12a.) Ditch side slope 1					
12b.) Ditch side slope 2					
12c.) Bottom width		ft			
12d.) Depth of flow		ft			
12.) Cross sectional flow area, a		ft ²	0	0	
13.) Wetted Perimeter, P _w		ft	0	0	
14.) Hydraulic Radius, r = a/P _w	Compute r	ft	0	0	
15.) Channel Slope, s		ft/ft			
16.) Manning's roughness coeff., n					
1 40-2/3 1/2					
$ v = \frac{1.49r^{2/3}s^{1/2}}{17.9}$	Compute v	ft/s	o	0	
n	oomputo v	,,,,	•		
18.) Flow Length, L		ft			
I I	Commute T				
$T_t = \frac{L}{3600 \text{ v}}$	Compute T _t	hr	0 +	0	=0
20.) Watershed or subarea T_c or T_t	(add T _t in steps 6, 11,	19)		h	0.010135
				mi	n 1
	(210-VI-TR-55 Second	Ed June 1986)			

HMS Model Results Summary

	taken no see a		
Dook	Runoff	FLOW	Data

	Feat Kulloff Flow Nate																			
			Duration				Duration				Duration				Duration				r Duration	
Area	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year 1	100-year	2-year	10-year	50-year	100-year
							Grave	Existing	Conditi	on										
SS1	0.17	0.48	1.09	1.46	0.17	0.38	0.72	0.93	0.13	0.27	0.5	0.61	0.09	0.18	0.31	0.4	0.06	0.11	0.2	0.24
SS2	0.39	1.13	2.54	3.41	0.41	0.9	1.68	2.19	0.3	0.64	1.17	1.49	0.21	0.42	0.74	0.93	0.14	0.27	0.46	0.57
SS3	0.24	0.7	1.58	2.12	0.25	0.56	1.04	1.36	0.19	0.39	0.73	0.92	0.13	0.26	0.46	0.58	0.09	0.17	0.28	0.35
SS4	0.29	0.83	1.87	2.5	0.3	0.66	1.23	1.61	0.22	0.47	0.86	1.09	0.15	0.31	0.54	0.68	0.1	0.2	0.34	0.42
SS5	0.08	0.22	0.49	0.66	0.08	0.17	0.32	0.42	0.06	0.12	0.23	0.29	0.04	0.08	0.14	0.18	0.03	0.05	0.09	0.11
SS6																				
SS7								n/a (pa	art of Mo	narch site	during e	xisting con	ditions)							
SS8	0.1	0.3	0.68	0.91	0.11	0.24	0.45	0.58	0.08	0.17	0.31	0.4	0.06	0.11	0.2	0.25	0.04	0.07	0.12	0.15
Subarea1 (SW of Site)	15.3	29.06	51.67	64.62	11.12	20.15	33.16	40.63	7.84	13.62	21.89	26.43	4.96	8.54	13.46	16.2	3.08	5.14	7.99	9.58
Subarea 2 (NE of Site)	3.84	7.58	13.26	16.48	2.67	4.88	8.13	9.93	1.88	3.27	5.25	6.33	1.19	2.04	3.21	3.87	0.73	1.23	1.9	2.28
Monarch (SW of Site)	2.57	5	8.63	10.69	1.7	3.11	5.16	6.3	1.18	2.06	3.29	3.97	0.75	1.28	2.01	2.42	0.46	0.77	1.19	1.43
							Grass	Proposed	Conditi											
SS1	0.17	0.48	1.09	3.7.0.0	0.17	0.38	0.72	0.93		0.27	0.5	0.64	0.09	0.18	0.31	0.4	0.06	0.11	0.2	0.24
SS2	0.39	1.13	2.54	3.41	0.41	0.9	1.68	2.19		0.64	1.17	1.49	0.21	0.42	0.74	0.93	0.14	0.27	0.46	0.57
SS3	0.24	0.7	1.58	2.12	0.25	0.56	1.04	1.36	0.19	0.39	0.73	0.92	0.13	0.26	0.46	0.58	0.09	0.17	0.28	0.35
SS4	0.29	0.83	1.87	2.5	0.3	0.66	1.23	1.61	0.22	0.47	0.86	1.09	0.15	0.31	0.54	0.68	0.1	0.2	0.34	0.42
SS5	0.08	0.22	0.49	0.66	0.08	0.17	0.32	0.42	0.06	0.12	0.23	0.29	0.04	0.08	0.14	0.18	0.03	0.05	0.09	0.11
SS6	0.1	0.3	0.68	0.91	0.11	0.24	0.45	0.58	0.08	0.17	0.31	0.4	0.06	0.11	0.2	0.25	0.04	0.07	0.12	0.15
SS7	0.05	0.15	0.34	0.46	0.05	0.12	0.22	0.29	0.04	0.08	0.16		0.03	0.06	0.1	0.12	0.02	0.04	0.06	0.08
SS8	0.1	0.3	0.68	0.91	0.11	0.24	0.45	0.58	0.08	0.17	0.31	0.4	0.06	0.11	0.2	0.25	0.04	0.07	0.12	0.15
Subarea1 (SW of Site)	3.51	9.14	19.25	25.47	4.11	9.57	18.69	24.21	3.61	7.82	14.64		2.71	5.58	9.96	12.51	1.9	3.63	6.22	7.8
Subarea 2 (NE of Site)	1.84	2.18	4.58	6.07	0.98	2.28	4.45	5.76	0.86	1.86	3.49	4.43	0.65	1.33	2.37	2.98	0.45	0.86	1.48	1.86
Monarch (SW of Site)	4.07	6.16	9.06	10.66	2.27	3.4	4.98	5.84	1.38	2.06	3	3.52	0.83	1.25	1.8	2.12	0.48	0.72	1.04	1.22
Precip (inches)	1.43	2.1	3.04	3.56	1.94	2.86	4.14	4.85	2.28	3.35	4.85	5.68	2.64	3.89	5.62	6.59	3.04	4.47	6.46	7.58

Peak Flow Rate

	1 Hour Duration 2-year 10-year 50-year 100					3 Hour	Duration	1		6 Hour	Duration	1		12 Hour	Duration	n		24 Hou	Duration	1
Area	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year
								Existing												
To Albany Avenue Sewer (South West of																				
Site)	10.0	10.4	14.4	16.8	10.2	10.1	11.8	13.0	9.0	10.2	10.2	11.1	5.7	9.8	10.2	10.2	3.5	5.9	9.2	10.2
Direct Runoff to South West of Site (side																				
swale runoff)	0.0	0.0	0.0	0.9	0.0	0.0	0.9	1.9	0.0	0.1	0.9	1.8	0.0	0.2	1.0	1.6	0.0	0.2	0.8	0.9
To Whipple Street Sewer through Catch																				
Basin (NE of site)	1.0	1.1	1.1	1.1	1.0	1.1	1.1	1.1	1.0	1.1	1.1	1.1	1.0	1.0	1.1	1.1	0.7	1.0	1.1	1.1
To Whipple Street through Direct Runoff																	1 1			
(NE of site side swale overflow)	0.0	0.0	0.0	1.1	0.0	0.0	1.3	2.3	0.0	0.0	1.2	2.1	0.0	0.2	1.1	1.5	0.0	0.2	0.7	0.9
Total Direct Runoff	0.0	0.0	0.0	2.1	0.0	0.0	2.2	4.2	0.0	0.1	2.1	3.9	0.0	0.4	2.0	3.1	0.0	0.4	1.6	1.8
							Grass	Proposed	Conditi	on										
To Outfall #178 (South West of site)	6.1	8.6	9.5	9.8	6.7	8.8	9.7	10.1	5.5	8.6	9.5	9.9	4.2	7.5	9.1	9.5	2.9	5.4	7.9	8.4
Direct Runoff to South West of Site (side																				
swale runoff)	0.0	0.0	0.6	0.9	0.0	0.1	0.8	1.4	0.0	0.1	0.6	0.8	0.0	0.2	0.4	0.6	0.0	0.1	0.2	0.3
To Whipple Street through Direct Runoff															- 1					
(NE of site side swale overflow)	0.0	0.0	0.0	0.0	0.0	0.0	0.6	1.6	0.0	0.0	0.9	1.5	0.0	0.2	0.8	1.4	0.0	0.1	0.7	0.9
Total Direct Runoff	0.0	0.0	0.6	0.9	0.0	0.1	1.4	3.0	0.0	0.1	1.5	2.3	0.0	0.3	1.2	1.9	0.0	0.3	0.9	1.2
Decrease in Peak Flow to SW	3.9	1.9	4.9	6.9	3.5	1.3	2.1	3.0	3.5	1.6	0.7	1.2	1.5	2.3	1.1	0.7	0.6	0.5	1.3	1.8
Percent Decrease	39%	18%	34%	41%	34%	13%	18%	23%	39%	16%	7%	11%	27%	23%	11%	7%	18%	8%	14%	18%

Peak Elevation in Stage-Storage-Discharge Curve

4 Hour Duration Character and Character 42 Hour Duration 24 Hour Duration 24 Hour Duration																				
		1 Hour	Duration			3 Hour	Duration	ì		6 Hour	Duration			12 Hour	Duration	1		24 Hou	r Duration	1
Area	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year
							Grave	Existing	Conditi	on										
SS1	593.2	593.4	593.7	593.9	593.3	593.7	594	594	593.5	593.8	594	594	593.6	594	594	594	593.9	594	594	594
SS2 andSS3	593.2	593.5	593.9	594	593.4	593.8	594	594	593.6	594	594	594	593.7	594	594	594	593.9	594	594	594
SS4	593.2	593.5	593.9	594	593.4	593.8	594	594	593.6	594	594	594	593.7	594	594	594	593.9	594	594	594
SS5	593.2	593.5	593.8	594	593.4	593.7	594	594	593.5	593.7	594	594	593.7	594	594	594	593.8	594	594	594
SS8	593.2	593.5	593.8	594	593.4	593.7	594	594	593.5	593.9	594	594	593.7	594	594	594	593.8	594	594	594
Subarea1	596.1	596.7	597.2	597.4	596.1	596.7	597.3	597.6	593.5	596.5	597.2	597.5	591.1	594.3	596.9	597.2	590.2	591.2	593.7	596.5
Subarea 2	597.3	597.9	598.2	598.3	597.4	598	598.3	598.5	597.2	598	598.3	598.5	597	597.6	598.2	598.4	594.8	597.1	598	598.2
Monarch										1	n/a									
							Grass	Proposed	Conditi	ion										
SS1	593.1	593.2	593.5	593.6	593.2	593.4	593.7	593.8	593.3	593.6	593.8	594	593.4	593.7	594	594.2	593.5	593.8	594.2	594.4
SS2 andSS3	593.2	593.4	593.7	593.9	593.4	593.7	594	594	593.5	593.8	594	594	593.6	594	594	594	593.7	594	594	594
SS4	593.1	593.2	593.5	593.6	593.1	593.3	593.5	593.6	593.1	593.2	593.5	593.6	593.1	593.2	593.3	593.4	593.1	593.1	593.2	593.3
SS5 and SS6	593.3	593.7	594	594	593.6	594	594	594	593.7	594	594	594	593.9	594	594	594	594	594	594	594
SS7 and SS8	593.1	593.1	593.3	593.4	593.1	593.2	593.3	593.4	593.1	593.1	593.3	593.3	593.1	593.1	593.2	593.2	593	593.1	593.1	593.2
Subarea1	593.2	596.8	597.6	598	594.2	597.1	598	598.2	593.4	597	597.7	598.2	592.1	596	597.5	598	591.4	593.4	596.9	597.4
Subarea 2	596.3	598.2	598.8	599	597.3	598.3	599.1	599.2	596.6	598.3	599.1	599.2	594.8	598.1	598.9	599.1	593.6	596.6	598.4	598.9
Monarch	592.4	592.6	592.8	592.9	592.3	592.5	592.7	592.8	591.3	592.3	592.5	592.6	590.1	590.9	592.3	592.4	589.7	590	590.4	590.9

Proposed Conditions

6" restricto
9" restricto
4" restricto
6" restricto
6" restricto

proposed conditions is grass (CN-78) and existing conditions is gravel (CN -89)

		Top of	Bottom	Max	Min
Max	Min	Basin	Pond	Depth	Freeboar
594	593.2	594	593	1	0
594	593.2	594	593	1	0
594	593.2	594	593	1	0
594	593.2	594	593	1	0
594	593.2	594	593	1	0
597.6	590.2	598	594.78	2.82	0.4
598.5	594.8	599	596.23	2.27	0.5
594.4	593.1	594.5	593	1.4	0.1
594	593.2	594	593	1	0
593.6	593.1	594	593	0.6	0.4
594	593.3	594	593	1	0
593.4	593	594	593	0.4	0.6
598.2	591.4	599	595.78	2.42	0.8
599.2	593.6	600	597.23	1.97	0.8
592.9	589.7	596	594.81	-1.91	3.1

Peak Runoff Flow Rate

									1-1	ount rearre	711 1 10 11 1	iuto								
		1 Hou	r Duration			3 Hour	Duration			6 Hour	Duration			12 Hou	r Duration			24 Hou	r Duratio	n
Area	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year
Gravel Existing Condition																				
SS1	0.17	0.48	1.09	1.46	0.17	0.38	0.72	0.93	0.13	0.27	0.5	0.61	0.09	0.18	0.31	0.4	0.06	0.11	0.2	0.24
SS2	0.39	1.13	2.54	3.41	0.41	0.9	1.68	2.19	0.3	0.64	1.17	1.49	0.21	0.42	0.74	0.93	0.14	0.27	0.46	0.57
SS3	0.24	0.7	1.58	2.12	0.25	0.56	1.04	1.36	0.19	0.39	0.73	0.92	0.13	0.26	0.46	0.58	0.09	0.17	0.28	0.35
SS4	0.29	0.83	1.87	2.5	0.3	0.66	1.23	1.61	0.22	0.47	0.86	1.09	0.15	0.31	0.54	0.68	0.1	0.2	0.34	0.42
SS5	0.08	0.22	0.49	0.66	0.08	0.17	0.32	0.42	0.06	0.12	0.23	0.29	0.04	0.08	0.14	0.18	0.03	0.05	0.09	0.11
SS6												-								
SS7								n/a (pa	art of Mor	arch site	during ex	isting cond	ditions)							
SS8	0.1	0.3	0.68	0.91	0.11	0.24	0.45	0.58	0.08	0.17	0.31	0.4	0.06	0.11	0.2	0.25	0.04	0.07	0.12	0.15
Subarea1 (SW of Site)	15.3	29.06	51.67	64.62	11.12	20.15	33.16	40.63	7.84	13.62	21.89	26.43	4.96	8.54	13.46	16.2	3.08	5.14	7.99	9.58
Subarea 2 (NE of Site)	3.84	7.58	13.26	16.48	2.67	4.88	8.13	9.93	1.88	3.27	5.25	6.33	1.19	2.04	3.21	3.87	0.73	1.23	1.9	2.28
Monarch (SW of Site)	2.57	5	8.63	10.69	1.7	3.11	5.16	6.3	1.18	2.06	3.29	3.97	0.75	1.28	2.01	2.42	0.46	0.77	1.19	1.43
						G	ravel Pro	posed Co	ndition											
SS1	0.17	0.48	1.09	1.46	0.17	0.38	0.72	0.93	0.13	0.27	0.5	0.64	0.09	0.18	0.31	0.4	0.06	0.11	0.2	0.24
SS2	0.39	1.13	2.54	3.41	0.41	0.9	1.68	2.19	0.3	0.64	1.17	1.49	0.21	0.42	0.74	0.93	0.14	0.27	0.46	0.57
SS3	0.24	0.7	1.58	2.12	0.25	0.56	1.04	1.36	0.19	0.39	0.73	0.92	0.13	0.26	0.46	0.58	0.09	0.17	0.28	0.35
SS4	0.29	0.83	1.87	2.5	0.3	0.66	1.23	1.61	0.22	0.47	0.86	1.09	0.15	0.31	0.54	0.68	0.1	0.2	0.34	0.42
SS5	0.08	0.22		0.66	0.08	0.17	0.32	0.42	0.06	0.12	0.23	0.29	0.04	0.08	0.14	0.18	0.03	0.05	0.09	0.11
SS6	0.1	0.3	0.68	0.91	0.11	0.24	0.45	0.58	0.08	0.17	0.31	0.4	0.06	0.11	0.2	0.25	0.04	0.07	0.12	0.15
SS7	0.05	0.15	0.34	0.46	0.05	0.12	0.22	0.29	0.04	0.08	0.16	0.2	0.03	0.06	0.1	0.12	0.02	0.04	0.06	0.08
SS8	0.1	0.3	0.68	0.91	0.11	0.24	0.45	0.58	0.08	0.17	0.31	0.4	0.06	0.11	0.2	0.25	0.04	0.07	0.12	0.15
Subarea1 (SW of Site)	15.3	29.06		64.62		20.15	33.16	40.63		13.62	21.89	26.43		8.54	13.46	16.2	3.08	5.14	7.99	9.58
Subarea 2 (NE of Site)	3.84	7.58		16.48	2.67	4.88	8.13	9.93		3.27	5.25	6.33		2.04	3.21	3.87	0.73	1.23	1.9	2.28
Monarch (SW of Site)	4.07	6.16	9.06	10.66	2.27	3.4	4.98	5.84	1.38	2.06	3	3.52	0.83	1.25	1.8	2.12	0.48	0.72	1.04	1.22
Precip (inches)	1.43	2.1	3.04	3.56	1.94	2.86	4.14	4.85	2.28	3.35	4.85	5.68	2.64	3.89	5.62	6.59	3.04	4.47	6.46	7.58

Peak Flow Rate

			Duration				Duration				Duration				Duration				r Duratio	
Area	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year
Gravel Existing Condition																				
To Albany Avenue Sewer (South West of Site)	10.0	10.4	14.4	16.8	10.2	10.1	11.8	13.0	9.0	10.2	10.2	11.1	5.7	9.8	10.2	10.2	3.5	5.9	9.2	10.2
Direct Runoff to South West of Site (side swale																				
runoff)	0.0	0.0	0.0	0.9	0.0	0.0	0.9	1.9	0.0	0.1	0.9	1.8	0.0	0.2	1.0	1.6	0.0	0.2	0.8	0.9
To Whipple Street Sewer through Catch Basin																				
(NE of site)	1.0	1.1	1.1	1.1	1.0	1.1	1.1	1.1	1.0	1.1	1.1	1.1	1.0	1.0	1.1	1.1	0.7	1.0	1.1	1.1
To Whipple Street through Direct Runoff (NE of																				
site side swale overflow)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Direct Runoff	0.0	0.0	0.0	0.9	0.0	0.0	0.9	1.9	0.0	0.1	0.9	1.8	0.0	0.2	1.0	1.6	0.0	0.2	0.8	0.9
						G	ravel Pro	posed Co	ndition											
To Outfall #178 (South West of site)	8.5	9.1	10.0	10.3	8.5	9.2	10.0	10.3	7.8	9.0	9.8	10.1	6.9	8.1	9.4	9.7	4.4	7.0	8.2	8.7
Direct Runoff to South West of Site (side swale																				
runoff)	0.0	0.0	0.6	0.9	0.0	0.1	0.8	1.4	0.0	0.1	0.6	0.8	0.0	0.2	0.4	0.6	0.0	0.1	0.2	0.3
To Whipple Street through Direct Runoff (NE of																				
site side swale overflow)	0.0	0.0	0.0	0.0	0.0	0.0	0.6	1.6	0.0	0.0	0.9	1.5	0.0	0.2	0.8	1.4	0.0	0.1	0.7	0.9
Total Direct Runoff	0.0	0.0	0.6	0.9	0.0	0.1	1.4	3.0	0.0	0.1	1.5	2.3	0.0	0.3	1.2	1.9	0.0	0.3	0.9	1.2
Decrease in Peak Flow to SW	1.5	1.3	4.4	6.5	1.7	0.9	1.8	2.7	1.2	1.2	0.4	1.0	-12	1.7	0.8	0.5	-0.9	-1.1	1.0	1.5
Percent Decrease	15%	12%	31%	39%	16%	9%	15%	21%	13%	12%	4%	9%	-21%	17%	8%	5%	-25%	-18%	11%	15%

Peak Elevation in Stage-Storage-Discharge Curve

		1 Hour	Duration			3 Hour	Duration			6 Hour	Duration			12 Hour	Duration	1		24 Hou	r Duration	
Area	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year	2-year	10-year	50-year	100-year
Gravel Existing Condition																				
SS1	593.2	593.4	593.7	593.9	593.3	593.7	594	594	593.5	593.8	594	594	593.6	594	594	594	593.9	594	594	594
SS2 andSS3	593.2	593.5	593.9	594	593.4	593.8	594	594	593.6	594	594	594	593.7	594	594	594	593.9	594	594	594
SS4	593.2	593.5	593.9	594	593.4	593.8	594	594	593.6	594	594	594	593.7	594	594	594	593.9	594	594	594
SS5	593.2	593.5	593.8	594	593.4	593.7	594	594	593.5	593.7	594	594	593.7	594	594	594	593.8	594	594	594
SS8	593.2	593.5	593.8	594	593.4	593.7	594	594	593.5	593.9	594	594	593.7	594	594	594	593.8	594	594	594
Subarea1	596.1	596.7	597.2	597.4	596.1	596.7	597.3	597.6	593.5	596.5	597.2	597.5	591.1	594.3	596.9	597.2	590.2	591.2	593.7	596.5
Subarea 2	597.3	597.9	598.2	598.3	597.4	598	598.3	598.5	597.2	598	598.3	598.5	597	597.6	598.2	598.4	594.8	597.1	598	598.2
Monarch											n/a									
						G	ravel Pro	posed Co	ndition											
SS1	593.1	593.2	593.5	593.6	593.2	593.4	593.7	593.8	593.3	593.6	593.8	594	593.4	593.7	594	594.2	593.5	593.8	594.2	594.4
SS2 andSS3	593.2	593.4	593.7	593.9	593.4	593.7	594	594	593.5	593.8	594	594	593.6	594	594	594	593.7	594	594	594
SS4	593.1	593.2	593.5	593.6	593.1	593.3	593.5	593.6	593.1	593.2	593.5	593.6	593.1	593.2	593.3	593.4	593.1	593.1	593.2	593.3
SS5 and SS6	593.3	593.7	594	594	593.6	594	594	594	593.7	594	594	594	593.9	594	594	594	594	594	594	594
SS7 and SS8	593.1	593.1	593.3	593.4	593.1	593.2	593.3	593.4	593.1	593.1	593.3	593.3	593.1	593.1	593.2	593.2	593	593.1	593.1	593.2
Subarea1	597.1	597.8	598.3	598.5	597.1	597.9	598.4	598.7	596.9	597.6	598.3	598.6	595.7	597.2	598.1	598.4	592.5	595.8	597.4	597.9
Subarea 2	598.3	598.9	599.2	599.3	598.4	599	599.3	599.5	598.2	598.9	599.3	599.5	598	598.6	599.2	599.4	595.4	598.1	598.9	599.1
Monarch	592.4	592.6	592.8	592.9	592.3	592.5	592.7	592.8	591.3	592.3	592.5	592.6	590.1	590.9	592.3	592.4	589.7	590	590.4	590.9

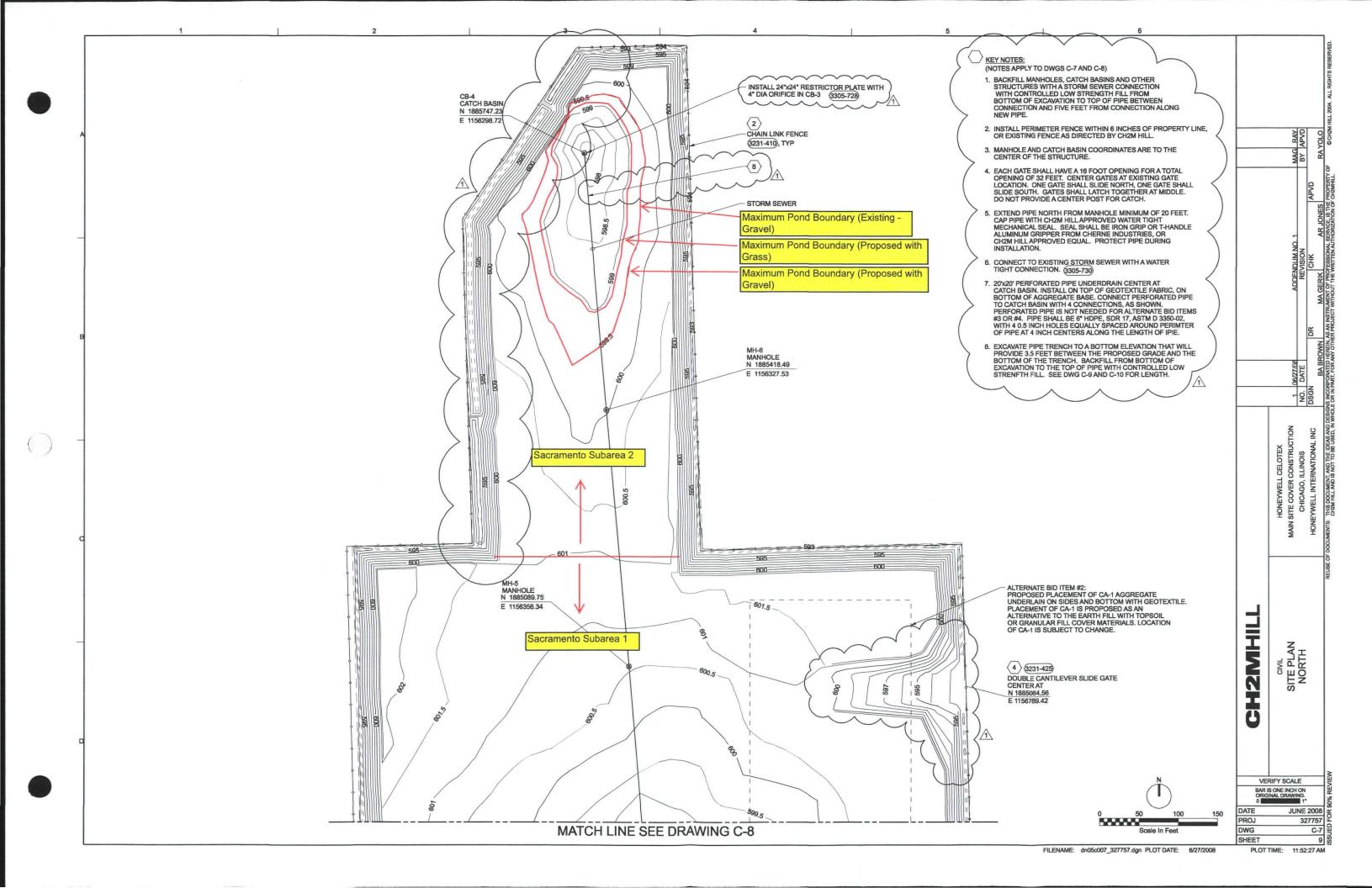
Proposed Conditions

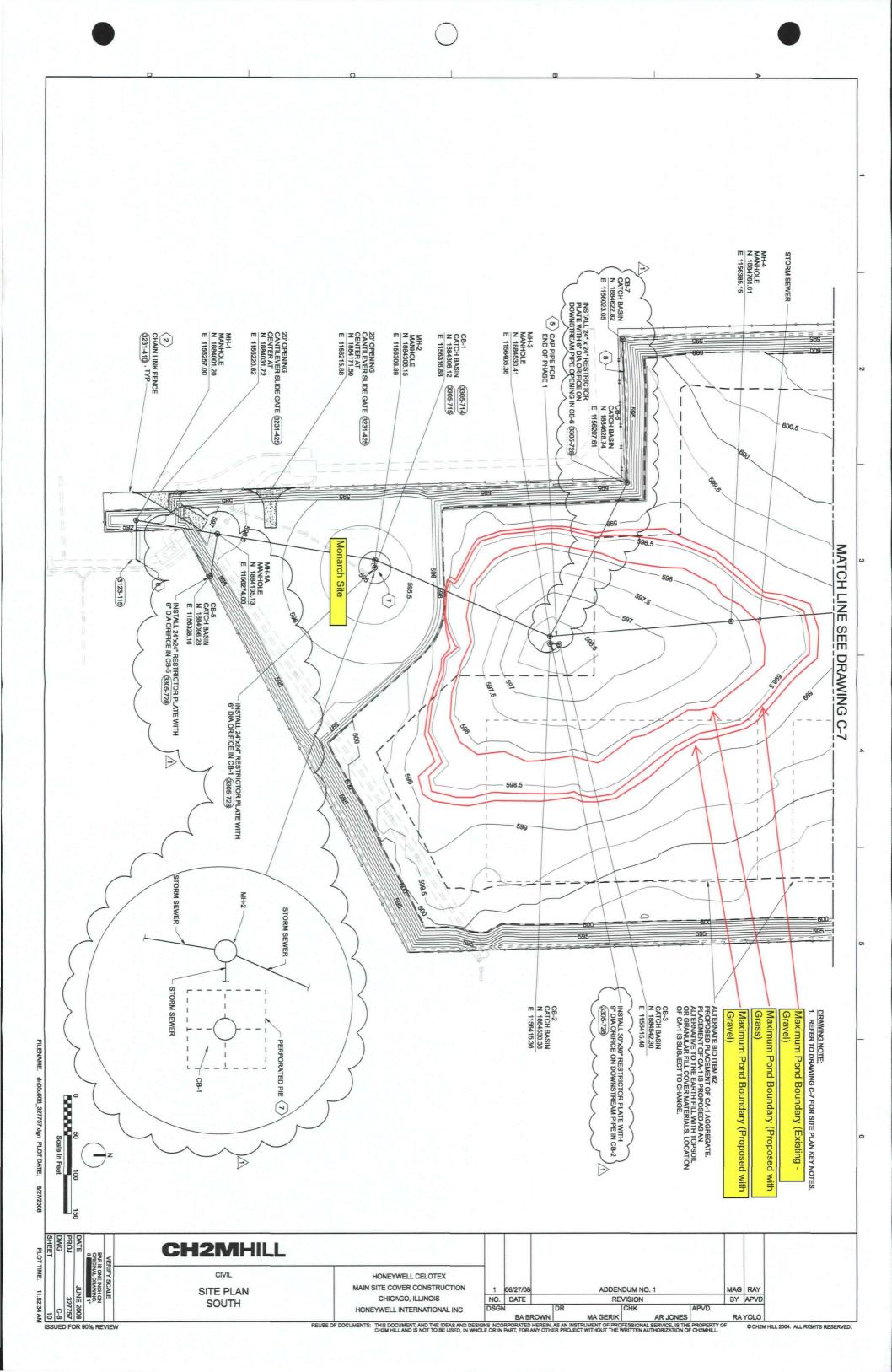
Monarch 6" restrictor Sacramento #1 9" restrictor Sacramento #2 4" restrictor SS4 6" restrictor SS7 and SS8 6" restrictor

Both proposed conditions and existing conditions are gravel - CN -89

			Bottom	Max	Min
Max	Min	Top of Basin	Pond	Depth	Freeboar
594	593.2	594	593	1	0
594	593.2	594	593	1	0
594	593.2	594	593	1	0
594	593.2	594	593	1	0
594	593.2	594	593	1	0
597.6	590.2	598	594.78	2.82	0.4
598.5	594.8	599	596.23	2.27	0.5
594.4	593.1	594.5	593	1.4	0.1
594	593.2	594	593	1	0
593.6	593.1	594	593	0.6	0.4
594	593.3	594	593	1	0
593.4	593	594	593	0.4	0.6
598.7	592.5	599	595.78	2.92	0.3
599.5	595.4	600	597.23	2.27	0.5
592.9	589.7	596	594.81	-1.91	3.1

Attachment 4 – Existing and Proposed Ponding Areas





Attachment 5 – Erosion and Sediment Control Plan (Stormwater Pollution Prevention Plan)

Main Site Cover Construction Storm Water Pollution Prevention Plan

For the Former Celotex Site 2800 South Sacramento Avenue Chicago, Illinois 60623

Prepared for

Honeywell International Inc.

August 2008



Table of Contents

	le of Contents	
Acr	onyms and Abbreviations	
1.0	Introduction	
2.0	Site Description	
2.1	Description of Construction Activities	
	2.1.1 Main Site	
	2.1.2 Staging Areas	
	2.1.3 Potential Sources of Contamination from Construction Activities	
2.2	Affected Area of the Sites	
	2.2.1 Staging Areas	
	2.2.2 Sacramento Parcel	
	2.2.3 Monarch Parcel	2-3
2.3	Runoff Coefficient	
	2.3.1 Staging Area	2-3
	2.3.2 Main Site	2-3
2.4	Site Map	2-4
2.5	Topography	2-4
2.6	Area and Site Surface Waters	2-4
2.7	Endangered/Threatened Species	2-5
2.8	Historic Preservation	
3.0	Best Management Practices for Storm Water Pollution Prevention	3-1
3.1	Control Measures for Pollutant Sources during Construction Activities	
3.2	Erosion and Sediment Controls	
3.3	Material Handling	3-4
3.4	Spill Prevention, Control, and Response	
3.5	Measures to Protect Endangered/Threatened Species	
3.6	Measures to Protect Historic Places	
3.7	Other Controls	3-5
	3.7.1 Employee Training	
	3.7.2 General Controls	
4.0	Maintenance	
5.0	Inspections	
5.1	Requirements During Construction	
5.2	Requirements Prior to Final Stabilization	
6.0	Non-Storm Water Discharges	
7.0	Contractor Certification	
8.0	Retention of Records	8-1

Tables

Table 3-1	Structural and Stabilization Measures
Table 5-1	Storm Water Inspection/Maintenance Guidelines

Appendices

Appendix A NPDES General Permit (ILR10) for Storm Water Discharges from Construction Activities Appendix B **Figures** General Site Location Map B-1 B-2 Sedimentation and Erosion Control Plan (North) B-3 Sedimentation and Erosion Control Plan (South) B-4 Decontamination Detail - Staging Area Appendix C SWP3 Inspection Checklist Appendix D List of Materials Stored Onsite Form

Appendix E Contractor Certification
Appendix F SWP3 Certification
Appendix G Miscellaneous Forms

Acronyms and Abbreviations

BMP Best Management Practices

C Run-off coefficient

USEPA United States Environmental Protection Agency

MWRDGC Metropolitan Water Reclamation District of Greater Chicago

MSDS Material Safety Data Sheet

NPDES National Pollutant Discharge and Elimination System

IEPA Illinois Environmental Protection Agency

CSSC Chicago Sanitary and Ship Canal

SWP3 Storm Water Pollution Prevention Plan

1.0 Introduction

This Storm Water Pollution Prevention Plan (SWP3) was developed for Main Site cover construction activities associated with the former Celotex Site located in Cook County, Chicago, Illinois. The SWP3 was developed following the General National Pollutant Discharge Elimination System Permit for Storm Water Discharges from Construction Site Activities for Illinois, as guidance. A copy of this permit (ILR10) is provided in Appendix A.

This SWP3 applies to construction activities at two locations in Cook County, Chicago, Illinois, which are associated with the former Celotex Site (Main Site). The scope of this SWP3 applies to construction activities to be performed by CH2M HILL and CH2M HILL's subcontractors on the Sacramento and Monarch parcels of the Main Site in the City of Chicago, in Cook County, Illinois. A map showing the general location of the Main Site parcels is provided in Appendix B.

The former Celotex Main Site consists of an approximately 20-acre parcel currently owned by the 2600 Sacramento Corporation (Sacramento), and an approximately 2-acre parcel currently owned by Monarch Asphalt (Monarch). The primary staging area for construction equipment will be located at the Monarch Asphalt property, 3031 South Albany Avenue, Chicago, Illinois, in Cook County. The United States Geological Survey (USGS) reference for the Main Site indicates that it is situated in the West 1/2 of the Southwest 1/4 of Section 25, Township 39 North, Range 13 East of the Third Prime Meridian on the Englewood 7.5 Minute Quadrangle. An additional staging area, yet to be determined, will be utilized during cover construction activities on the Monarch parcel. Similar practices will be utilized for both the Monarch parcel and the additional staging areas.

This plan provides an overview of construction activities and includes procedures that will be implemented during construction activities to prevent or reduce pollutants in storm water discharges. Each of the following elements is addressed:

- Site Description
- Control measures or Best Management Practices (BMPs) that will be implemented to control pollutants in storm water discharges
- Procedures for maintaining control measures
- Inspection procedures
- Identification of non-storm water discharges

This plan will be modified if there is a change in design, operation, or maintenance approach for construction activities. The plan will also be revised if procedures or controls prove to be ineffective in eliminating or significantly minimizing pollutants from potential sources.

2.0 Site Description

This SWP3 addresses cover construction activities at the former Celotex Site in Chicago, Illinois.

The Main Site was historically used for making, storing, and selling asphalt-roofing products. Former operations at the 22-acre Main Site during the approximate period of 1911 to 1989 may have resulted in the release of polycyclic aromatic hydrocarbons (PAHs) to the ground and into the air, thereby potentially impacting surface soil in the vicinity of the Main Site. Residential properties are located north, west and northeast of the Main Site. Facility closure occurred in 1989 and demolition of the Main Site was conducted in 1993.

2.1 Description of Construction Activities

2.1.1 Main Site

Construction activities for this SWP3 will include: demolition of abandoned utility poles, weigh scale near the current Sacramento parcel entrance, near surface and subsurface concrete structures, existing fences, removal of trees and general debris, removal and recontouring of side slope and swale area materials on the Sacramento and Monarch parcels, installation of a storm sewer system, placement of the Sacramento parcel cover (granular or granular and topsoil material), placement of the Monarch parcel cover (granular material), storm water management activities, construction of a new perimeter fence and disposal of general debris and excavated soil off-site at an approved disposal facility.

2.1.2 Staging Areas

Construction activities at the staging areas include: temporary parking, field trailers, portable sanitary facilities, and laydown of equipment and materials. A 500-gallon capacity diesel aboveground storage tank (AST) will be located at the staging area with lined and bermed secondary containment. A decontamination area will also be established in the staging area using secondary containment and ecology blocks to prevent runoff. An entrance and exit road will be constructed and maintained, and dust abatement measures will be in place during operations. The location of the primary staging area is shown on Figure B-1 and a plan view of the primary staging area is shown on Figure B-2 provided in Appendix B.

Following use of the Monarch parcel for staging activities, cover construction activities as described in Section 2.2.3 will be completed and an alternate staging area will be identified for use during the Monarch cover construction activities.

2.1.3 Potential Sources of Contamination from Construction Activities

The potential sources of pollutants that could be discharged in storm water during construction activities include:

- Vehicle and equipment fueling
- Vehicle and equipment decontamination areas
- · Loading and unloading areas
- Vehicle and equipment maintenance areas
- Soil excavation and deposition areas
- Soil stockpile areas
- Waste and material storage areas

2.2 Affected Area of the Site

The affected areas of the Main Site are described as three subareas due to the differing activities to be completed at each area. The three subareas cover the staging areas, including the Monarch Parcel for a portion of the project, along with construction activities at both the Sacramento and Monarch parcels. Upon completion of staging area use, they will be disturbed for cover construction activities. For the purposes of this SWP3, the staging areas and Main Site areas disturbed by cover construction activities are considered a cumulative whole for the project.

2.2.1 Staging Areas

The staging areas will encompass an area of approximately 2 acres, of which, varying acreage will be disturbed at any given time. The disturbed area includes the area for polylined temporary stockpiles, temporary parking, field trailers, portable sanitary facilities, laydown of equipment and materials, and the construction site entrance and exit road. A 500-gallon capacity aboveground storage tank (AST) containing diesel fuel will be located at the staging area with lined and bermed secondary containment. A truck decontamination area will also be established in the staging area using secondary containment and ecology blocks to prevent runoff.

2.2.2 Sacramento Parcel

The Sacramento parcel encompasses an area of approximately 20-acres. The entire property will be disturbed during cover construction. Fence removal, temporary construction and silt fence placement, truck scale demolition, and removal of miscellaneous debris and surface and shallow subsurface features will be conducted. The side slopes will be cleared of trees and vegetation followed by excavation to re-establish a consistent sized shallow swale around the perimeter of the property. The cover material will consist of either ungraded gravel (CA-6, surface area), or topsoil with clean earth fill (swale and side slope area). The entire parcel will be covered with at least 24 inches of clean material.

2.2.3 Monarch Parcel

The Monarch parcel encompasses an area of approximately 2-acres. The entire property will be disturbed during cover construction. The side slopes will be cleared of trees and vegetation followed by excavation to create a shallow swale around the perimeter of the property. The cover material will consist of either CA-1 stone, or a combination of CA-6 gravel over earthen fill. The entire parcel will be regraded with at least 24-inches of clean material.

2.3 Runoff Coefficient

The runoff coefficient (C) is a factor used to predict peak runoff flow using the Rational Formula. This is influenced by the type of ground cover, the type of soil, and the slope of the terrain. The less precipitation that infiltrates into the ground, the higher the C value. The weighted C values for the staging areas, cover construction areas, and side slope/swale area are determined in the following subsections. Runoff coefficients were calculated using typical C values from *City of Chicago Stormwater Management Ordinance Manual*.

2.3.1 Staging Area

The pre-construction (existing) weighted runoff coefficient for the staging areas are:

Type of Cover	% of Area Covered	Typical C Value	Weighted C Value
Undeveloped	25	.10	.03
Gravel	75	.70	.53
		Weighted C =	.56

Soil at the staging areas are generally composed of gravel with some scattered grass and brush growing up through the gravel. The area has a few small trees around the perimeter of the property. The estimated C value after construction is complete is 0.70 to reflect the proposed gravel condition. Side slopes proposed will be grassed swales with a runoff coefficient of 0.47 (heavy soil, steep >7%).

2.3.2 Main Site

Before construction activities, the average weighted runoff coefficient for the Main Site equals:

Type of Cover	% of Area Covered	Typičal 🤅 Value 👙	Weighted C Value
Soil and grass	25	.42	.11
(side slope and swale area)			
Aggregate (CA-6)	75	.70	.52
(Sacramento Parcel)			
Aggregate (CA-1)			
(Monarch Parcel)	<u></u>		

Weighted C =	.63

The estimated C value after construction for the top of the Sacramento Parcel would be 0.30 (heavy soil, 0% to 2%) for the grass condition alternative or 0.70 for the gravel condition alternative. Side slopes will be vegetated corresponding to a 0.30 C value and the Monarch Parcel will be a gravel condition (C value of 0.70) to be paved in the future (C value of 0.95)...

2.4 Site Map

A figure showing the location of the staging areas, Monarch parcel and Sacramento parcel is provided as Figure B-1 in Appendix B. Figure B-1 illustrates the general drainage patterns. Drawings of the Main Site areas (Figures B-2 through B-4) illustrate other features and include the following, as necessary:

- Construction site boundaries
- Areas of soil disturbance
- Areas that will not be disturbed (none)
- Approximate slopes after major grading
- Locations of major structural and non-structural controls
- Locations where stabilization practices are expected to occur
- · Springs, streams, wetlands, and other surface waters
- Storm water discharges
- 100 year flood plain, if determined
- Storage area locations (equipment, supplies, waste, stockpiles, etc.)

The figures will be updated to reflect any warranted changes or additions. Inspections may reveal necessary revisions and the figures may be manually updated.

2.5 Topography

Topography in this area is generally flat, developed with some areas of very gentle relief.

2.6 Area and Site Surface Waters

The Collateral Channel, which is a tributary to the Chicago Sanitary and Ship Canal (CSSC), is located approximately 200 feet south of the staging area across 31st Street. The Collateral Channel is a north-south slip, approximately 1,500 feet long and 130 feet wide. It empties into the CSSC.

The storm water from the Main Site enters the City of Chicago's combined sanitary and storm water collection system. The combined sanitary and storm water is treated by the MWRDGC. Future storm water from the Main site will eliminate all flow to the City's

combined sewer system by connecting directly to the collateral channel outfall pipe as proposed in the *Honeywell Celotex Main Site Cover Construction Work Plan Addendum – July 23, 2008 Update* (CH2M HILL, July 2008).

2.7 Endangered/Threatened Species

There are no known endangered/threatened species at the staging area or residential properties locations.

2.8 Historic Preservation

There are no known historic properties or places at the staging area or Main Site.

3.0 Best Management Practices for Storm Water Pollution Prevention

CH2M HILL will implement the Best Management Practices (BMPs) described below to prevent and control storm water run-on and run-off during construction activities at the staging area and Main Site. The description of controls includes:

- Control measures for potential pollutant sources
- Erosion and sediment controls, including structural and stabilization controls
- Material handling
- Spill prevention, control, and response
- Measures to protect endangered/threatened species
- Measures to protect Historic Places

3.1 Control Measures for Pollutant Sources during Construction Activities

The potential pollutant sources were described previously in Section 2.1.3. Specific measures to control pollutant discharges from these sources include:

- Vehicle and Equipment Fueling Areas: All fueling stations will have temporary secondary containment around the fuel tanks.
- Vehicle and Equipment Decontamination Areas: Vehicles and equipment will be
 cleaned of material prior to leaving the properties. A temporary decontamination area
 will be established, as necessary, and located within the construction site. If liquid
 decontamination is necessary, the liquids and solids generated will be contained,
 collected, sampled, and disposed at an approved disposal facility.
- Loading and Unloading Areas: Any soils or other materials spilled during loading or unloading will be cleaned up immediately. This includes soils on the outside of trucks (side rails), ground, and road surfaces.
- Vehicle and Equipment Maintenance Areas: If vehicle or equipment maintenance is necessary, it will be performed in an area designated for this purpose. Any spills will be cleaned up immediately. Precautions will be taken to prevent the release of pollutants to the environment from vehicle and equipment maintenance. Precautions will include the use of drip pans, mats, and other similar methods. No vehicle wash water will be allowed to run off the construction site or enter waters of the state.
- Excavation and Deposition Areas: To prevent the mobilization of pollutants in storm water runoff from excavation and deposition areas, BMPs described in the Erosion and Sediment Control section will be implemented.
 - Geotextile fabric may be placed over storm sewer inlets in areas where construction is being conducted. The geotextile fabric for use in inlet protection shall be nonwoven fabric consisting of continuous chain polymer filaments, formed into a

stable network by needle punching. The inlet filter material will be cleaned every storm event or as needed.

- Soil Stockpile Areas: In general, stockpiles are managed in the following manner:
 - Stockpiles of soil are placed on plastic sheeting at least 2-feet from the excavation within the disturbed area.
 - When precipitation is forecast, stockpiles of soil will be provided with a liner, cover, and perimeter berm to prevent run-on, run-off, and infiltration of precipitation. Typically, liners and covers are 6 mil polyethylene and berms are typically hay bales placed beneath the liner.
 - Covers and perimeter berms will be secured in place when not in use and at the end of each workday, or as necessary to prevent wind dispersion or runoff from major precipitation events.
- Waste and Material Storage Areas: Materials on the sites will be stored in areas
 designated for that purpose. Suitable measures will be taken in these areas to reduce the
 likelihood of a discharge. For example, when practicable, materials will be sheltered
 from rainfall.
- Offsite Vehicle Tracking: Sediment and the generation of dust shall be minimized.

3.2 Erosion and Sediment Controls

Construction activities will be implemented to attain the following goals and criteria, as applicable:

- Implement erosion and sediment controls during construction to retain sediment onsite to the extent practicable.
- Select, install, and maintain control measures in accordance with manufacturer's specifications and good engineering practices. If periodic inspections or other information indicate that a control measure has been used inappropriately or incorrectly, that control measure will be modified or replaced, as necessary.
- In the event that sediment escapes the construction site, remove offsite accumulations of sediment to minimize offsite impacts.
- Implement construction practices that prevent litter, construction debris, and chemicals exposed to storm water from becoming a pollutant source for storm water discharges.
- Erosion and sediment runoff is controlled through the use of structural and / or stabilization practices. Structural control practices may include the use of straw bales, silt fence, earth dikes, drainage swales, sediment traps, sediment basins, etc.
 Stabilization practices may include temporary or permanent seeding, mulching, geotextiles, sod stabilization, vegetative buffer strips, protection of trees, preservation of mature vegetation, etc.

Table 3-1 lists several structural and stabilization measures that may be used to control the quality of the storm water coming off the construction sites.

TABLE 3-1
Structural and Stabilization Measures
Main Site Cover Construction
Former Celotex Site – Chicago, Illinois

Control Measure	Location	Description of Control Measure ¹
Silt Fence	Along the perimeter of the construction sites.	To protect streams or wetland areas, to prevent erosion, and to keep sediment onsite. Silt fence consists of posts with filter fabric stretched across the posts. The lower end of the fence fabric is anchored or vertically trenched and covered with backfill. This prevents water from passing by the fence without first being filtered. The fabric allows for the water to pass offsite while retaining the sediment onsite.
Straw Bales	Around areas requiring protection, such as streams, and to form a temporary containment.	Straw bales work much like silt fence and may be used instead of silt fence. They can be used to form a barrier or redirect water. They impede storm water flow. Unlike silt fence, straw bales do not allow water to flow through freely, thus they are used where detention, not just filtration, is necessary.
Limit Entrance/Exit	Designated construction site entrances/exits. Exact location is determined in the field.	The purpose is to reduce tracking of soil off the site. These entrances/exits are usually constructed of fabric and large stone. The fabric is laid down on the soil and the rock is then placed on the fabric. The rough surface will shake and pull the soil from tires.
Temporary Seeding	Disturbed areas where the construction activity has temporarily ceased for more than 21 days. Seeding is to be implemented within 14 days of activity ceasing.	Growing of a short-term vegetative cover on disturbed areas that may be in danger of erosion.
Mulching	On slopes steeper than 2:1 or on areas that have been seeded. Must be implemented within 14 days of activity ceasing.	Temporary soil stabilization or erosion control practices where materials, such as, grass, wood chips, hay, etc. are placed on the soil surface.
Preservation of Natural Vegetation	Wherever practical.	Wherever possible, existing vegetation should be retained. It minimizes erosion potential and protects water quality. The preservation of natural vegetation between the silt fence and stream will provide additional water quality improvement prior to the storm water entering State or U.S. waters.
Permanent Seeding or Sod	On appropriate disturbed areas once construction is complete and within 14 days.	Provides permanent stabilization to the soil and reduces erosion.

¹ There are no identified streams or wetland areas located near the Main Site.

3.3 Material Handling

The following material handling procedures will be implemented during construction activities:

- Waste containers (solid and liquid) will be emptied frequently enough to prevent them
 from overflowing. The area will be kept free of trash and spills. Liquid waste containers,
 such as waste oil, will have secondary containment.
- Trash receptacles will be equipped with covers.
- Storage containers (drums, bags, etc.) will be stored away from traffic to prevent accidental spills.
- Containers will be kept closed, except to add or remove material, as necessary.
- Containers will be stored in such a manner to prevent corrosion that could result from contact between the container and the ground, resulting in a release.
- Containers will be labeled to show name and type of substance, health hazards, and other appropriate information.
- Material Safety Data Sheets (MSDS) for substances used or stored onsite will be available for review and use.

Materials stored onsite shall be inventoried on the form provided in Appendix E and records of the inventories will be maintained at the CH2M HILL field office.

3.4 Spill Prevention, Control, and Response

The following procedures shall be followed for the prevention and mitigation of minor spills and releases during construction activities.

Incidental spills and releases are considered small spills (not reportable). CH2M HILL and CH2M HILL's subcontractors shall respond to all minor spills as soon as practicable. CH2M HILL and CH2M HILL's subcontractors shall respond to medium or large spills (reportable quantities or larger), according to the project Spill Response Plan and the Emergency Response Plan contained in the Health and Safety Plan. These plans are maintained at the field office.

General spill prevention procedures follow:

- Fuel and waste containers/tanks shall be bermed or otherwise contained to prevent releases. The bermed volume shall be equal to the full capacity of the container(s)/tank(s). When practicable, for areas on soil, the area inside the berm will be covered with an oil resistant membrane to minimize soil contamination in the event of a spill. Additionally, if practicable, these areas will be sheltered from precipitation to prevent overflow of the bermed volumes.
- Fueling operations and vehicle/equipment maintenance shall be performed at designated facilities, when practical.
- Drip pans and tarpaulins will be used during maintenance and fueling to capture minor spills and leaks during fueling and maintenance.

- Each location having fueling operations, fuel containers/tanks, and/or waste container/tanks shall have a sufficient number of spill kits to contain minor spills and leaks.
- For detailed spill response procedures, refer to the Spill Response Plan. The general procedures for spill response are as follows:
 - Assure personal safety, and then evaluate the area and nature of the spill.
 - Identify the source and stop the flow of pollutants, if it can be done safely.
 - Contain the spill with absorbent materials or by berming the area.
 - Remove and contain the spilled material, contaminated media, and cleanup material, and transport to the designated location for collection of such material.
 - Contact the appropriate personnel listed in the Spill Response Plan.
 - Record pertinent facts.

3.5 Measures to Protect Endangered/Threatened Species

There are no endangered species identified in the remedial action area. If endangered species and/or critical habitats are found on or near these sites, work will be stopped and the situation evaluated.

3.6 Measures to Protect Historic Places

There are no historic places identified in the remedial action area. If historic places are found on or near these sites, work will be stopped and the situation evaluated.

3.7 Other Controls

3.7.1 Employee Training

Appropriate CH2M HILL and CH2M HILL subcontractor personnel will be trained and aware of the SWP3 requirements and measures that will need to be implemented. Additionally, CH2M HILL's subcontractors will be responsible for their lower tier subcontractor(s) being trained and aware of the requirements and measures to be implemented under the SWP3.

3.7.2 General Controls

The following general erosion control requirements shall be implemented during construction activities:

- Minimize the time that bare soil is exposed before stabilization.
- Minimize the disturbance of existing vegetation.
- Prevent solid materials, oils, greases, etc. from discharging into waters of the State and U.S.

4.0 Maintenance

All erosion and sediment control measures and other protection measures will be maintained in effective operating condition. Maintenance will be performed on an "asneeded" basis. Specific maintenance requirements include, but are not limited to:

- Removal of sediment and other debris collected behind silt fence or straw bales.
- Gravel and sediment shall be removed from construction entrances/exits and replaced
 with new gravel whenever 50 percent or more of the void space appears filled with
 sediment, based on visual inspection.

5.0 Inspections

Inspections will be performed to review the areas for evidence of, or the potential for, pollutants leaving the site. The controls identified in Section 3 will be inspected to verify they are being implemented properly.

As necessary, the SWP3 will be revised to incorporate any changes that come about as a result of the inspection. Changes that affect the description of pollutant sources or the pollution prevention control measures will be made to the SWP3 within 7 days of the inspection. A record of the inspections will be maintained at the CH2M HILL field office as part of the SWP3.

5.1 Requirements During Construction

The following areas will be inspected at a minimum, every 14 days, and within 24 hours of the end of a storm event of 0.5 inches or greater:

- Disturbed areas that have not been finally stabilized
- Storage areas that are exposed to precipitation
- Structural control measures
- Construction entrances/exits

Inspections shall be the responsibility of and performed by CH2M HILL and/or CH2M HILL's subcontractors. Inspections will be recorded on the SWP3 Inspection Checklist, provided in Appendix D. A copy of the detailed area drawings will be used during inspections and will be manually updated during inspections, as necessary, to reflect any changes or additions to the following features:

- Construction site boundaries
- Areas of soil disturbance
- Areas which will not be disturbed
- Approximate slopes after major grading
- Areas used for storage of materials, soil, or waste
- Locations of major erosion control features/structures (silt fence, straw bales, etc.)
- Springs, streams, wetlands, and other surface waters
- Storm water discharge locations

The updated drawings and Inspection Checklists will be maintained at the CH2M HILL field office. Table 5-1 provides storm water BMP inspection/maintenance guidelines.

TABLE 5-1

Storm Water Inspection/Maintenance Guidelines Main Site Cover Construction Former Celotex Site – Chicago, Illinois

EROSION CONTROL BLANKET

Is fabric damaged, loose, or need repairs?

MULCHING

- · Distributed uniformly?
- Any evidence of mulch being blown or washed away?

SILT FENCE

- Is the fence damaged, collapsed, or ineffective?
- Is excessive sedimentation against the fence present?
- Has sediment been removed from behind fence?
- Is the silt fence properly installed and positioned?

STRAW BALES

- Are the straw bales damaged or deteriorated, or ineffective?
- Has sediment been removed from behind the bales?
- Are the bales installed and positioned correctly?

TEMPORARY SEEDING

- Is the seeding protected by mulch?
- Has any erosion occurred in the seeded area?
- Any evidence of vehicle tracking on seeded areas?

VEHICLE TRACKING

- Is the gravel surface clogged with mud or sediment?
- Is the gravel surface sinking into the ground?
- Has sediment been tracked onto public roads? If yes, has it been cleaned up?

5.2 Requirements Prior to Final Stabilization

Inspections will be reduced to once per month after construction activities are complete. A record of these inspections will be maintained at the CH2M HILL field office.

6.0 Non-Storm Water Discharges

Discharges, other than storm water from construction activities, are not anticipated. However, the following discharges are allowable:

- Fire fighting activities
- Fire hydrant flushing
- Vehicle wash water (where detergents are not used)
- Water used to control dust
- Potable water sources (includes waterline flushing)
- External building washdown (which does not use detergents)
- Pavement washdown (where spills or leaks of toxic or hazardous materials have not occurred and where detergents are not used)
- Air conditioning condensate
- Uncontaminated groundwater or spring water
- Foundation or footing drains (where flows are not contaminated with process materials, such as solvents)

7.0 Contractor Certification

The Contractor Certification forms signed by CH2M HILL's subcontractors are provided in Appendix E.

SWPPP_MS_FINAL_080708.DOC

7-1

8.0 Retention of Records

A copy of this SWP3 and all inspection reports are required to be maintained at the CH2M HILL field office during the duration of the construction period, project initiation through final stabilization. The SWP3, inspection records, and reports shall be retained for a period of at least 3 years from the date the areas are finally stabilized.

APPENDIX A

National Pollutant Discharge Elimination System General Permit (ILR10) for Storm Water Discharges from Construction Activity

Public Notice Beginning Date: June 6, 2008 Public Notice Ending Date: July 7, 2008

National Pollutant Discharge Elimination System (NPDES)
Permit Program

PUBLIC NOTICE/FACT SHEET

of

Reissued General NPDES Permit to Discharge Storm Water From Construction Site Activities into Waters of the State

The Illinois Environmental Protection Agency (IEPA) has made a tentative determination to reissue NPDES General Permit No. ILR10 for the discharge of storm water associated with industrial activity from construction sites into waters of the state for the following types of dischargers:

Coverage under this permit This Permit covers all areas of the State of Illinois

Eligibility

- 1. This permit shall authorize all discharges of storm water associated with industrial activity from construction sites that will result in the disturbance of one or more acres total land area, construction sites less than one acre of total land that is part of a larger common plan of development or sale if the larger common plan will ultimately disturb one or more acres total land area. Construction sites that are designated by the Agency that have the potential for contribution to a violation of water quality standards or significant contribution of pollutants to waters of the State, occurring after the effective date of this permit (including discharges occurring after the effective date of this permit where the construction activity was initiated before the effective date of this permit), except for discharges identified under paragraph I.B.3 (Limitations on Coverage) are also authorized by this permit.
- 2. This permit may only authorize a storm water discharge associated with industrial activity from a construction site that is mixed with a storm water discharge from an industrial source other than construction, where:
 - a. the industrial source other than construction is located on the same site as the construction activity;
 - b. storm water discharges associated with industrial activity from the areas of the site where construction activities are occurring are in compliance with the terms of this permit; and
 - c. storm water discharges associated with industrial activity from the areas of the site where industrial activity other than construction are occurring (including storm water discharges from dedicated asphalt plants and dedicated concrete plants) are covered by a different NPDES general permit or individual permit authorizing such discharges.
- 3. Limitations on Coverage. The following storm water discharges from construction sites are not authorized by this permit:
 - a. storm water discharges associated with industrial activity that originate from the site after construction activities have been completed and the site has undergone final stabilization.
 - b. discharges that are mixed with sources of non-storm water other than discharges identified in Part III.A (Prohibition on Non-Storm Water Discharges) of this permit and in compliance with Part IV.D.5 (Non-Storm Water Discharges) of this permit.
 - c. storm water discharges associated with industrial activity that are subject to an existing NPDES individual or general permit or which are issued a permit in accordance with Part VI.N (Requiring an Individual Permit or an Alternative General Permit) of this permit. Such discharges may be authorized under this permit after an existing permit expires provided the existing permit did not establish numeric limitations for such discharges.
 - d. storm water discharges from construction sites that the Agency has determined to be or may reasonably be expected to be contributing to a violation of a water quality standard.
 - e. Storm water discharges that the Agency, at its discretion, determines are not appropriately authorized or controlled by this general permit.

Final Conditions

Length of Permit:

Classification of Receiving Waters:

Discharge No(s).:

Type of Waste

Flow Rate:

Approximately 5 Years

All surface waters of the State

Various Locations

Storm Water Runoff

Varies

The general permit does not name any Permittees, nor does it authorize any person to discharge. The authorization to discharge under a general permit will be by separate letter, issued to a specific applicant. The letters can be issued at any time while the Permit is in effect.

Interested persons are invited to submit written comments on the draft permits to the IEPA at the above address. The NPDES permit number(s) must appear on each comment page. Any interested person may submit a written request for a public hearing on a draft permit, stating his or her name and address, the nature of the issues proposed to be raised and the evidence proposed to be presented with regards to those issues.

The Public Notice, Fact Sheet, draft permit, comments received, and other documents are available for inspection and may be copied at the IEPA between 9:30 a.m. and 3:30 p.m. Monday through Friday.

All comments on the draft permit and requests for hearing must be received by the IEPA not later than 30 days from the date of this publication. If written comments or requests indicate a significant degree of public interest in the draft permit, the permitting authority may, at its discretion, hold a public hearing. Public notice will be given 30 days before any public hearing. For further information call the Public Notice Clerk at 217/782-0610.

Public Notice/Fact Sheet Issued By:

Illinois Environmental Protection Agency Division of Water Pollution Control Permit Section 1021 North Grand Avenue East Post Office Box 19276 Springfield, Illinois 62794-9276 217/782-0610

ILR10TMLpn2008.doc

Part V. RETENTION OF RECORDS

- A. The permittee shall retain copies of storm water pollution prevention plans and all reports and notices required by this permit, and records of all data used to complete the Notice of Intent to be covered by this permit, for a period of at least three years from the date that the permit coverage expires or is terminated. This period may be extended by request of the Agency at any time.
- B. The permittee shall retain a copy of the storm water pollution prevention plan required by this permit at the construction site from the date of project initiation to the date of final stabilization.

Part VI. STANDARD PERMIT CONDITIONS

A. Duty to Comply.

The permittee must comply with all conditions of this permit. Any permit noncompliance constitutes a violation of Illinois Environmental Protection Act and the CWA and is grounds for enforcement action; for permit termination, revocation and reissuance, or modification; or for denial of a permit renewal application.

- B. Continuation of the Expired General Permit. This permit expires five years from the date of issuance. An expired general permit continues in force and effect until a new general permit or an individual permit is issued. Only those facilities authorized to discharge under the expiring general permit are covered by the continued permit.
- C. Need to halt or reduce activity not a defense. It shall not be a defense for a permittee in an enforcement action that it would have been necessary to halt or reduce the permitted activity in order to maintain compliance with the conditions of this permit.
- D. **Duty to Mitigate**. The permittee shall take all reasonable steps to minimize or prevent any discharge in violation of this permit which has a reasonable likelihood of adversely affecting human health or the environment.
- E. **Duty to Provide Information**. The permittee shall furnish within a reasonable time to the Agency or local agency approving sediment and erosion plans, grading plans, or storm water management plans; or in the case of a storm water discharge associated with industrial activity which discharges through a municipal separate storm sewer system with an NPDES permit, to the municipal operator of the system, any information which is requested to determine compliance with this permit. Upon request, the permittee shall also furnish to the Agency or local agency approving sediment and erosion plans, grading plans, or storm water management plans; or in the case of a storm water discharge associated with industrial activity which discharges through a municipal separate storm sewer system with an NPDES permit, to the municipal operator of the system, copies of records required to be kept by this permit.
- F. Other Information. When the permittee becomes aware that he or she failed to submit any relevant facts or submitted incorrect information in the Notice of Intent or in any other report to the Agency, he or she shall promptly submit such facts or information.
- G. **Signatory Requirements**. All Notices of Intent, storm water pollution prevention plans, reports, certifications or information either submitted to the Agency or the operator of a large or medium municipal separate storm sewer system, or that this permit requires be maintained by the permittee, shall be signed.
 - 1. All Notices of Intent shall be signed as follows:
 - a. For a corporation: by a responsible corporate officer. For the purpose of this section, a responsible corporate officer means: (1) a president, secretary, treasurer, or vice-president of the corporation in charge of a principal business function, or any other person who performs similar policy or decision-making functions for the corporation; or (2) the manager of one or more manufacturing, production or operating facilities employing more than 250 persons or having gross annual sales or expenditures exceeding \$25,000,000 (in second-quarter 1980 dollars) if authority to sign documents has been assigned or delegated to the manager in accordance with corporate procedures;
 - b. For a partnership or sole proprietorship: by a general partner or the proprietor, respectively; or
 - c. For a municipality, State, Federal, or other public agency: by either a principal executive officer or ranking elected official. For purposes of this section, a principal executive officer of a Federal agency includes (1) the chief executive officer of the agency, or (2) a senior executive officer having responsibility for the overall operations of a principal geographic unit of the agency.
 - All reports required by the permit and other information requested by the Agency shall be signed by a person described above or by a duly authorized representative of that person. A person is a duly authorized representative only if:
 - a. The authorization is made in writing by a person described above and submitted to the Agency.
 - b. The authorization specifies either an individual or a position having responsibility for the overall operation of the regulated facility or activity, such as the position of manager, operator, superintendent, or position of equivalent responsibility or an individual or position having overall responsibility for environmental matters for the company. (A duly authorized representative may thus be either a named individual or any individual occupying a named position).
 - c. Changes to authorization. If an authorization under paragraph I.C (Authorization) is no longer accurate because a different individual or position has responsibility for the overall operation of the construction site, a new authorization satisfying the requirements of paragraph I.C must be submitted to the Agency prior to or together with any reports, information, or applications to be signed by an authorized representative.
 - d. Certification. Any person signing documents under this Part shall make the following certification:

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for

- Inspect at reasonable times any facilities, equipment (including monitoring and control equipment), practices, or operations regulated or required under this permit; and
- 4. Sample or monitor at reasonable times, for the purposes of assuring permit compliance or as otherwise authorized by the Clean Water Act, any substances or parameters at any location.
- R. **Permit Actions**. This permit may be modified, revoked and reissued, or terminated for cause. The filing of a request by the permittee for a permit modification, revocation and reissuance, or termination, or a notification of planned changes or anticipated noncompliance does not stay any permit condition.

Part VII. REOPENER CLAUSE

- A. If there is evidence indicating potential or realized impacts on water quality due to any storm water discharge associated with industrial activity covered by this permit, the discharger may be required to obtain an individual permit or an alternative general permit in accordance with Part I.C (Authorization) of this permit or the permit may be modified to include different limitations and/or requirements.
- B. Permit modification or revocation will be conducted according to provisions of 35 III. Adm. Code, Subtitle C, Chapter I and the provisions of 40 CFR 122.62, 122.63, 122.64 and 124.5 and any other applicable public participation procedures.
- C. The Agency will reopen and modify this permit under the following circumstances:
 - 1. the U.S. EPA amends its regulations concerning public participation;
 - a court of competent jurisdiction binding in the State of Illinois or the 7th Circuit issues an order necessitating a modification of public participation for general permits; or
 - 3. to incorporate federally required modifications to the substantive requirements of this permit.

Part VIII. DEFINITIONS

"Agency" means the Illinois Environmental Protection Agency.

"Best Management Practices" ("BMPs") means schedules of activities, prohibitions of practices, maintenance procedures, and other management practices to prevent or reduce the pollution of waters of the United States. BMPs also include treatment requirements, operating procedures, and practices to control plant site runoff, spillage or leaks, sludge or waste disposal, or drainage from raw material storage.

"Commencement of Construction" - The initial disturbance of soils associated with clearing, grading, or excavating activities or other construction activities.

"CWA" means Clean Water Act (formerly referred to as the Federal Water Pollution Control Act or Federal Water Pollution Control Act Amendments of 1972) Pub.L. 92-500, as amended Pub. L. 95-217, Pub. L. 95-576, Pub. L. (96-483 and Pub. L. 97-117, 33 U.S.C. 1251 et.seg.)

"Dedicated portable asphalt plant" - A portable asphalt plant that is located on or contiguous to a construction site and that provides asphalt only to the construction site that the plant is located on or adjacent to. The term dedicated portable asphalt plant does not include facilities that are subject to the asphalt emulsion effluent limitation guideline at 40 CFR 443.

"Dedicated portable concrete plant" - A portable concrete plant that is located on or contiguous to a construction site and that provides concrete only to the construction site that the plant is located on or adjacent to.

"Dedicated sand or gravel operation" - An operation that produces sand and/or gravel for a single construction project.

"Director" means the Director of the Illinois Environmental Protection Agency or an authorized representative.

"<u>Final Stabilization</u>" means that all soil disturbing activities at the site have been completed, and that a uniform perennial vegetative cover with a density of 70% the cover for unpaved areas and areas not covered by permanent structures has been established or equivalent stabilization measures (such as the use of riprap, gabions or geotextiles) have been employed.

"Large and Medium municipal separate storm sewer system" means all municipal separate storm sewers that are either:

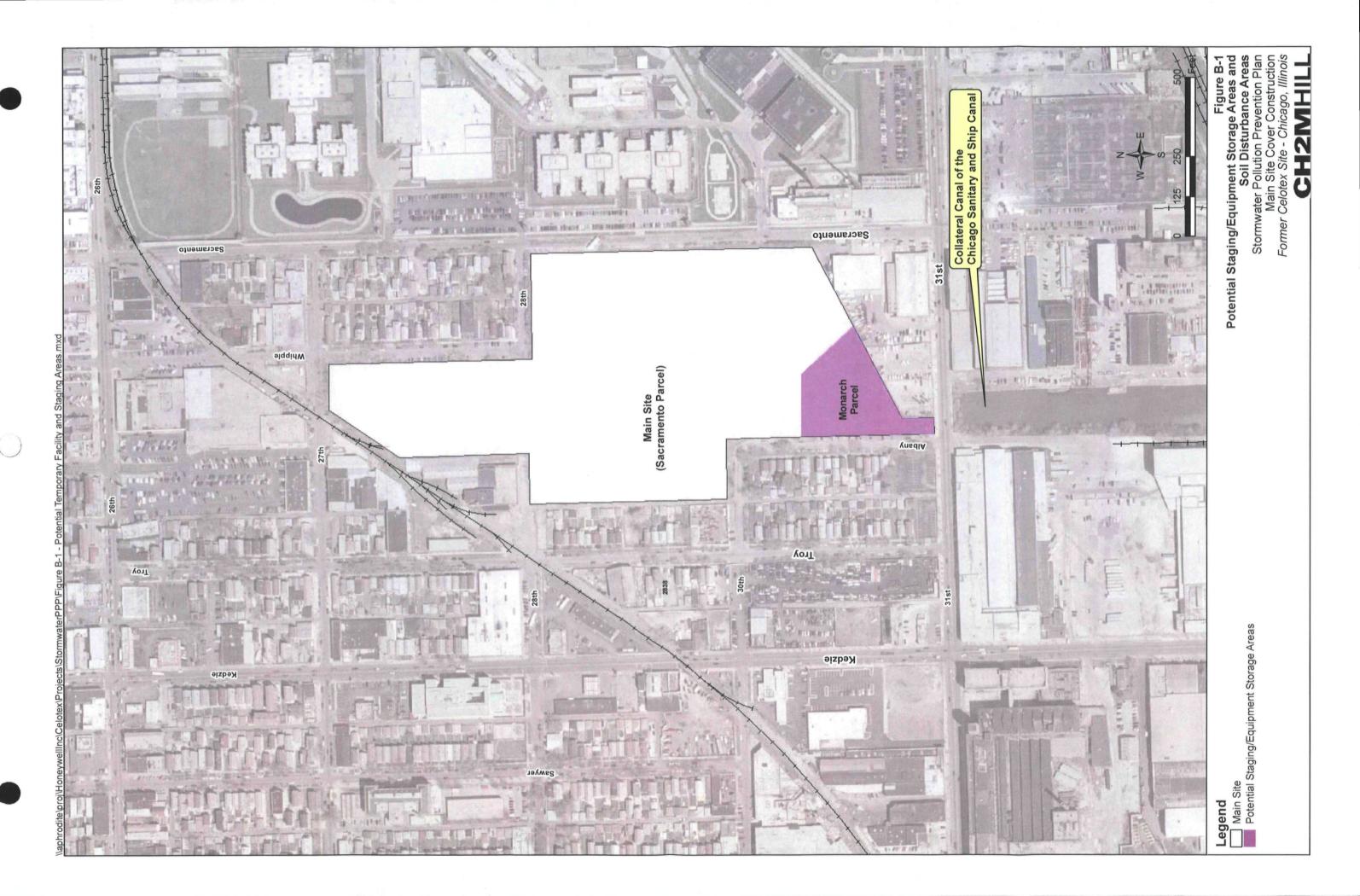
- (i) Located in an incorporated place (city) with a population of 100,000 or more as determined by the latest Decennial Census by the Bureau of Census (these cities are listed in Appendices F and G of 40 CFR Part 122); or
- (ii) Located in the counties with unincorporated urbanized populations of 100,000 or more, except municipal separate storm sewers that are located in the incorporated places, townships or towns within such counties (these counties are listed in Appendices H and I of 40 CFR Part 122); or
- (iii) Owned or operated by a municipality other than those described in paragraph (i) or (ii) and that are designated by the Director as part of the large or medium municipal separate storm sewer system.

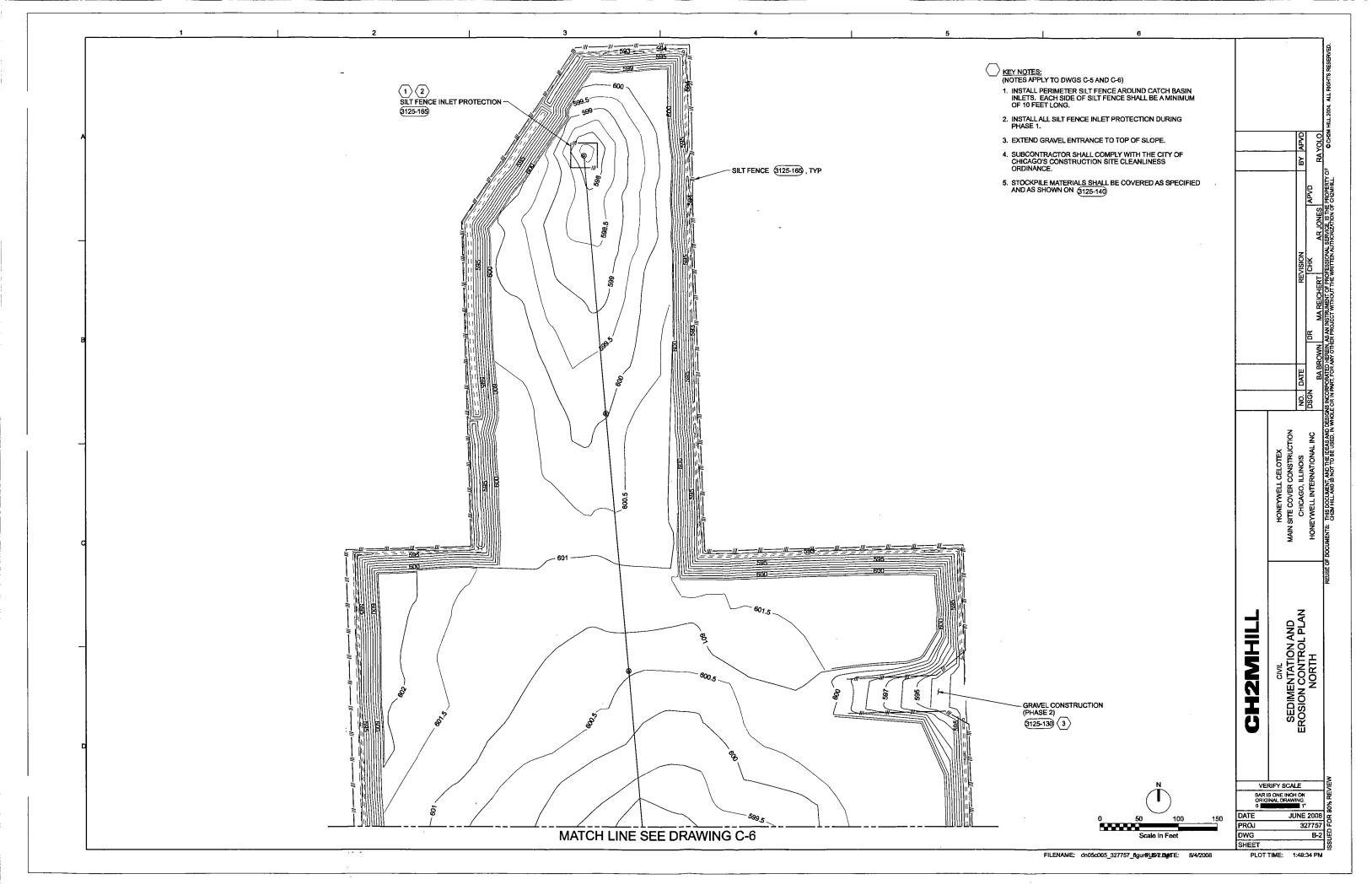
"NO!" means notice of intent to be covered by this permit (see Part II of this permit.)

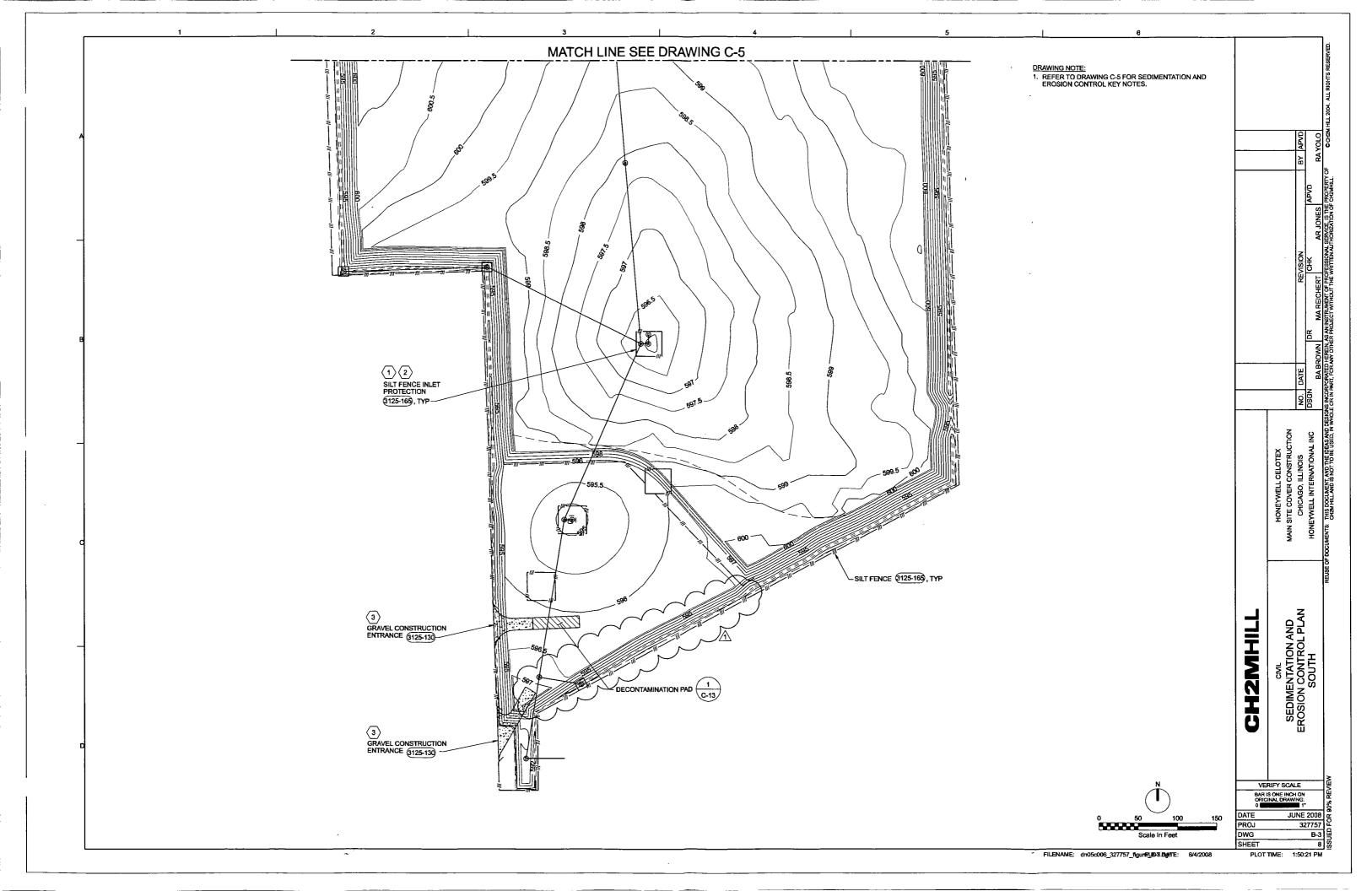
"Point Source" means any discernible, confined, and discrete conveyance, including but not limited to, any pipe, ditch, channel, tunnel, conduit, well, discrete fissure, container, rolling stock, concentrated animal feeding operation, landfill leachate collection system, vessel or other floating craft from which pollutants are or may be discharges. This term does not include return flows from irrigated agriculture or agricultural storm water runoff.

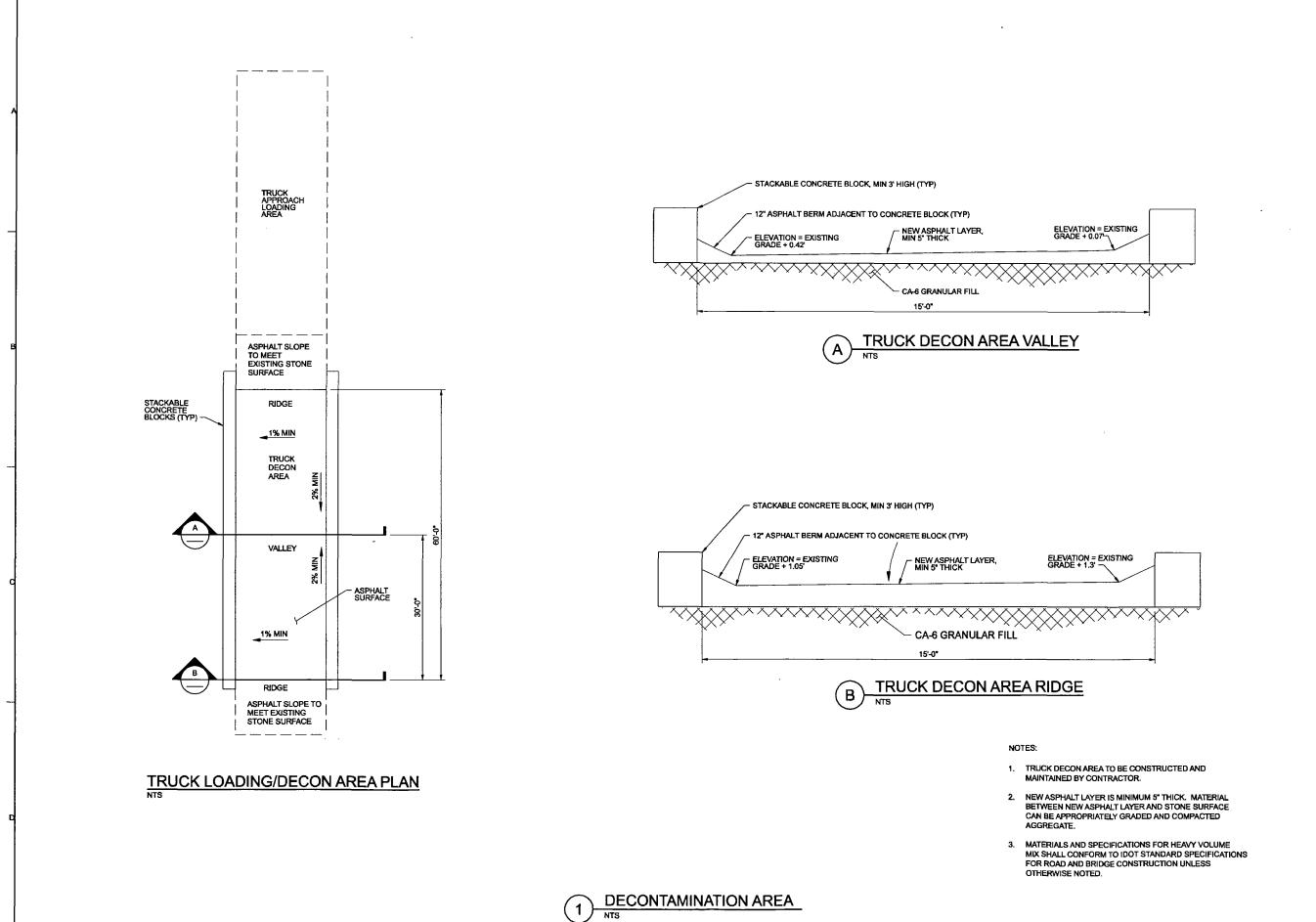
"Runoff coefficient" means the fraction of total rainfall that will appear at the conveyance as runoff.

"Storm Water" means storm water runoff, snow melt runoff, and surface runoff and drainage.









FILENANE: dn05c013_327757_figur@LB04.Bg/TE: 8/11/2008

CIVIL DECONTAMINATION PAD DETAIL

VERIFY SCALE
BAR IS ONE INCH ON
ORIGINAL DRAWING.

PLOT TIME: 3:11:31 PM

JUNE 2008

365109

CH2MHILL

PROJ

DWG SHEET

APPENDIX C

SWP3 Inspection Checklist

SWP3 Inspection Checklist

Location of Inspection:	Date:
Inspector:	Company:

Inspection Procedure	Yes/No	Comments	Date of Corrective Action	Corrective Action Taken
Is there any evidence of sediment leaving the construction site? If so, note areas.				
Have any adverse impacts, such as, flooding, structural damage, erosion, spillage, or accumulation of sediment, debris, or litter occurred on adjacent property, wetlands, or surface waters?				
Have the storm water BMPs been placed properly and effectively?				
Are the storm water BMPs functioning as intended?				
Is there evidence of discharges or spills of fuels or lubricants?				

LIST OF MATERIALS STORED ONSITE

Project Name:	_Celotex Residential Removal Action	Date:	
---------------	-------------------------------------	-------	--

Description of Material	Period on Site	Quantity	Location of Storage	Method of Storage	Description of Material Management Practices

Contractor Certification

(To be signed following project implementation)

"I certify under penalty of law that I understand the terms and conditions of the general National Pollutant Discharge Elimination System (NPDES) permit (ILR10) that authorizes the storm water discharges associated with industrial activity from the construction site identified as part of this certification."

Signature:	
Name (Printed or Typed):	
Title:	
Certification Date:	
Company:	
Address:	
Telephone Number:	
Site Address:	
2800 South Sacramento, Chicago, IL, 60623	

APPENDIX F

SWP3 Certification

Certification

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage this system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations."

Signature: Chuch Cealehon	
Name (Printed or Typed):	
Chick Geadelmann	
Title: Corporate Manage/	
Certification Date: $8/8/6$	

TEMPORARY OR PERMANENT STOP WORK RECORDS

Location:	·
Location.	

TEMPORARY OR PERMANENT	DATE STARTED	DATE ENDED	LOCATION	REMARKS
			-	
			.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	

MAJOR GRADING RECORDS

Location:			 No.

DATE STARTED	DATE ENDED	LOCATION	REMARKS
	1		

STABILIZATION RECORDS

Location:				
Location.				

TYPE	DATE STARTED	DATE ENDED	LOCATION	REMARKS
-	540			

Attachment 6 – Plat of Survey (2 copies)

Two copies of the original Plat of Survey were included in the original application to the City of Chicago Building Department. Copies of the Plat of Survey are available upon request in electronic format.

Attachment 7 – Building Code Matrix

CITY OF CHICAGO DEPARTMENT OF CONSTRUCTION AND PERMITS

GENERAL BUILDING REQUIREMENTS Per Chicago Zoning Ordinance(CZO) and Chicago Building Code (CBC) 2002 Edition

		CHAPTER/	Ordinance:	- Sec. 19	Requirement	Location/	Agency/	
II-EM	ISSUE	ARTICLE	Requirement	Actual	N/A	Sheet No.	Test No.	REMARKS
ZONI	NG REQUIREMENTS	, , , , , , , , , , , , , , , , , , , ,			300.0			
1.01	Zoning District	CZO Title 17	-			1		M2-3
1.02	Lot Area							19.7 Acres
BUIL	DING REQUIREMENTS							-
	Class J, miscellaneous buildings					• •		
2.01	and structures.	13-56-220					:	
	a) Fences	13-96-120	Х	Х				New fence installed around perimeter
				_				